Solid rocket motor propulsion

Satellite design & engineering

A. SQUELARD

Propulsion basics



Principles of propulsion

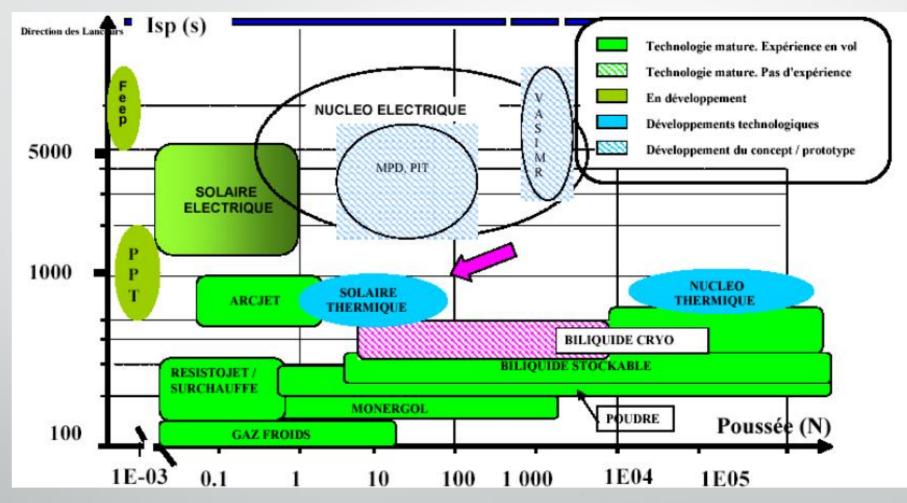
A reaction force (thrust) is created by the ejection of gas.

 $F \approx q \cdot V_e$

The thrust created by a balloon is clearly not sufficient ! Let's try to improve this technology ! Furthermore, the pressure in the balloon drops quickly ! We must find a way to maintain the pressure inside the motor. We need to increase q and V_e

To do that, the best solution is to use a controllable exothermic chemical reaction that transforms a liquid or a solid into a gas at high temperature : the commonest one is : combustion, but there are other solutions !

Other types of propulsion



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Liquid or solid propulsion

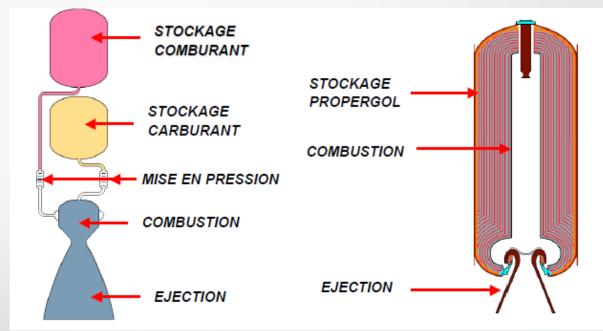
We will limit ourselves to combustion, and give the advantages of the two solutions

LIQUID

- High specific impulse
- Re-ignition and throttling possible

<u>SOLID</u> (fuel and oxidizer mixed in one solid block (grain)

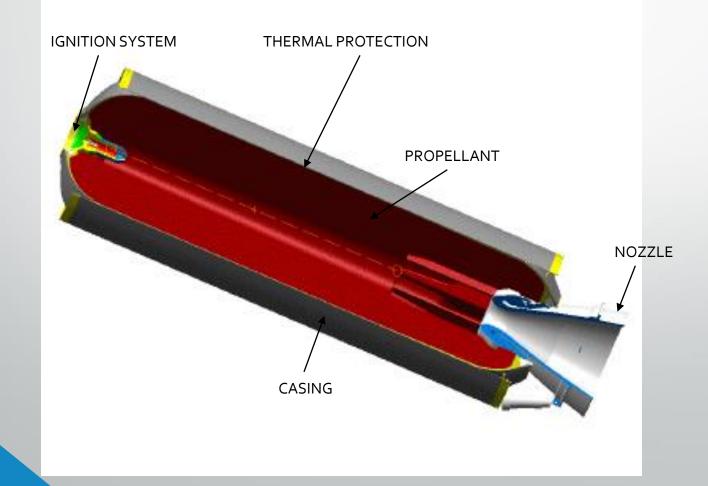
- Can deliver high thrust from a limited volume
- Almost immediate availability
- High reliability
- Moderate costs



From now on, we will limit ourselves to solid propulsion.

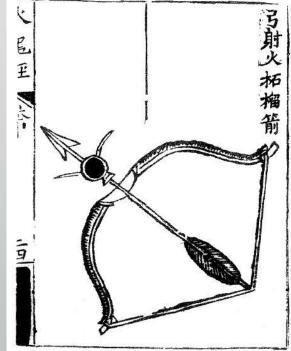
Solid propulsion

To reach sufficient thrusts, we will have to operate at pressures of several tens to hundreds bars, and eject the gasses at supersonic velocities. Therefore, the main elements of a solid rocket motor are :



History and applications

The first utilization dates back to 7th century, when black powder was invented in China, as incendiary arrows.

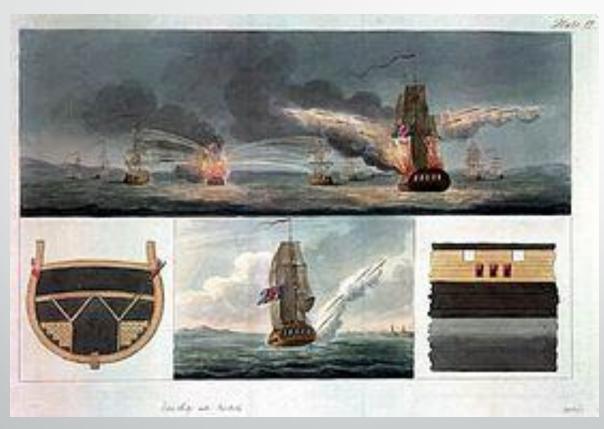




Propelled arrows were found in the 11th century, also in China

History (2)

The first scientific study is made by William Congreve, and the first rockets were used in battles against Napoleon, in particular Waterloo (1815).





History and applications

In 1888, Alfred Nobel discovers the homogeneous double base propellants, and that leads the way to military applications, which start growing during WWII.

Are well known the Stalin organs (USSR – 1941), the anti-tank weapons like the Panzerfaust (Germany – 1943), and the bazooka (USA – 1944). We find also applications to accelerate vehicles : (Opel car – 1928) and the JATO system (USA – 1942)

M13 rocket for Stalin organ

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C-130 takes off with the help of JATO rockets



Opel rocket car RAK-1-1928 -

Modern applications : military

Missiles

Strategic – ICBM Trident D2 (US)



Tactical – air-to-air MICA (France)

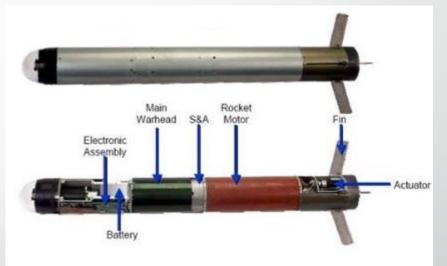


Boosters for missiles

Tomahawk cruise missile (US)

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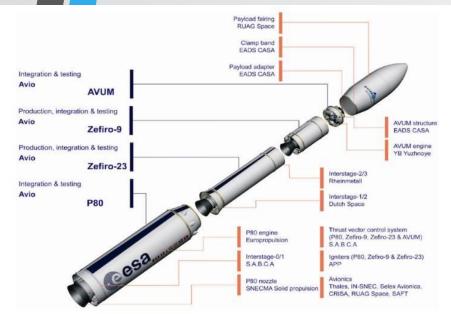
Tactical : anti-tank LAHAT (Israel)





Modern applications : civilian

Launcher stages



European Space Agency Agence spatiale européenne

Vega launcher – 3 solid propellant stages

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Launcher boosters

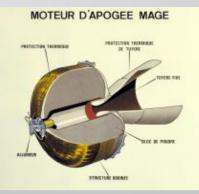


AJ-60A boosters mounted on Atlas V launcher

Other applications



STAR-5D rocket motors used to decelerate Mars Pathfinder to zero velocity on the Martian surface



The propellant grain

We have to define two parameters : composition and shape : these will define the performance and the thrust law of our motor.

COMPOSITION

History :

The first propellant was black powder (mixture of sulfur, charcoal and saltpeter [KNO₃]). Inefficient as propellant.

From end of XIX° century : homogeneous double base propellants : mixture of nitrocellulose and nitroglycerine. Still in use today (smokeless), but not able to be used in large motors (tens to hundreds of tons.

Composite propellants

Criteria of choice :

Energetic performances (high reaction temperature) Kinetic performances (combustion velocity) Mechanical behavior (resistance to loads) Safety and vulnerability (resistance to unwanted ignition) Resistance to ageing (life duration in storage) Cost in production Interface specifications

I will present here the composition that all the above requirements, and is used on all space launchers :

- Ammonium perchlorate (oxidizer) (70 %)
- Aluminum powder (fuel) (15 %)
- Polybutadiene matrix (binder and fuel) (12%)

Composite propellants

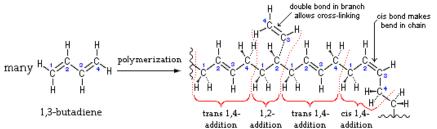
Ammonium perchlorate is a white powder. Its particle size controls :

- The viscosity
- The combustion velocity
- The particle size of Al₂O₃ (combustion by-product)

Aluminum is used in the form of powder. It increases the reaction temperature

The polybutadiene is a polymer that allows cross-linking betweer chains after curing, giving to the propellant grain its mechanical properties.





The propellant grain

After ignition, the burning reaction takes place on the free surface of the propellant. The mass flow, and consequently the thrust generated by a propellant grain is proportional to the

combustion surface at any moment of its operation.

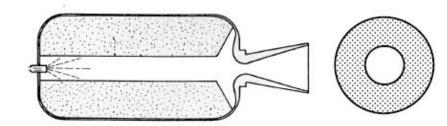
Assuming that the combustion velocity is the same in all directions, the combustion proceeds in parallel layers.

Therefore, the thrust depends on the motor and the propellant grain geometries.

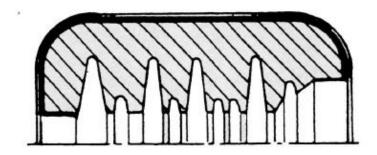
This initial geometry is the only way to control the thrust law of a solid rocket motor.

There are many geometries according to the required thrust law

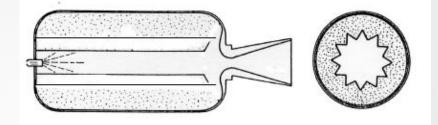
Shapes of propellant grain



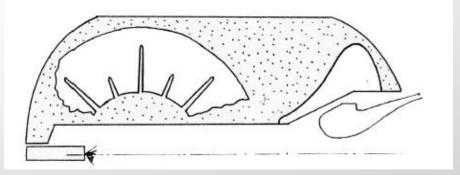
Cylindrical shape



Axisymmetric shape with teeth

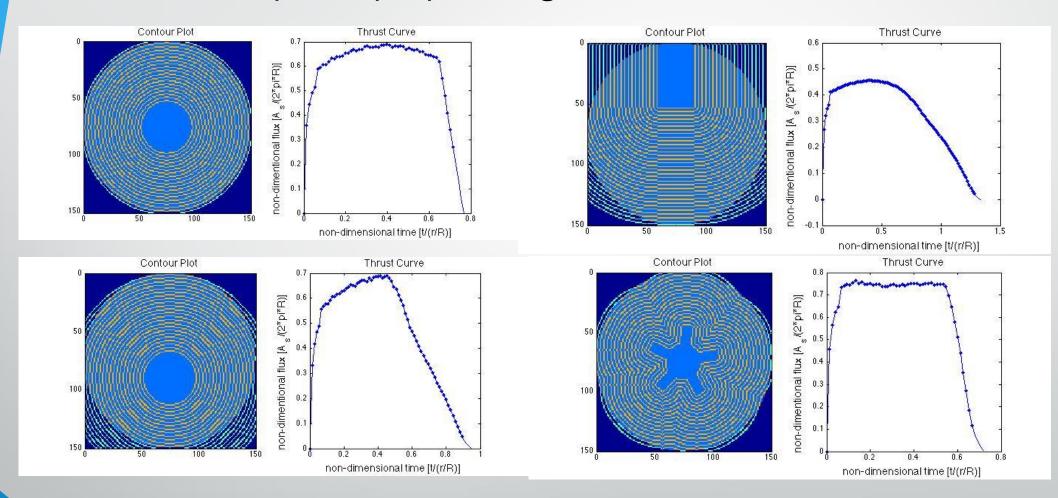


Star shape

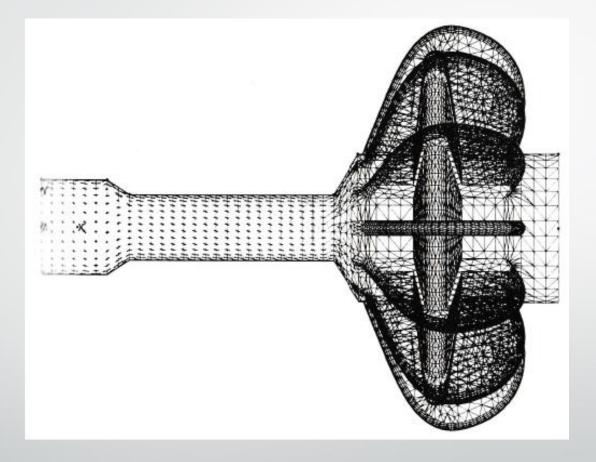


Cylindrical shape with rear finocyl

Shapes of propellant grains and thrust laws



Complex grain geometry represented by digital grid



Grain shape and thrust law : case of Ariane 5 MPS

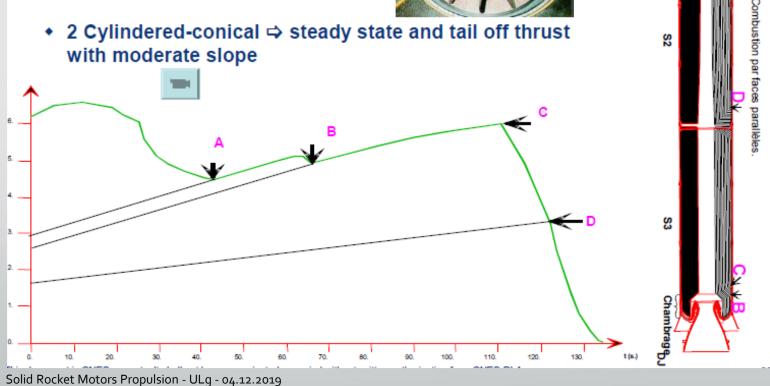
Example: MPS =

1 Star ⇒ high thrust for take-off

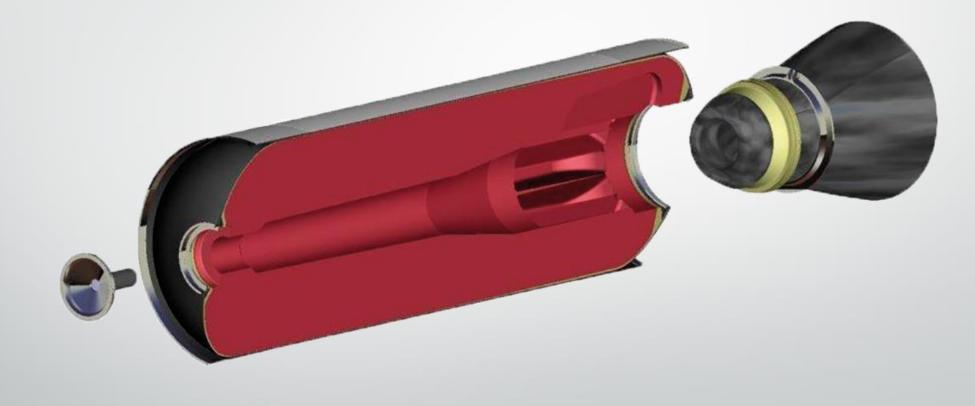


S2

with moderate slope



Ariane 6 booster (P120C)



Solid propulsion fundamental equations

$$\rho \cdot V_c \cdot S_c = C_D \cdot P_c \cdot A_t = gas mass flow$$

Where $\rho = \text{propellant density}$ $V_c = \text{combustion velocity}$ $S_c = \text{surface of combustion}$ $C_D = \text{nozzle discharge coefficient}$ $P_C = \text{combustion pressure}$ $A_t = \text{nozzle throat area}$

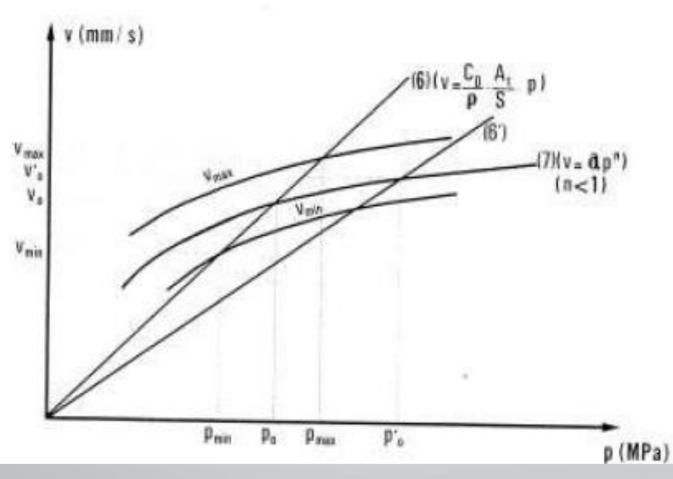
For most solid propellants :

 $V_c = a \cdot (P_c)^n$ with n < 1

With
$$\Gamma(\gamma) = \gamma \cdot \left(\frac{2}{\gamma+1}\right)^{\gamma+1/2(\gamma-1)}$$

 $C_D = \frac{\Gamma(\gamma)}{\sqrt{\gamma rT}}$

Operation point of a solid rocket motor



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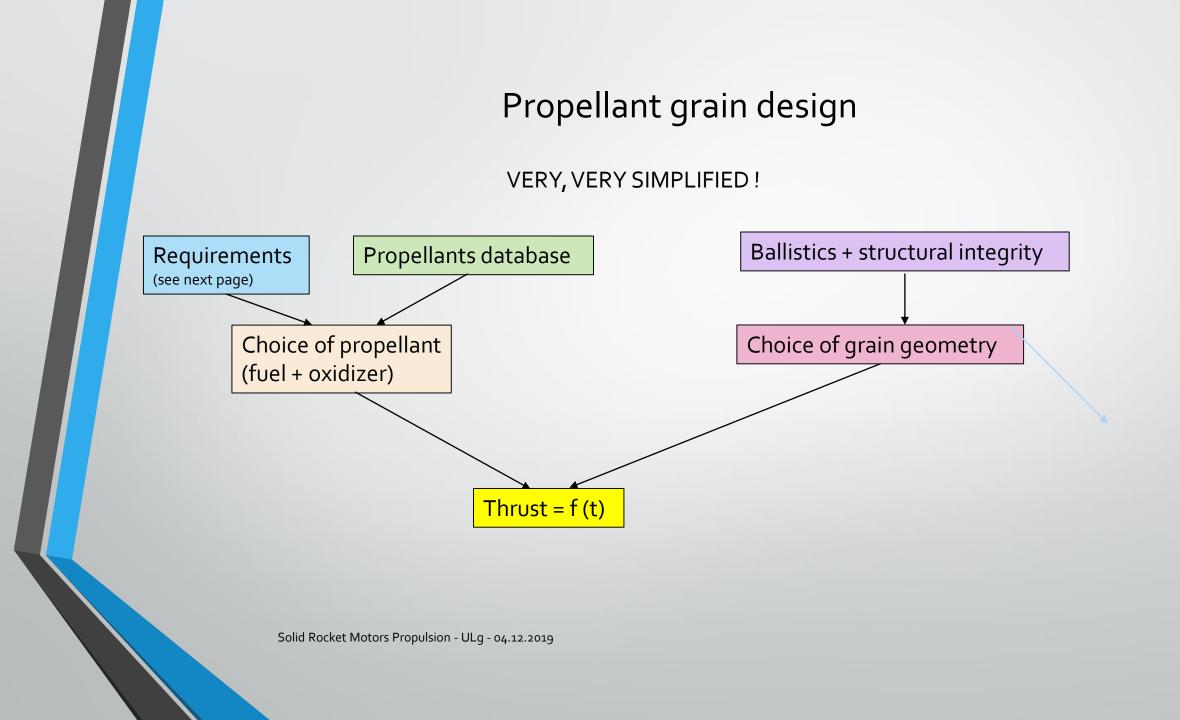
n < 1 (curve concavity oriented to the bottom) means stable operation for the motor.

n < 1 for most propellants, but not all !



SAFETY !!

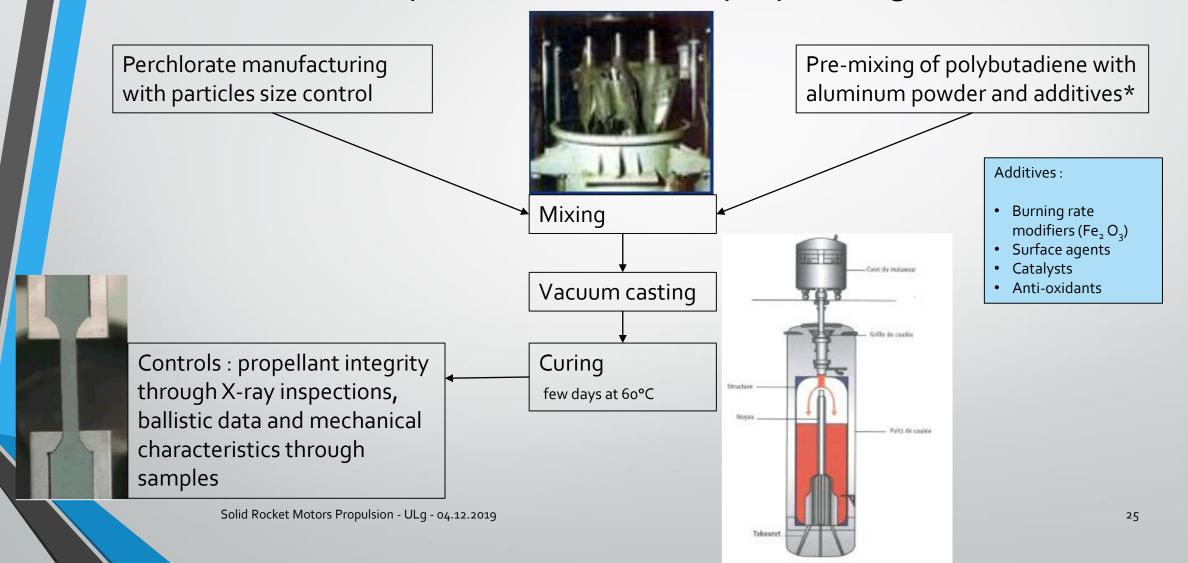
The linear burning rate of the propellant is the velocity at which the chemical reaction progresses under the effect of conduction and radiation and is function of pressure, but also of the initial temperature



Requirements for propellant design

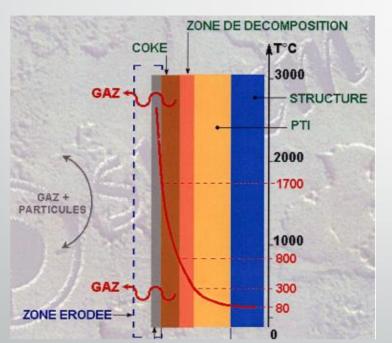
- Energy performance : I_{sp} , T_c , density
- Kinetic performances : maximum pressure, overall dimensions, weight
- Resistance to loads : shrinkage during curing, long-term storage, thermal cycles, firing
- Safety : resistance to mechanical or electrical aggression
- Resistance to ageing
- Compliance with interface specifications
- Production cost

Main steps to manufacture a propellant grain

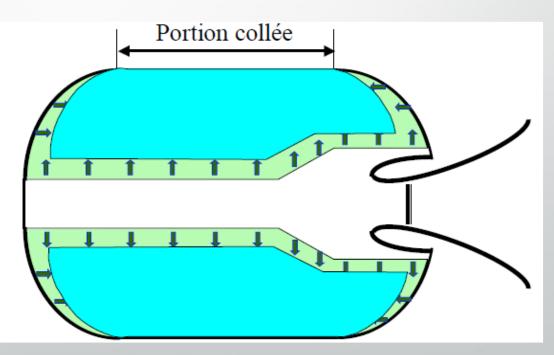


Thermal protections

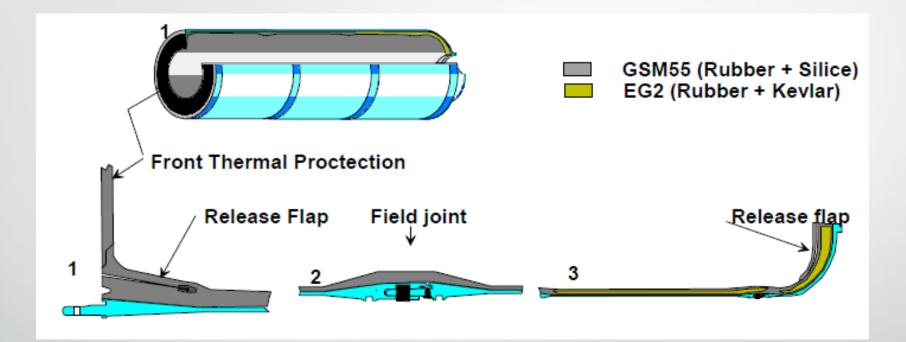
- Protects the casing from combustion gas when propellant has completely burned
- Inhibits the combustion where it is not needed (on Ariane MPS : frontal PT)
- Controls the loads due to propellant shrinkage when curing
- Made of rubber + additives







Thermal protections



Thermal protections installation

On metallic casings :

- Two possible processes
 - TP is installed on a mandrel, polymerized, machined, and then installed in the casing
 - TP in raw rubber is installed inside the casing by winding or draping and then polymerized in an autoclave.

On composite casings :

TP is wound around a mandrel, polymerized, machined, and then the casing is wound around the PTI.

Thermal protections installation



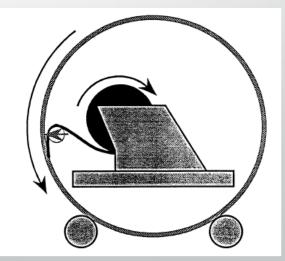
Manual draping on mandrel



Rubber tape machine feeding



Automatic winding machine



Casings (structures)

Two types of casings :

Metallic : steel or aluminum

Composite : carbon, glass or Kevlar fibers embedded in resin (epoxy)

The criteria of choice are :

- Production costs (raw materials, machines, control equipment, manufacturing difficultness)
- Performance (weight / allowable stress)
- Resistance to environment (heat, mechanical or chemical aggression)
- Other constraints (interfaces)

Comparison between materials

	$\rho \; (kg/m^3)$	E (MPa)	σ (MPa)	$E/\rho.g~(km)$	$\sigma/\rho.g~(km)$
ALU AZ5	2 800	75 000	420	2 730	15
TITANE TA6V	4 450	115 000	1 100	2 630	25
ACIER 35NCD16	7 800	205 000	1 500	2 680	19
D6AC (48 CDN 4-10) MPS	7 850	200 000	1 500	2 600	20
ACIER MARAGING (INOX)	8 000	190 000	1 900	2 420	24
COMPOSITE VERRE *	2 050	56 000	2 400	2 780	117
COMPOSITE KEVLAR *	1 350	85 000	2 300	6 420	170
COMPOSITE CARBONE *	1 550	170 000	4 200	11 000	276

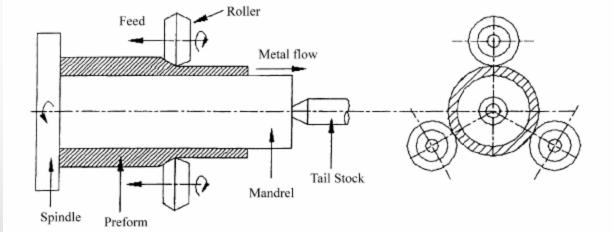
Metallic casings

Example : MPS of Ariane 5

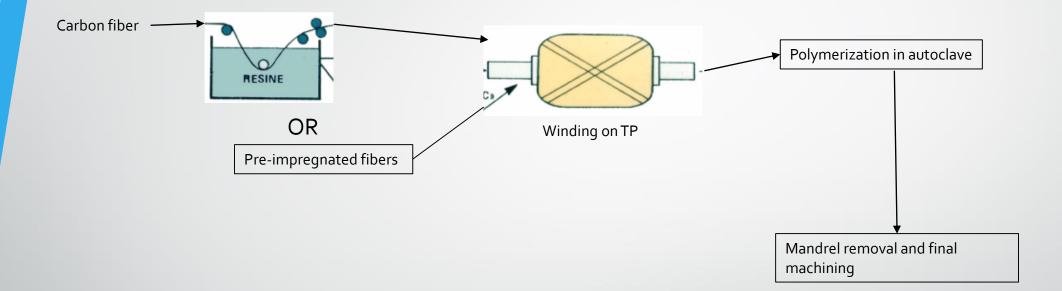
Material : Steel D6AC Domes : disk formed in shape of domes

Cylinders : from preforms flow-forming into cylinders, then heat treatment and welding of three cylinders



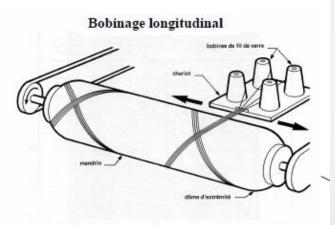


Composite casings

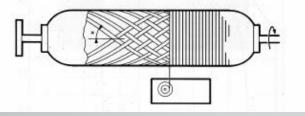


Composite casings

There are essentially two types of winding : polar and hoop



Bobinage circonférentiel





P8o (1st stage of VEGA) winding

Composite casings



Finished P8o composite casing

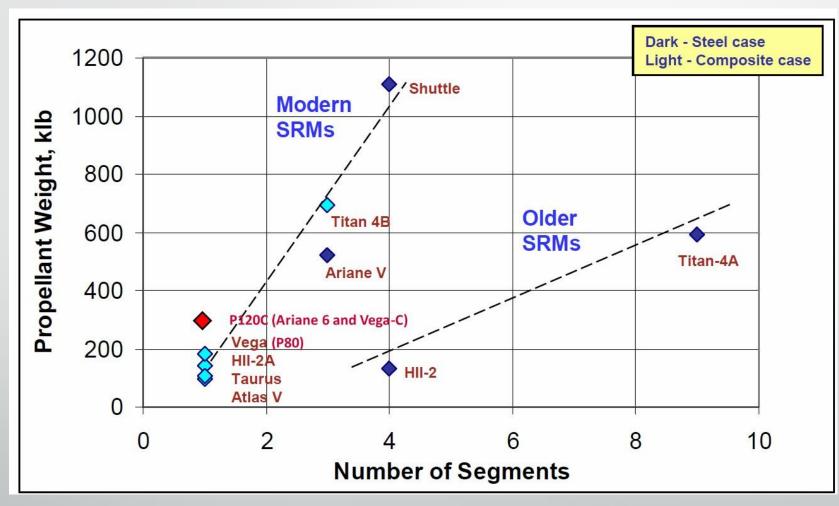


Finished Pathfinder booster segment (Prototype for SLS booster)

Booster segments

- For space launchers, the propellant grains are manufactured in several segments.
- To cast a booster grain in one piece would require huge installations for casting, handling and transportation.
- However, progress is made, and newer boosters stages are manufactured in one segment.

Booster segments (2)



Joints

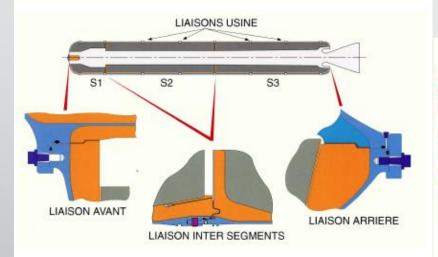
The joints between the segments are critical for safety. Any hot gas leak to the outside of the booster can have catastrophic consequences

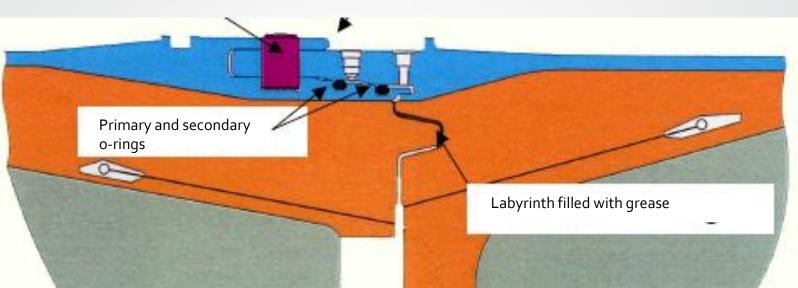
Casing tightness is made by redundant o-rings

Thermal protection tightness is made by a labyrinth geometry filled with grease. No flow \rightarrow the gasses cool rapidly.

Problem : the casing inflates when the inside pressure increases and the geometry around the o-rings changes : the pressure has to close gaps and not open them.

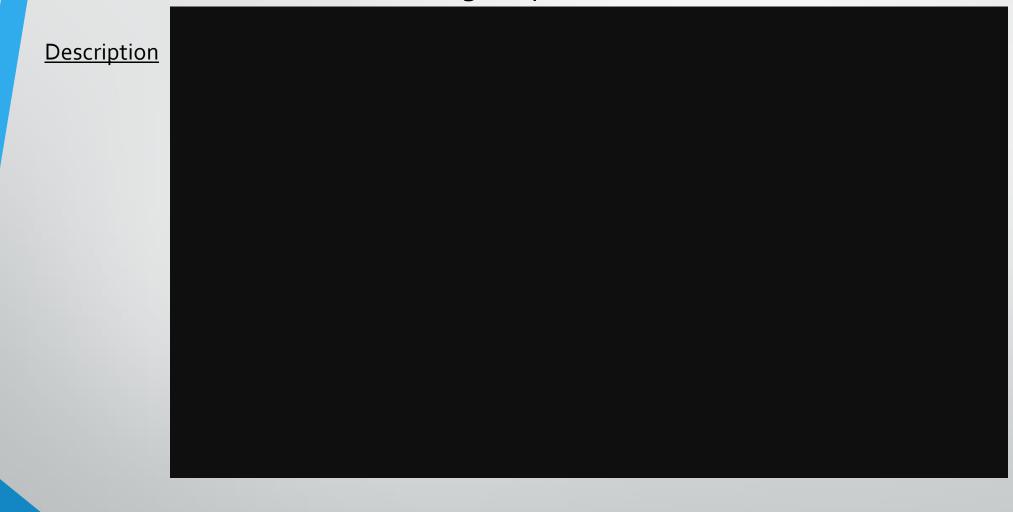
Joints (2)



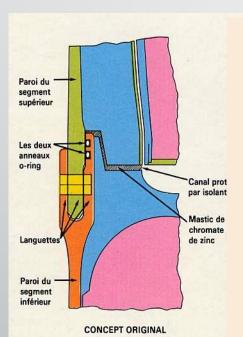




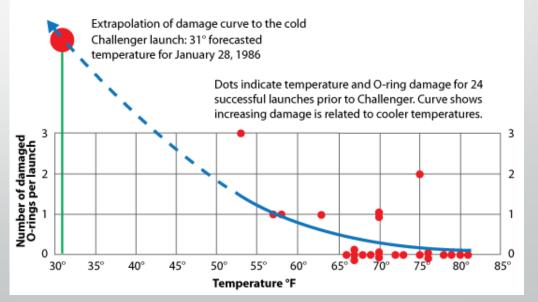
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The technical cause



At low temperatures, the elastomeric o-rings became hard, and they were sensitive to hot gas erosion. This was a known problem because it was seen on previous flights, but was considered as an acceptable risk (because of the redundancy of the secondary o-ring.) This resulted in a hot gas plume impacting the booster attachment point on the external tank, and eventually a large flame perforating the hydrogen tank wall. This caused the external tank explosion, and the vehicle breakup.



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The organizational causes

Reference : "The Challenger Launch Decision" by Diane Vaughan

- Normalization of deviance : increase of "acceptable risk" criteria : several observations of eroded orings became more and more acceptable, and the argument of the redundancy of the secondary Oring was more and more used, but wrong.
- 2. Culture of production : initially, NASA was managed by technicians, but it became more complex and bureaucratic, and the budgetary constraints transformed the organization into a production organization, with the objective to recommend launch in all cases.
- 3. Secrecy of information : the way information circulates, the processes, and the structure of regulatory relations have as a result that the information available to the top managers is filtered, and technical details, considered by engineers as "acceptable risk" were not clearly presented.

The lessons

- 1. The assessment of risks may not rely upon routine evaluations. In a production process, you may not use the argument "This has been already accepted" because other influential factors, or the environment, may have changed.
- 2. The budget scarcities, or the delay constraints, or the bureaucratic organization may not change the risk evaluation or let you use a limited rationale, not taking into account all the contributing factors.
- 3. The way information is relayed to top decision makers, and the way this information is presented (this is particularly true for statistics) must be carefully crafted, and must not deform the engineering reality.

The nozzle (theory)

<u>Objective</u> : to transform thermal energy of the gasses into kinetic energy.

Modelling of nozzle operation needs several simplifying assumptions :

- Combustion and expansion are two separate phenomena happening respectively in the combustion chamber and the nozzle.
- The expansion in the nozzle is isentropic
- The flow is one-dimensional.
- The gas kinetic energy at the entrance of the nozzle is negligible.
- The gas flow occurs without separating from the nozzle wall.
- The combustion gas is a perfect gas, and its molecular weight and γ are constant.

Nozzle theory (2)

We shall use the following variables :

- P, T and ρ : respectively pressure, temperature and density
- V : gas flow velocity
- A : cross section of the nozzle
- R : universal gas constant $r = \frac{R}{M}$
- a : the speed of sound $a = \sqrt{\gamma r T}$
- M : the Mach number $M = \frac{V}{a}$

And the following equations :

- The Mariotte law : $\frac{p}{\rho} = r.T = \frac{R.T}{\mathcal{M}}$
- The continuity equation : ρ . V. A = constant
- The energy conservation equation : $V^2 = 2. c_p. \Delta T$.
- The Mayer formula : $c_p c_v = r = \frac{R}{M}$

The nozzle theory (3)

From all the above, we can deduce :

- The Hugoniot formula : $\frac{dA}{A} = \frac{dV}{V}(M^2 1)$, showing that on a convergent-divergent nozzle :
 - The gas velocity increases continuously;
 - The gas velocity is equal to the speed of sound at the throat (M = 1)
- There is a maximum exhaust velocity, reached through isentropic expansion until absolute vacuum :

$$V_L = \sqrt{2.c_p.T_0} = \sqrt{2.\frac{\gamma}{\gamma - 1}.r.T_0}$$

• The isentropic flow allows us to write :

$$\frac{p}{p_0} = \left(\frac{T}{T_0}\right)^{\frac{\gamma}{\gamma-1}} = \left(\frac{\rho}{\rho_0}\right)^{\gamma}$$

The nozzle theory (4)

The velocity at the exit cone section can be written :

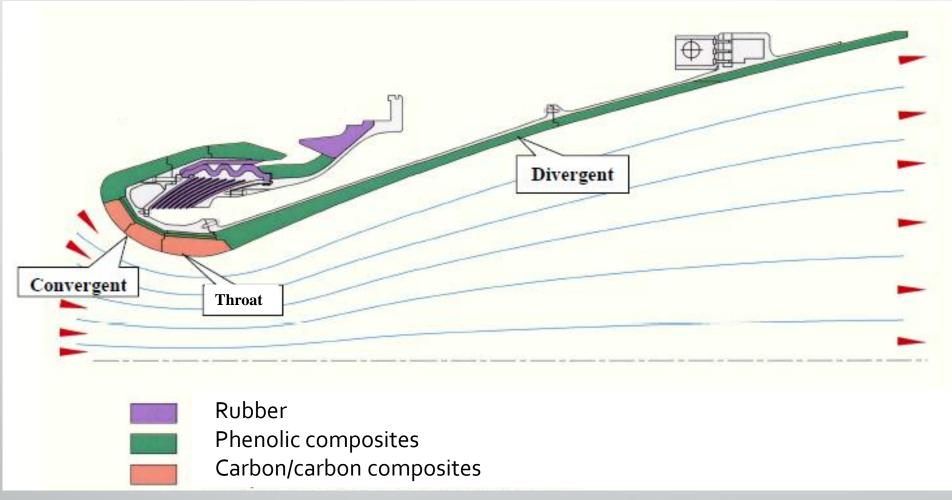
$$V_s = V_L \sqrt{1 - \left(\frac{p_s}{p_0}\right)^{\frac{\gamma-1}{\gamma}}}$$
 where $\frac{p_0}{p_s}$ is the expansion ratio.

To best see the influence of various parameters, this can be rewritten :

$$V_{S} = \sqrt{\frac{2}{\gamma - 1} \cdot \frac{R}{\mathcal{M}} T_{0} \left[1 - \left(\frac{p_{S}}{p_{0}}\right)^{\frac{\gamma - 1}{\gamma}} \right]}$$

The exhaust velocity increases with T_0 , and the expansion ratio, and when the gas molar mass decreases.

The nozzle – Example of Ariane 5 MPS



The nozzle : objectives

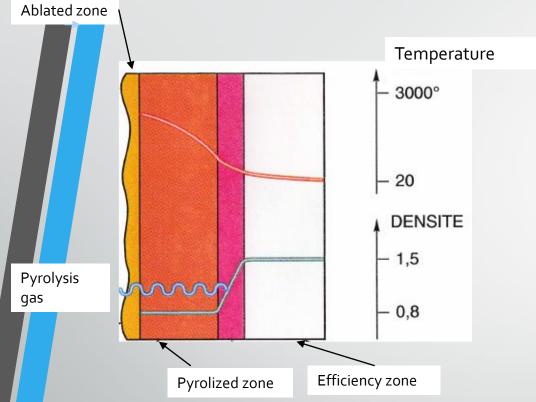
- 1. Transform the thermal energy into kinetic energy.
- 2. Give a guidance capability by allowing movement of the nozzle

Some figures for MPS nozzle :

- Mass : 6,1 tons
- Throat diameter : 900 mm
- Exit diameter : 2,9 m
- Gimbal angle : 7,1°

The design of a nozzle is very difficult : use of FE thermomechanical model, with complex phenomena like ablation (material is stripped off through action of 3000 K gas at high velocity.) Also the characterization of complex materials like carbon/carbon composites at high temperatures is very difficult. And finally, the loads are difficult to evaluate, due to the very high temperature gradients through the nozzle wall.

The nozzle : operation





The performance calculation of the motor must take into account the nozzle ablation and the corresponding diameter increase.

Piloting a launcher through nozzle orientation

To reach this objective, the nozzle must be movable in all directions, under control of two actuators positioned at 90° of each other.

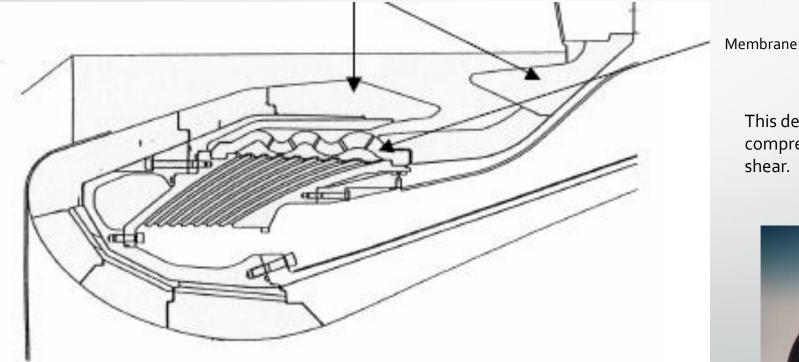
One end of each actuator is fixed on the nozzle, the other end on the stage structure.

Therefore, there must be a flexible object between the nozzle and the stage : on the MPS, it is the flex seal.



The flex seal

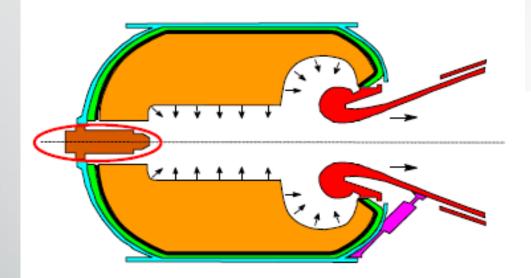
It is composed of alternating spherical layers of steel and rubber. The rubber must remain in compression under all loads. The flex seal must be protected from the hot gasses by a membrane.

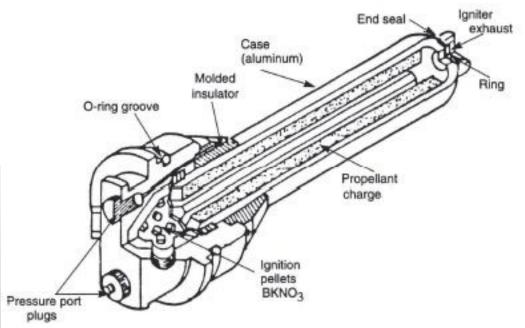


This design allows high stiffness in compression, but low stiffness in shear.



The ignition system



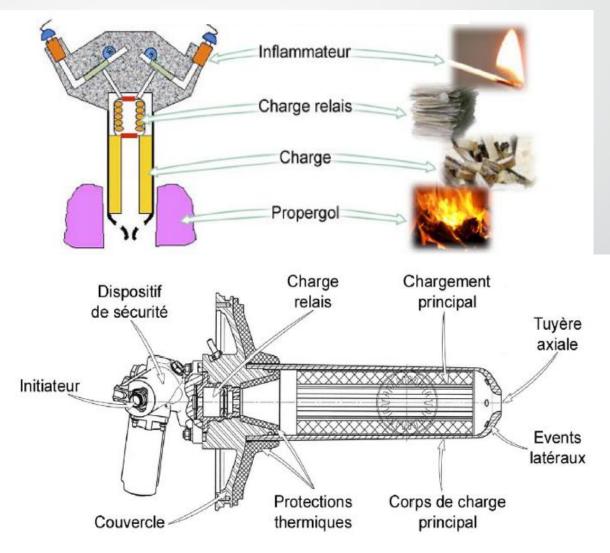


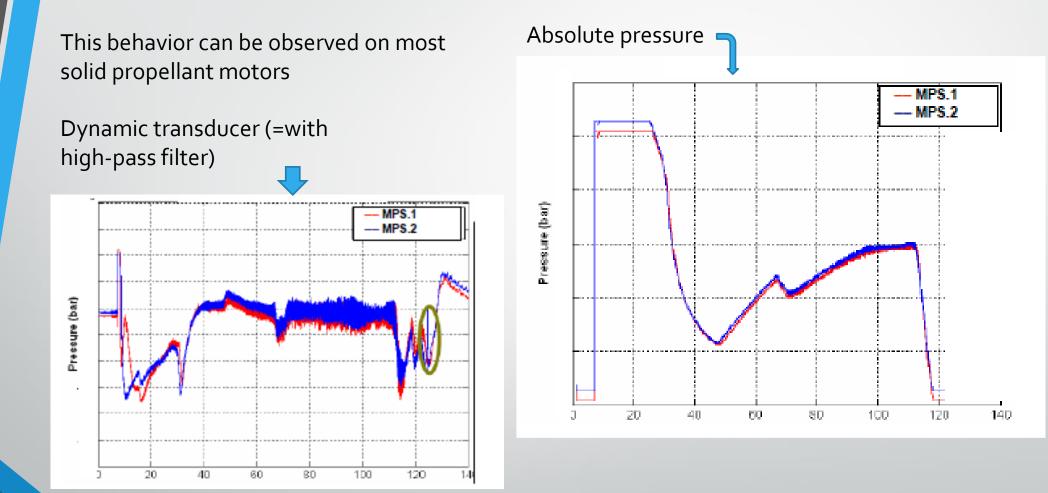
The ignition system

It is essentially a small solid propellant motor whose objective is to send hot gas and particles onto the motor propellant grain to ignite it. On the Ariane 5 EAP, it is a 3-stage

ignition system :

- A pyrotechnic ignition system made of BKNO₃ pellets.
- 2. A relay charge
- 3. The main charge.





These oscillations are of a few tenths of % in pressure, but of few % in thrust. This amounts to several kN ! The frequency of one of the modes can dangerously approach the structural resonant modes of the stage or the launcher, and possibly cause damage to the payloads !

This phenomenon has been actively investigated since the years 1970 : the origin is now understood : it comes from the interaction of vortices at the nozzle entrance and the acoustical cavity formed by the last segment of the booster.

The last segment is a hollow cylinder which has an acoustic longitudinal resonant frequency which varies slowly with time.

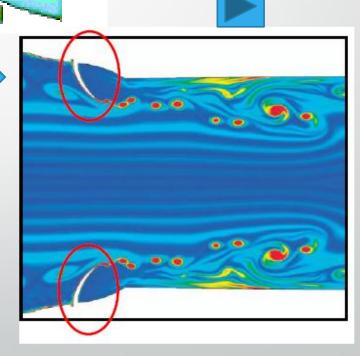
Vortices are created in the gas flow according to several phenomena.

1. Parietal vortices (created by the interaction of turbulent flow along the wall)

2. Obstacles vortices (created by inhibitor rings)

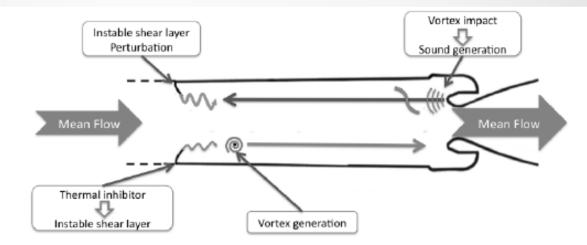
3. Discontinuity vortices (geometry of propellant grain)

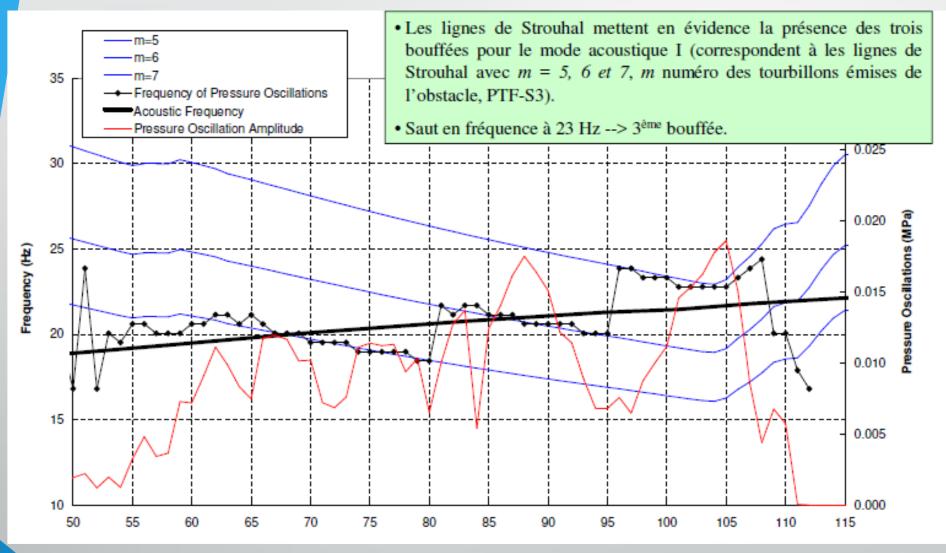




The frequency of these vortex shedding is characterized by a dimensionless number called Strouhal number : $St = \frac{f L}{U}$, where L is a characteristic length, f the frequency of the vortex shedding, and U is the flow velocity.

The pressure oscillations created by the vortices create a coupling with the combustion velocity, which resonates for certain frequencies corresponding to specific Strouhal numbers



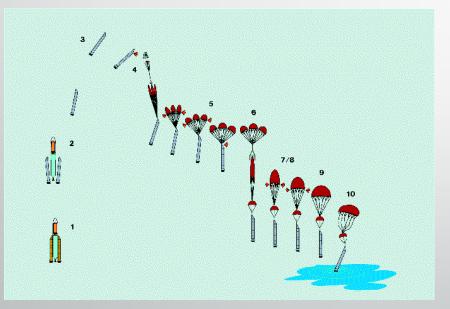


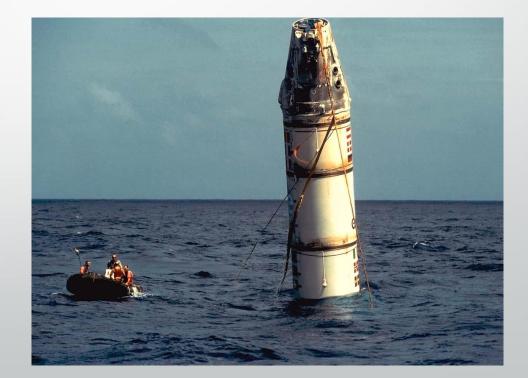
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Solid propellant stage qualification

 Through a qualification flight and, if possible, recovery. On Ariane 5, there are only a few (20) telemetry sensors, not sufficient to evaluate the correct operation of the whole EAP stage. For qualification flights, specific transducers have been added.

The recovery was made on a few stages, but needed a complex parachute system.





Solid propellant stage qualification

 Through a firing test on the ground Necessitates a specific firing test bench, and an additional operational stage, unusable to launch a satellite !

But : it eliminates the reentry damage, and allows much more measurements (in theory, no limit in the ground telemetry system), and can later be used for production improvements qualification.



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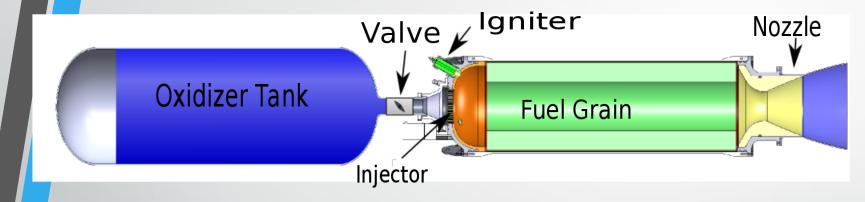


P120C firing test



Hybrid propulsion

This type of rocket engine uses liquid oxygen or nitrous oxide as oxidizer.



The main advantage of hybrid propulsion is that the propellant burn rate is driven by the oxidizer flow rate, and is therefore independent of defects in the propellant grain like cracks, debonding. It is also safer to handle and manufacture, is controllable, and has a higher Isp than solid propulsion.

Hybrid propulsion



That is why this type of propulsion is used on a commercial human space flight project : SpaceShip One and Two, by the companies Scaled Composites and Virgin Galactic.

SpaceShip Two was destroyed in flight due to premature aerodynamic brake deployment.



Thank you for your attention !