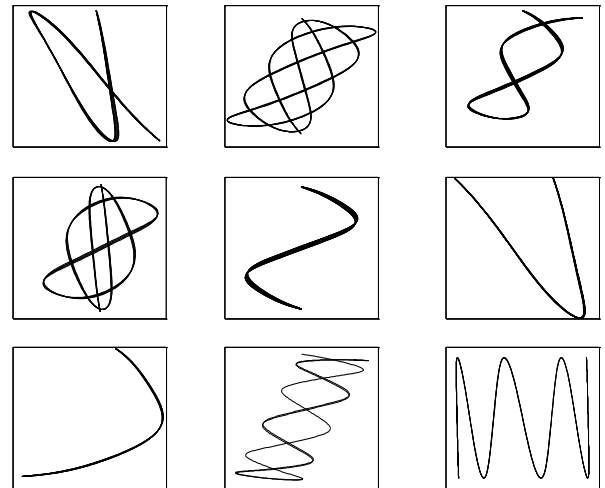


Nonlinear Vibrations of Aerospace Structures

L04 Modal analysis

Unforced dynamics
(2DOF)



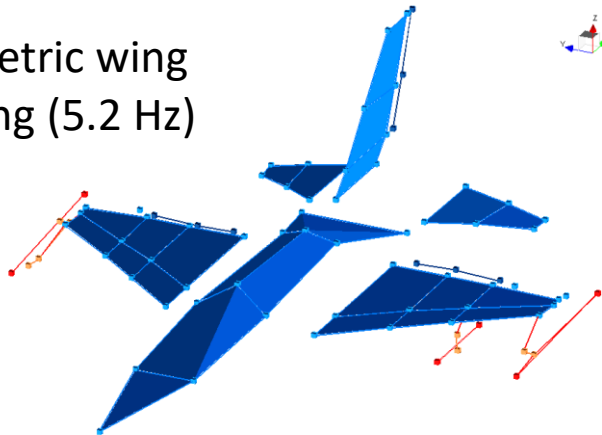
Modes correspond to the deformation at resonance



Modal analysis provides key information

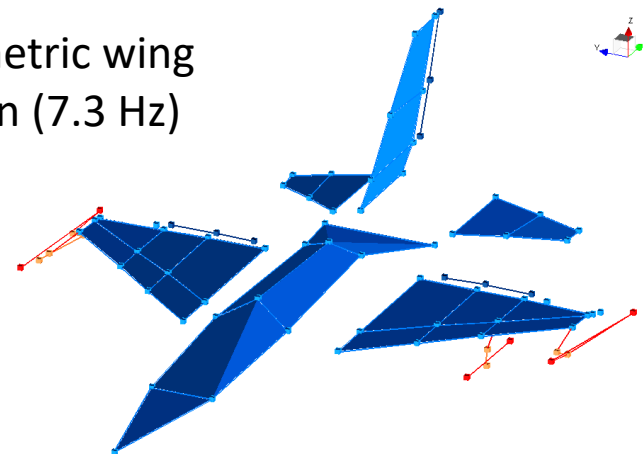


Symmetric wing bending (5.2 Hz)



Mode 3: 4.8665 Hz, 0.66 % Low level (80)

Symmetric wing torsion (7.3 Hz)



Mode 5: 7.0303 Hz, 0.58 % Low level (80)

What is a linear normal mode ?

2.2. Modes normaux de vibration

Pour résoudre les équations des petites oscillations libres (2.1.12)

$$M\ddot{\mathbf{q}} + K\mathbf{q} = 0$$

cherchons une solution particulière dans laquelle toutes les coordonnées généralisées suivent, à un facteur près, la même loi temporelle

$$\mathbf{q} = \mathbf{x} \phi(t) \quad (2.2.1)$$

où \mathbf{x} est un vecteur de constantes constituant *la forme propre du mouvement*, propre dans ce sens que le rapport de deux coordonnées est indépendant du temps et est toujours égal au rapport des éléments correspondants de \mathbf{x} . L'essai d'une solution de ce type fournit

$$\ddot{\phi}(t)M\mathbf{x} + \phi(t)K\mathbf{x} = 0 \quad (2.2.2)$$

How do we calculate linear normal modes ?

$$\ddot{q}_1 + (2q_1 - q_2) = 0$$

$$\ddot{q}_2 + (2q_2 - q_1) = 0$$

How do we calculate linear normal modes ?

$$q_{1,2} = A, B \cos \omega t$$

$$\ddot{q}_1 + (2q_1 - q_2) = 0$$

$$\ddot{q}_2 + (2q_2 - q_1) = 0$$

$$-\omega^2 A + 2A - B = 0$$

$$-\omega^2 B + 2B - A = 0$$

$$-\omega^2 A(2 - \omega^2) + 2A(2 - \omega^2) - A = 0$$

$$B = A(2 - \omega^2)$$
$$-\omega^2 B + 2B - A = 0$$

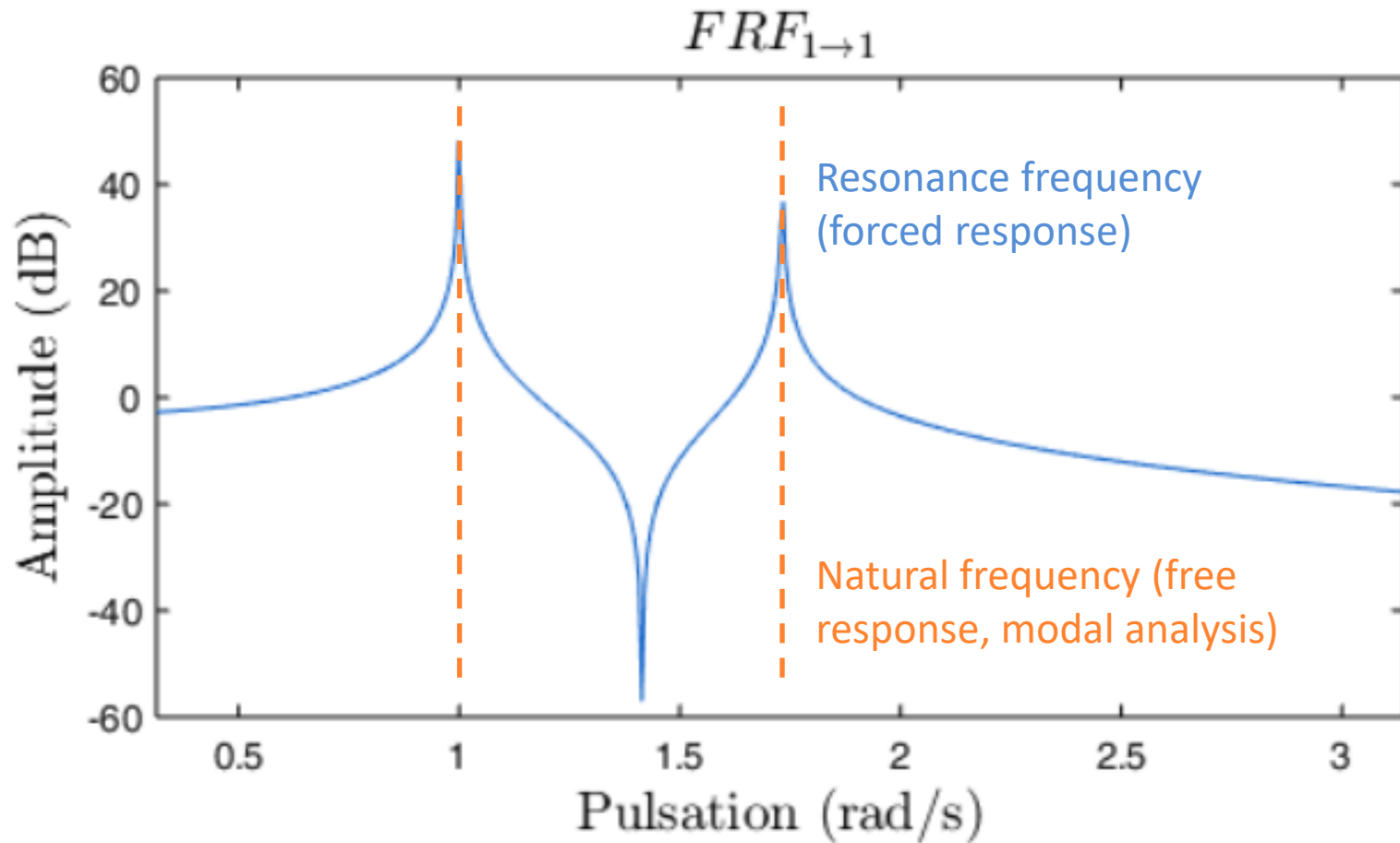
$$\omega^4 - 4\omega^2 + 3 = 0$$

$$\omega_1 = 1 \text{ rad/s with } A = B,$$

$$\omega_2 = \sqrt{3} \text{ rad/s with } A = -B,$$

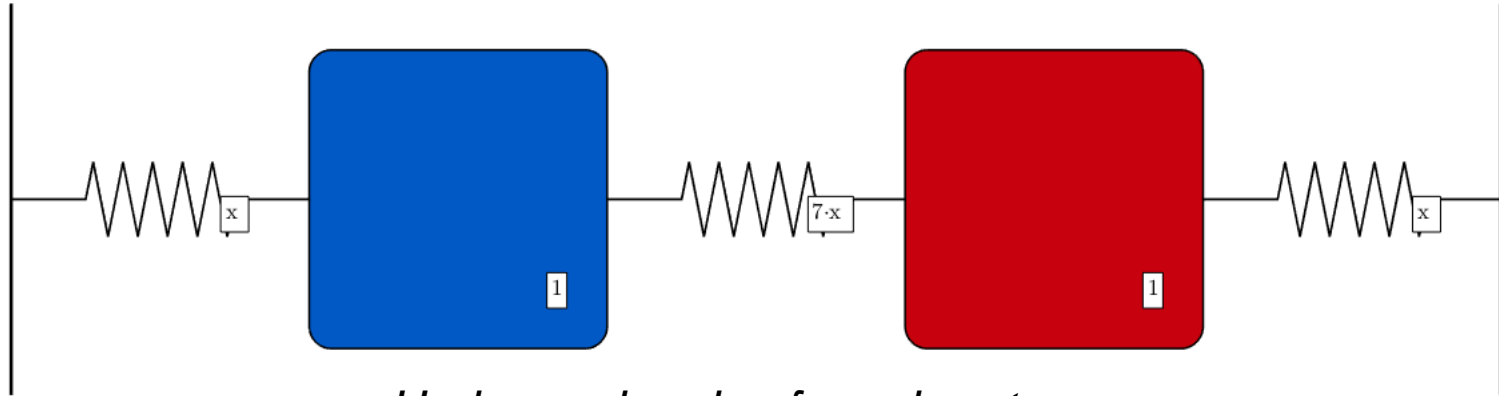
Linear modes are invariant

Link between natural and resonance frequencies

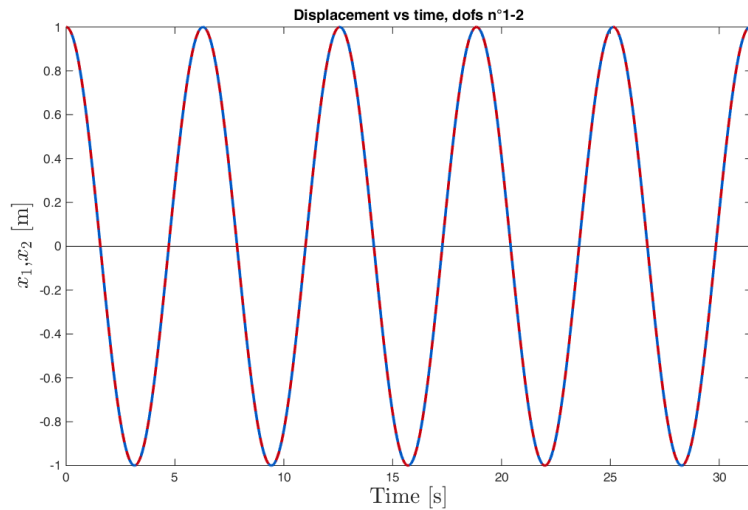


A linear mode is a time-periodic motion

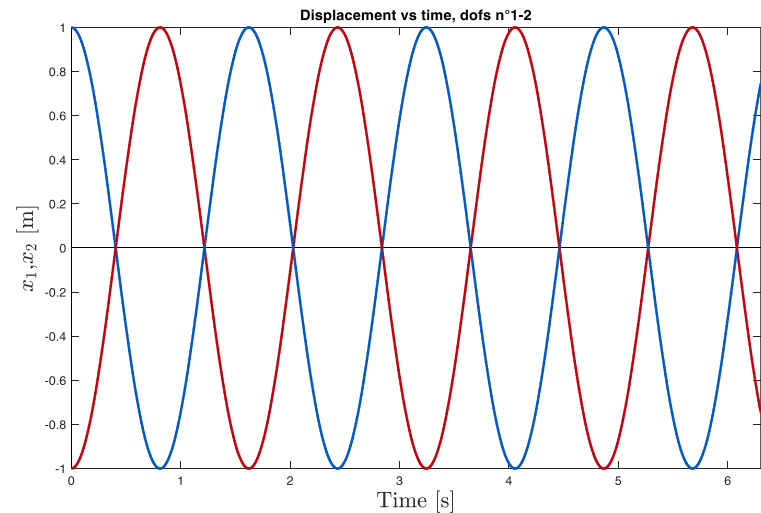
NI2D – 2DOF\Modes_Linear



Undamped and unforced system

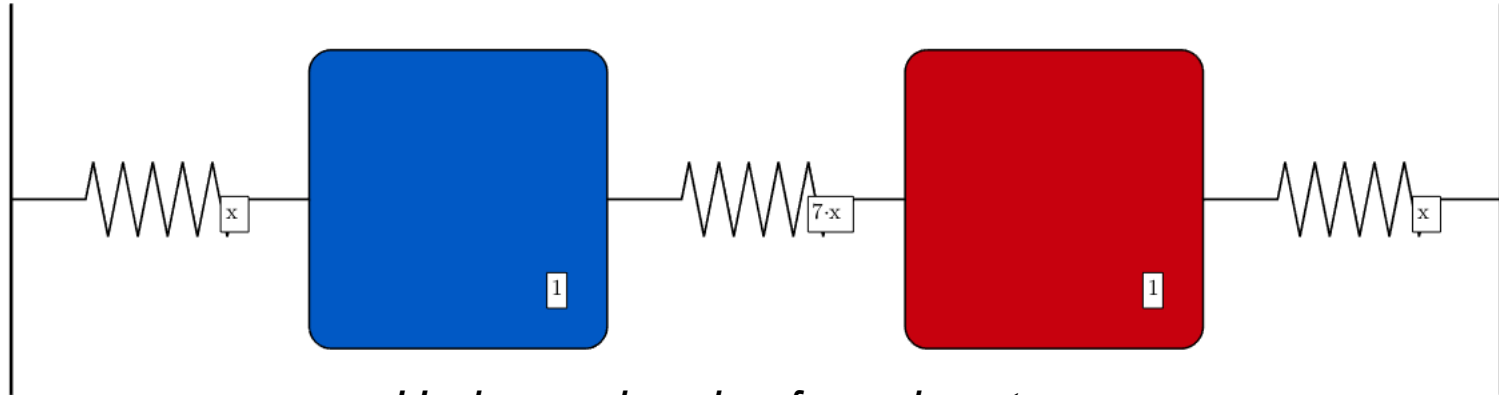


IN-PHASE MODE

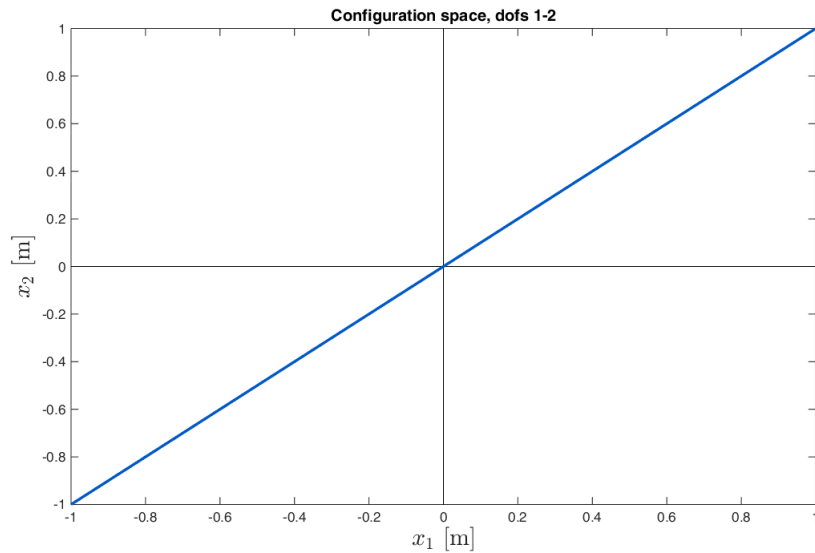


OUT-OF-PHASE MODE

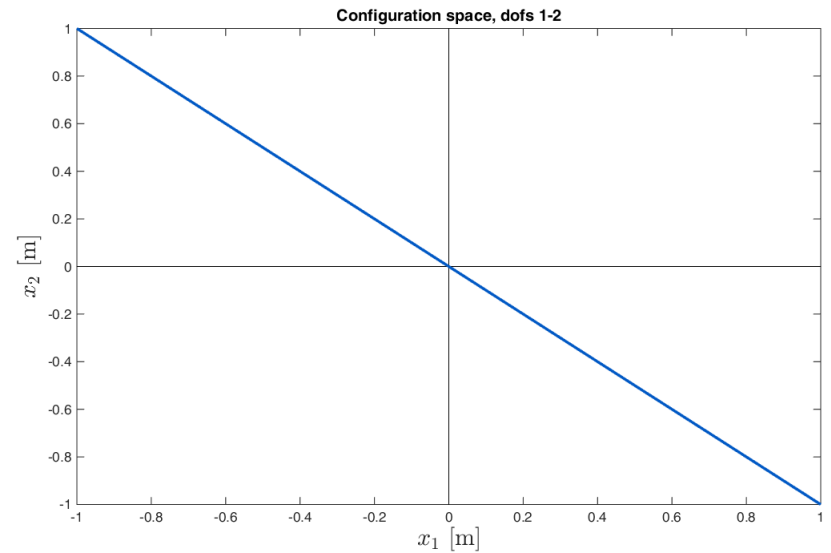
It is also a straight line in displacement space



Undamped and unforced system

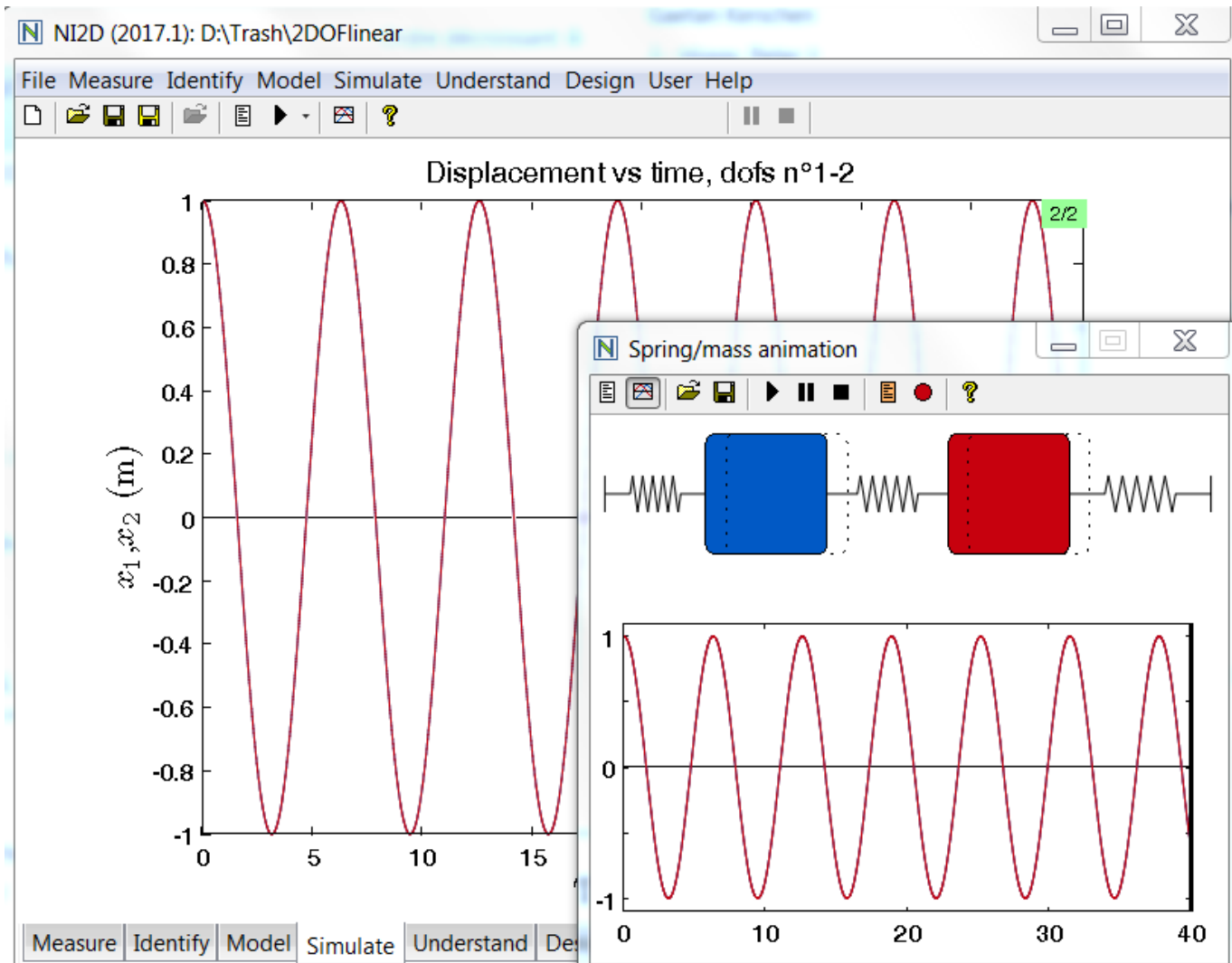


IN-PHASE MODE



OUT-OF-PHASE MODE

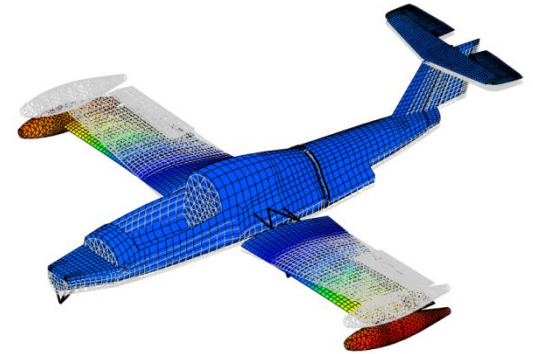
Animation



In summary

Clear physical meaning:

- ▶ Structural deformation at resonance
- ▶ Synchronous vibration of the structure



Important mathematical properties:

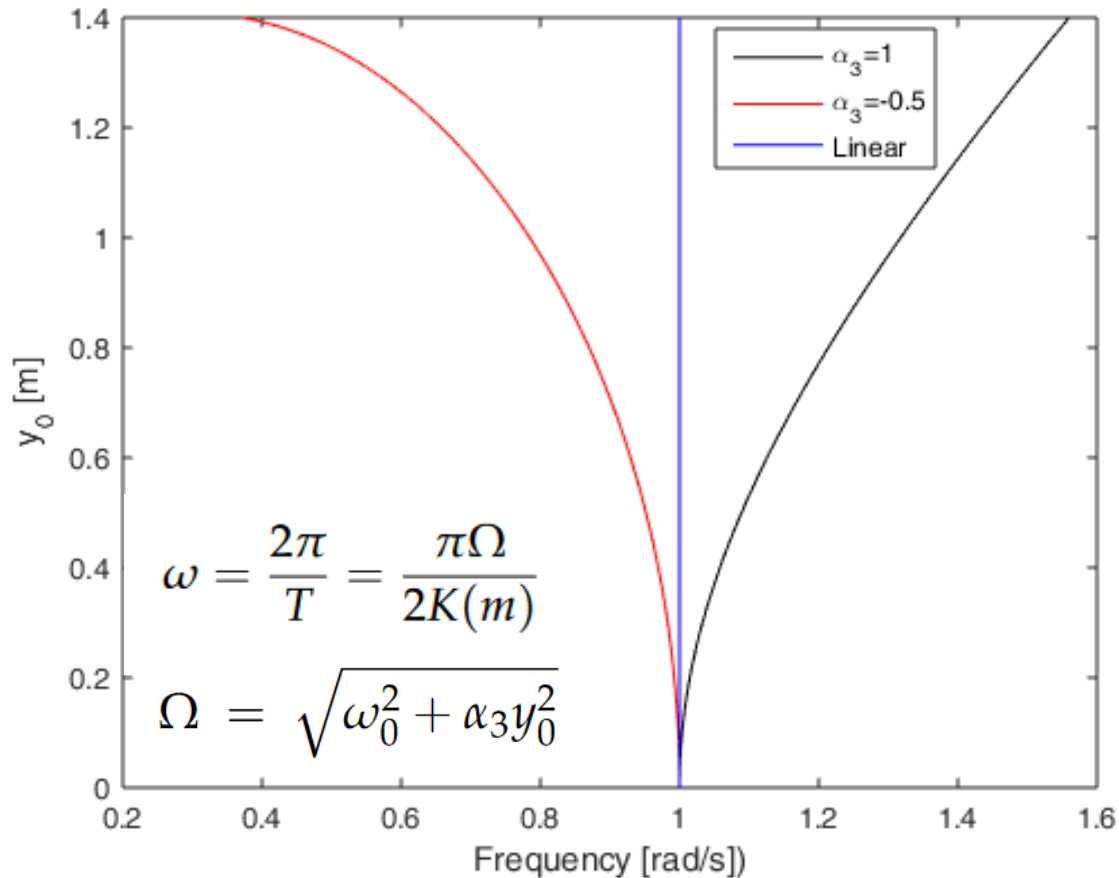
- ▶ Orthogonality
- ▶ Decoupling of the equations of motion (modal superposition)

Outline of this lecture

What are nonlinear modes ?

What are their fundamental properties ?

The 1DOF case

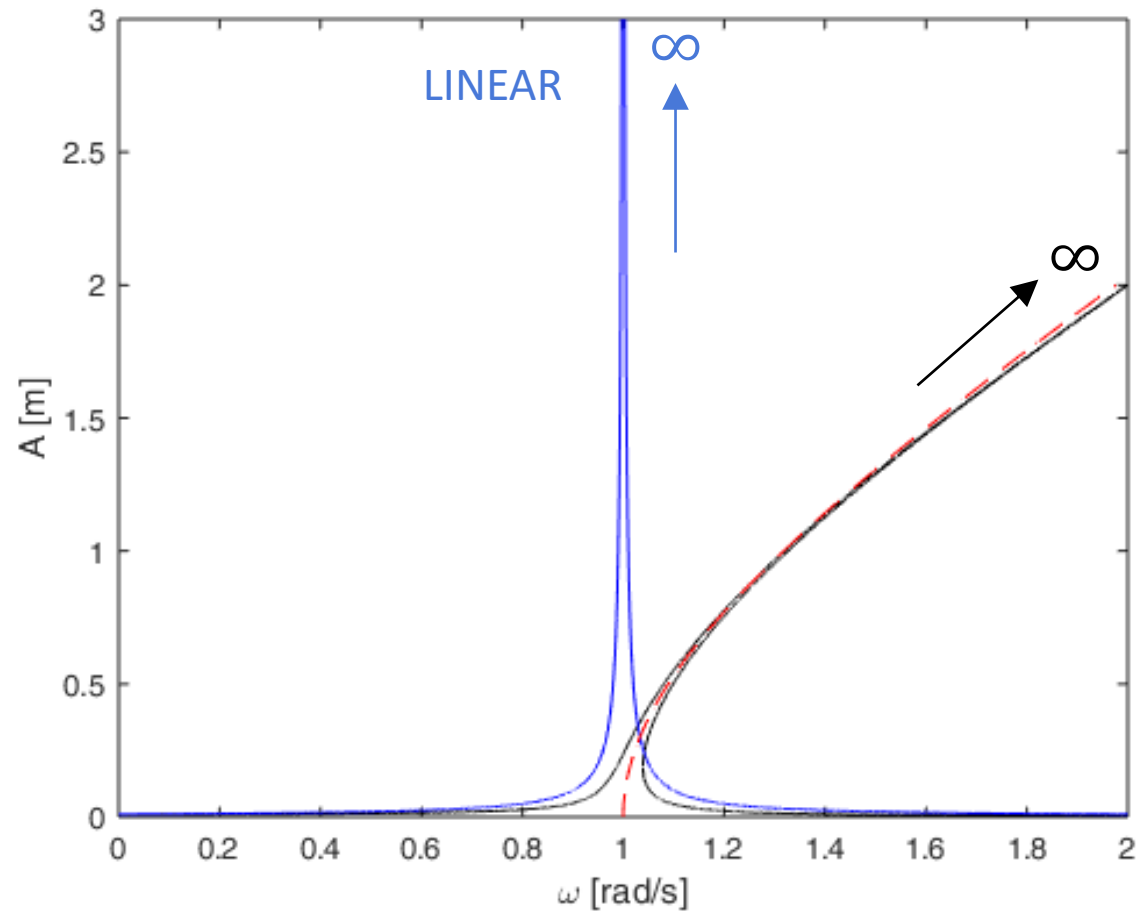


This highlights the frequency-amplitude dependence of nonlinear oscillations

Very important concept: the backbone curve

The 1DOF case

$$\ddot{y}(t) + y(t) + y^3(t) = 0.01 \sin \omega t$$



The MDOF case: nonlinear normal modes

Definition due to Rosenberg (1960), couldn't be simpler !

$$M\ddot{x}(t) + Kx(t) = 0$$

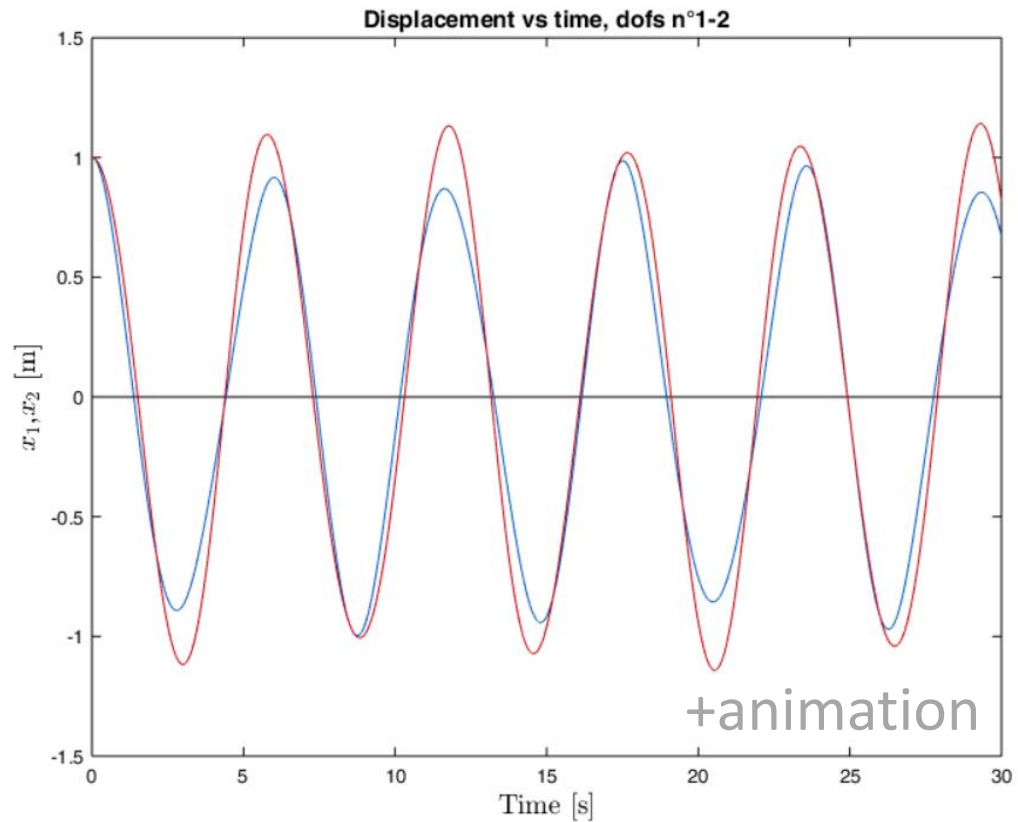
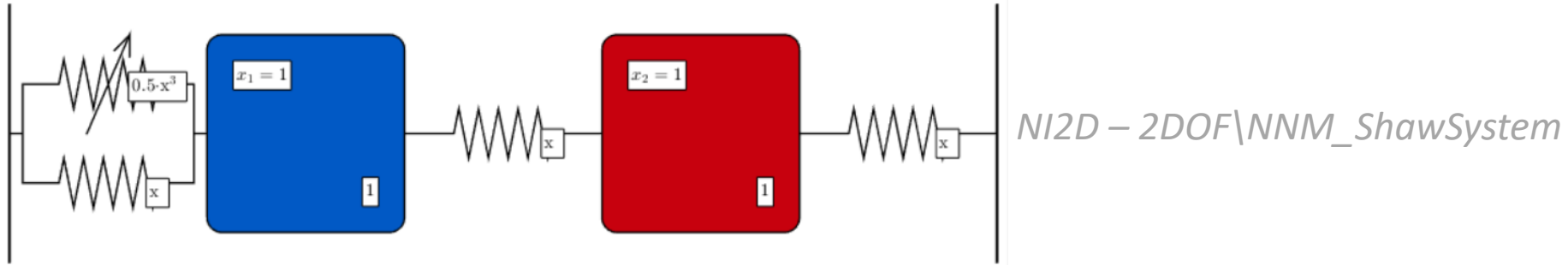
$$M\ddot{x}(t) + Kx(t) + f_{NL}[x(t)] = 0$$

LNM: periodic
motion.

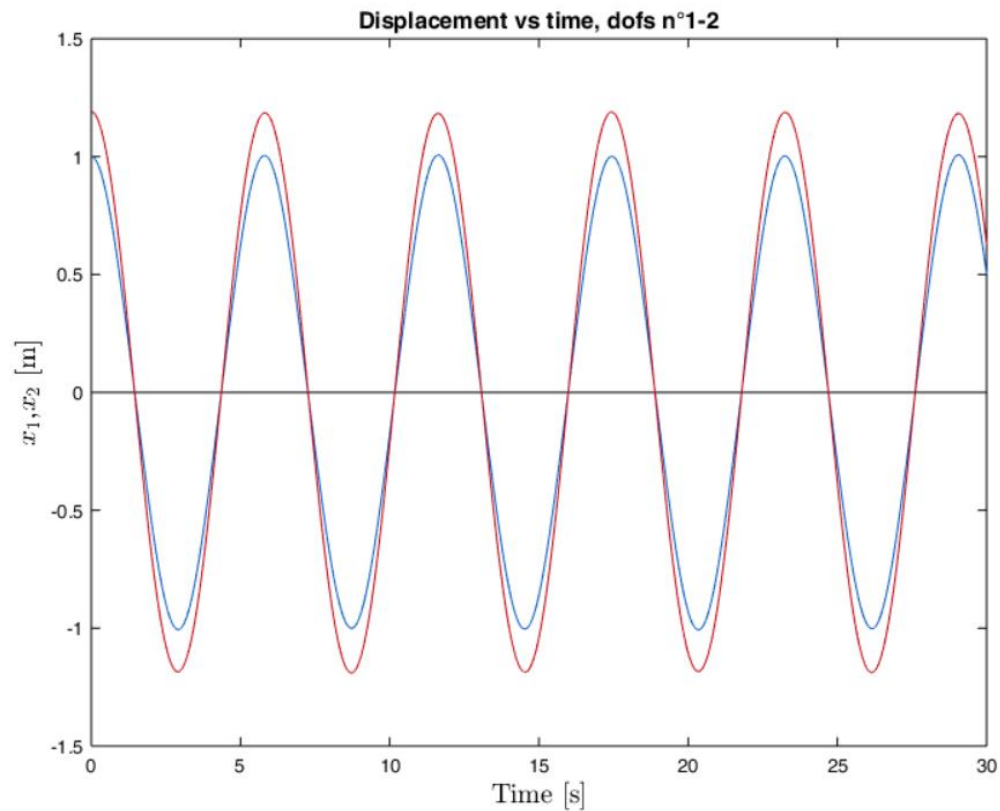
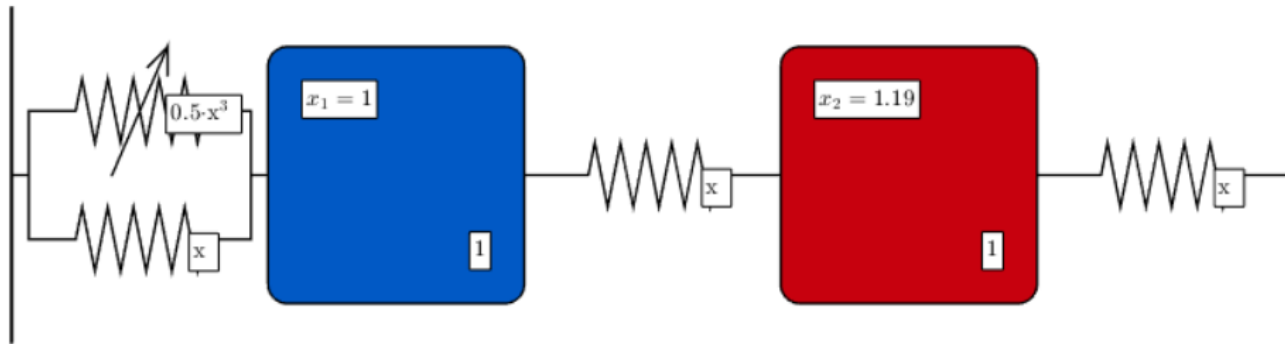


NNM: periodic
motion.

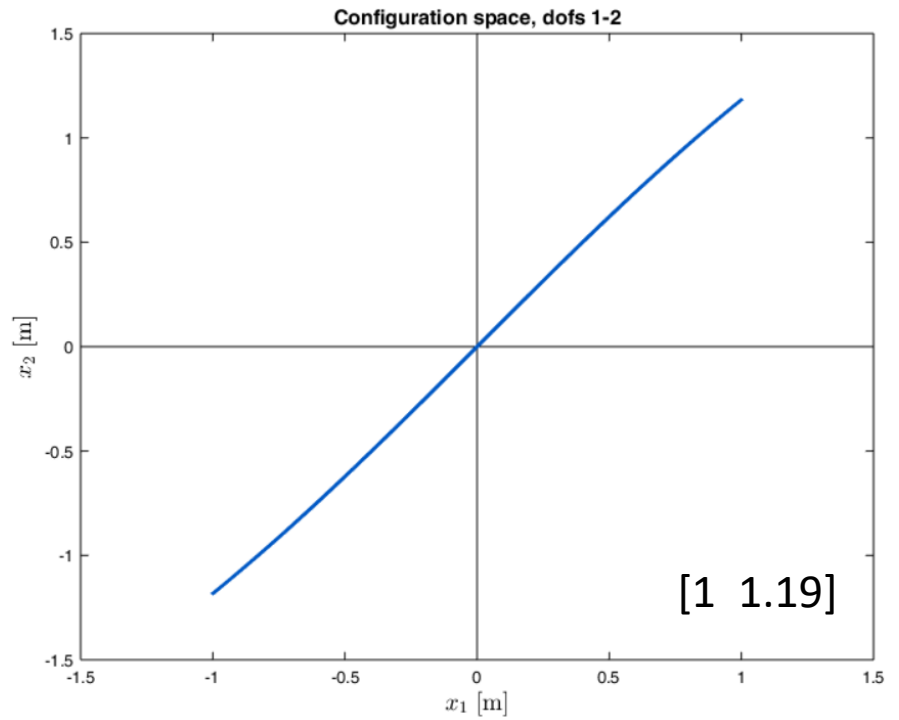
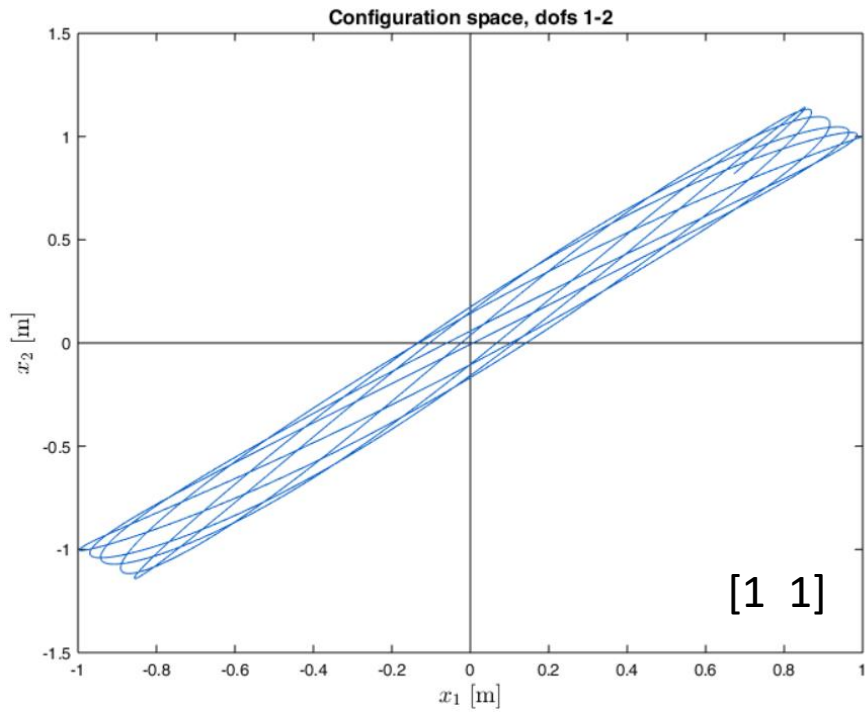
Is this a nonlinear mode ?



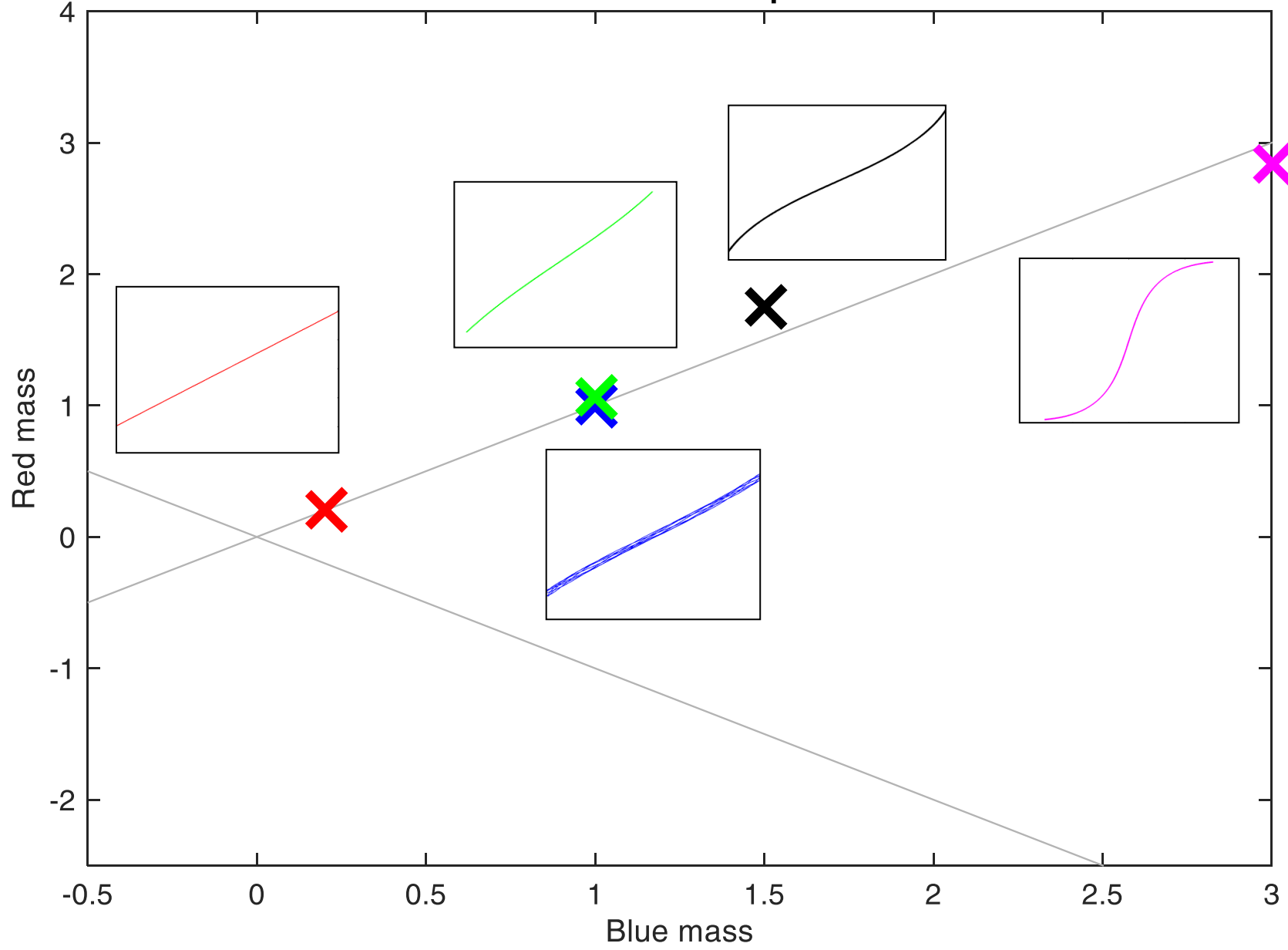
Is this a nonlinear mode ?



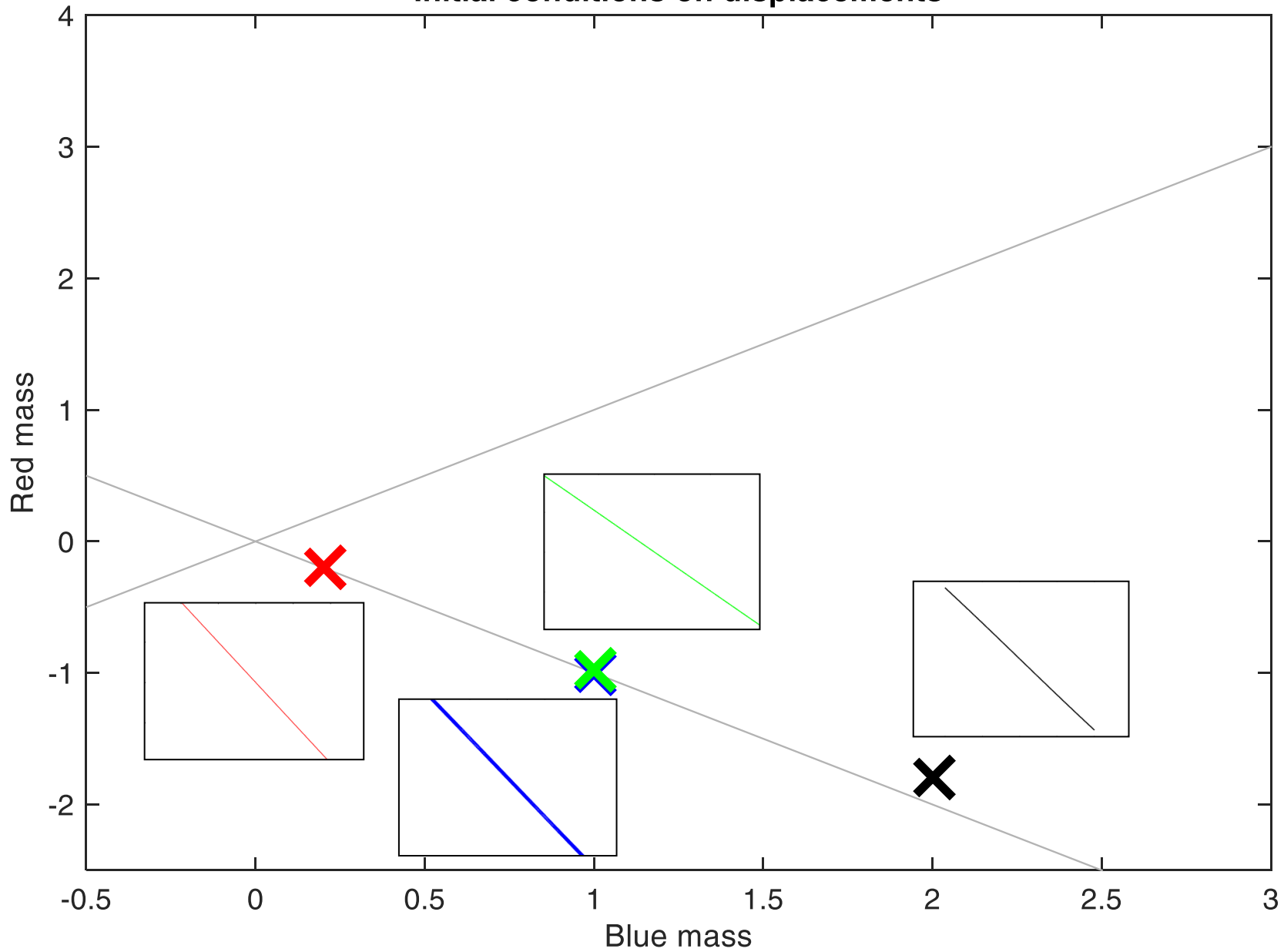
Is this a nonlinear mode ?



Initial conditions on displacements



Initial conditions on displacements



The 2DOF example

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) + 0.5q_1^3 &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

How do we calculate nonlinear modes ?

Assumption of harmonic motion: $q_{1,2} \cong A, B \cos \omega t$

The 1-term harmonic balance method

$$\cos 3\theta = 4\cos^3\theta - 3\cos\theta$$

$$\Rightarrow \cos^3\theta = \frac{1}{4}(\cos 3\theta + 3\cos\theta)$$

$$\ddot{q}_2 + 2q_2 - q_2 + \frac{1}{2}q_2^3 = 0 \rightarrow -\omega^2 A + 2A - B + \frac{3}{8}A^3 = 0 \quad (1)$$

$$\ddot{q}_1 + 2q_1 - q_1 = 0 \rightarrow -\omega^2 B + 2B - A = 0 \rightarrow \boxed{B = \frac{A}{2-\omega^2}} \quad (2)$$

$$(1) \& (2) \Rightarrow -\omega^2 A + 2A - \frac{A}{2-\omega^2} + \frac{3}{8}A^3 = 0$$

$$\Rightarrow -\omega^2 + 2 - \frac{1}{2-\omega^2} + \frac{3}{8}A^2 = 0$$

$$\Rightarrow -2\omega^2 + \omega^4 + 4 - 2\omega^2 - 1 + \frac{3}{8}A^2 - \frac{3}{8}A^2\omega^2 = 0$$

$$\Rightarrow A^2 \left(\frac{3}{4} - \frac{3}{8}\omega^2 \right) = -\omega^4 + 4\omega^2 - 3$$

$$\Rightarrow \boxed{A = \pm \sqrt{\frac{8(\omega^2-1)(\omega^2-3)}{3(\omega^2-2)}}$$

Fundamental difference between LNMs and NNMs

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

▼ $q_{1,2} = A, B \cos \omega t$

$$A = B, \quad \omega_1 = 1 \text{ rad/s}$$

$$A = -B, \quad \omega_2 = \sqrt{3} \text{ rad/s}$$

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) + 0.5q_1^3 &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

▼ $q_{1,2} \cong A, B \cos \omega t$

$$A = \pm \sqrt{\frac{8(\omega^2 - 3)(\omega^2 - 1)}{3(\omega^2 - 2)}}$$

$$B = \frac{A}{2 - \omega^2}$$

What do you observe ?

Fundamental difference between LNMs and NNMs

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

▼ $q_{1,2} = A, B \cos \omega t$

$$A = B, \quad \omega_1 = 1 \text{ rad/s}$$

$$A = -B, \quad \omega_2 = \sqrt{3} \text{ rad/s}$$

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) + 0.5q_1^3 &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

▼ $q_{1,2} \cong A, B \cos \omega t$

$$A = \pm \sqrt{\frac{8(\omega^2 - 3)(\omega^2 - 1)}{3(\omega^2 - 2)}}$$
$$B = \frac{A}{2 - \omega^2}$$

Modal shapes depend on frequency

Fundamental difference between LNMs and NNMs

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

▼ $q_{1,2} = A, B \cos \omega t$

$$A = B, \quad \omega_1 = 1 \text{ rad/s}$$

$$A = -B, \quad \omega_2 = \sqrt{3} \text{ rad/s}$$

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) + 0.5q_1^3 &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

▼ $q_{1,2} \cong A, B \cos \omega t$

$$A = \pm \sqrt{\frac{8(\omega^2 - 3)(\omega^2 - 1)}{3(\omega^2 - 2)}}$$

$$B = \frac{A}{2 - \omega^2}$$

The natural frequency
changes
(but existence conditions !)

Fundamental difference between LNMs and NNMs

$$\ddot{q}_1 + (2q_1 - q_2) = 0$$

$$\ddot{q}_2 + (2q_2 - q_1) = 0$$

▼ $q_{1,2} = A, B \cos \omega t$

$$A = B, \quad \omega_1 = 1 \text{ rad/s}$$

$$A = -B, \quad \omega_2 = \sqrt{3} \text{ rad/s}$$

$$\ddot{q}_1 + (2q_1 - q_2) + 0.5q_1^3 = 0$$

$$\ddot{q}_2 + (2q_2 - q_1) = 0$$

▼ $q_{1,2} \cong A, B \cos \omega t$

$$A = \pm \sqrt{\frac{8(\omega^2 - 3)(\omega^2 - 1)}{3(\omega^2 - 2)}}$$

$$B = \frac{A}{2 - \omega^2}$$

$$\omega_1 \in [1, \sqrt{2} [\text{ rad/s}$$

$$\omega_2 \in [\sqrt{3}, +\infty [\text{ rad/s}$$

Existence conditions for NNM

1. Frequency-energy dependence

Useful graphical representation

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) + 0.5q_1^3 &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

Initial conditions: $[q_1(0) \quad q_2(0) \quad \dot{q}_1(0) \quad \dot{q}_2(0)] = [A \quad B \quad 0 \quad 0]$

Total energy =
initial potential energy : $E = V = \frac{A^2}{2} + \frac{(B - A)^2}{2} + \frac{B^2}{2} + \frac{0.5A^4}{4}$



A frequency-energy plot is calculated by

- Selecting a frequency in the interval provided by the existence conditions,
- Calculating A and B according to the analytical formulas
- Calculating the corresponding total energy
- Representing the frequency as a function of the total energy

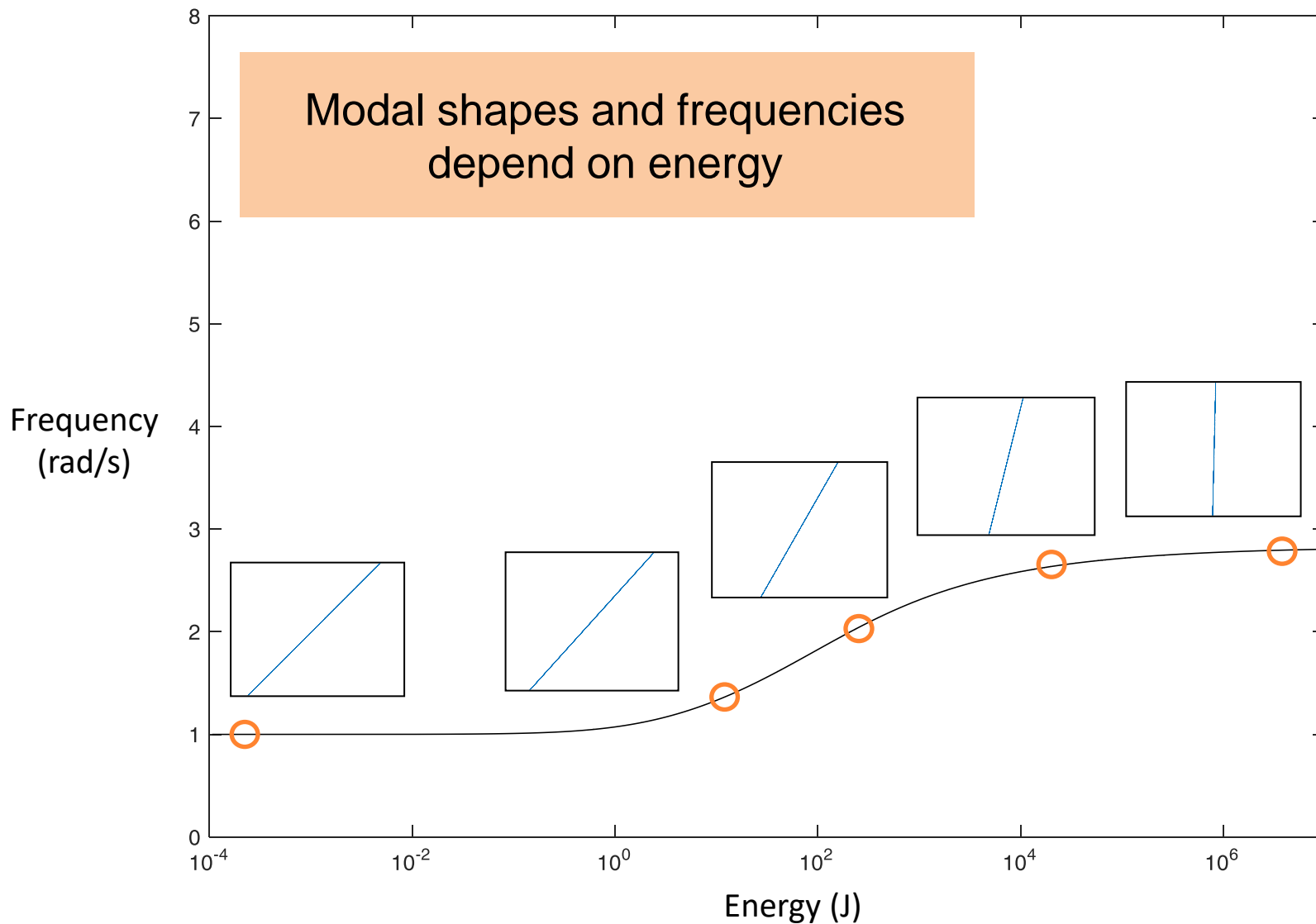
In Matlab

```
HB1_2DOF_FEP.m x +
clear all
close all

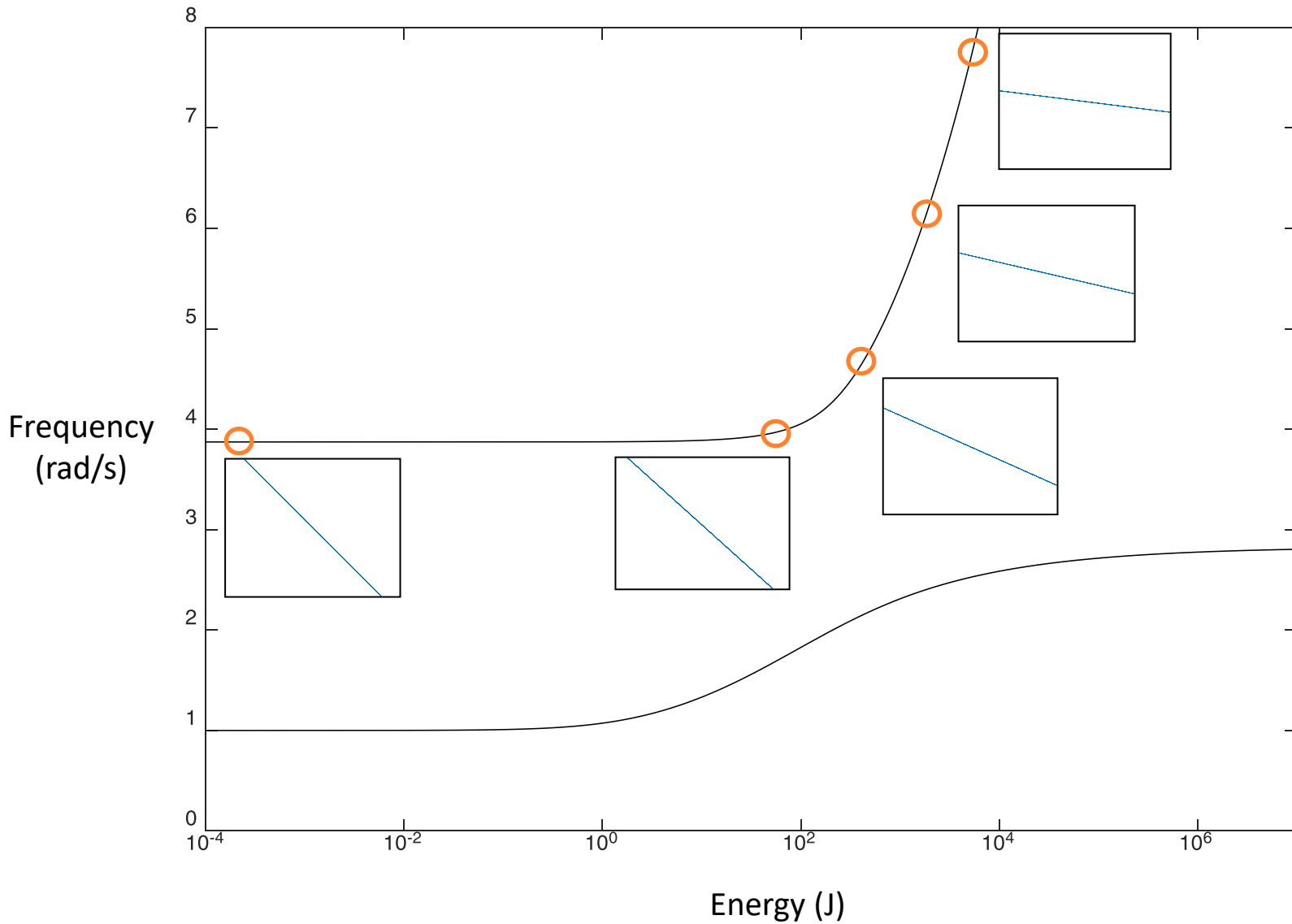
cpt=1;
for omeg=1.00001:0.001:sqrt(2)
    A=sqrt(8*(omeg^2-3)*(omeg^2-1)/3/((omeg^2-2)));
    B=A/(2-omeg^2);
    NRJ(cpt)=(A-B)^2/2+A^2/2+B^2/2+0.5*A^4/4;
    freq(cpt)=omeg;
    AIP(cpt)=A;
    BIP(cpt)=B;
    cpt=cpt+1;
end
semilogx(NRJ,freq,'k')

cpt=1;
for omeg=sqrt(3)+0.0000001:0.001:4
    A=sqrt(8*(omeg^2-3)*(omeg^2-1)/3/((omeg^2-2)));
    B=A/(2-omeg^2);
    NRJ2(cpt)=(A-B)^2/2+A^2/2+B^2/2+0.5*A^4/4;
    freq2(cpt)=omeg;
    AOP(cpt)=A;
    BOP(cpt)=B;
    cpt=cpt+1;
end
hold on
semilogx(NRJ2,freq2,'k')
```

The in-phase NNM in the FEP



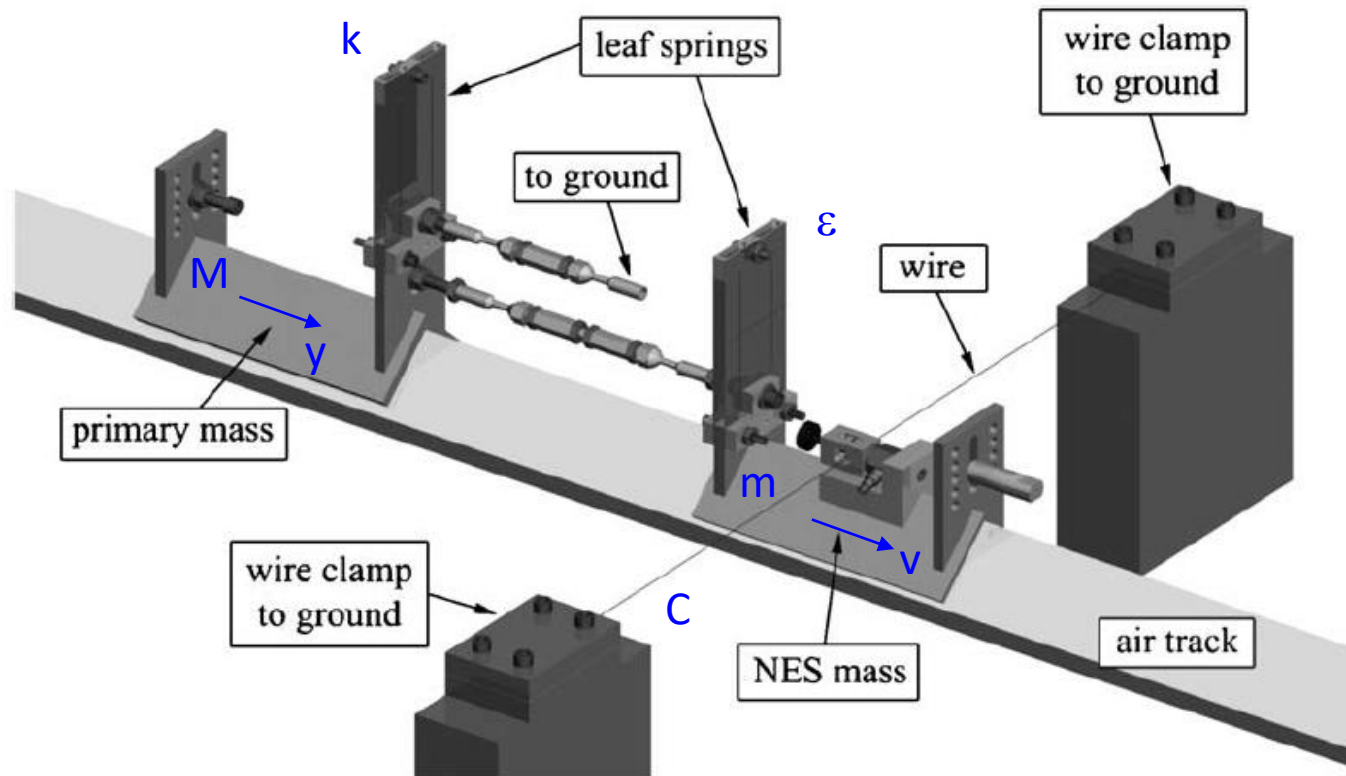
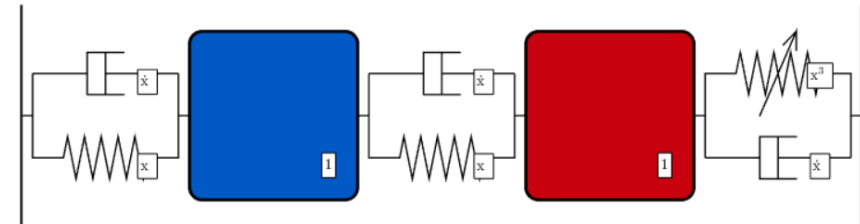
The out-of-phase NNM in the FEP



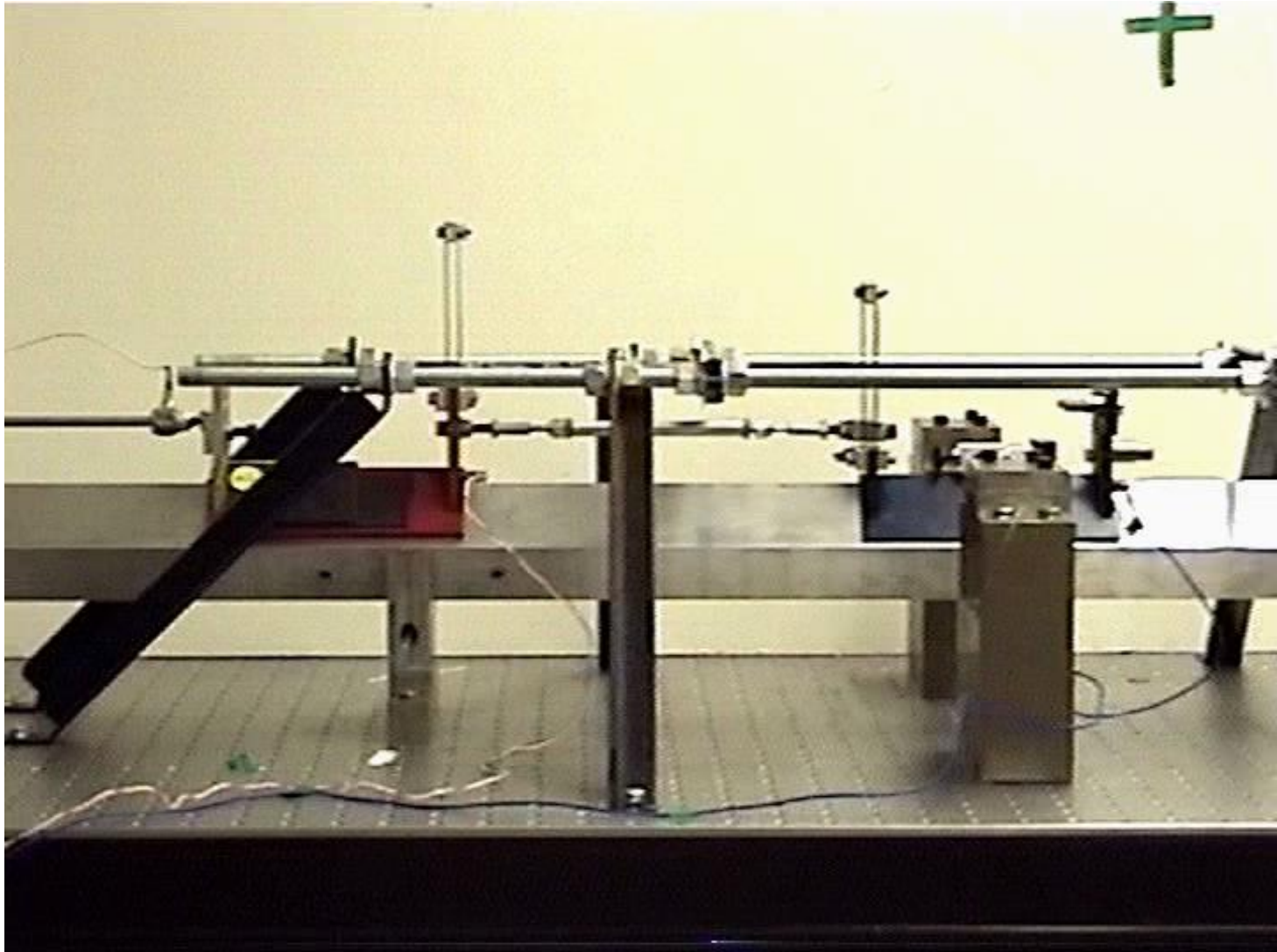
Experimental evidence of frequency-energy dependence

$$M\ddot{y} + \epsilon\lambda_1\dot{y} + \epsilon\lambda(\dot{y} - \dot{v}) + \epsilon(y - v) + ky = 0$$

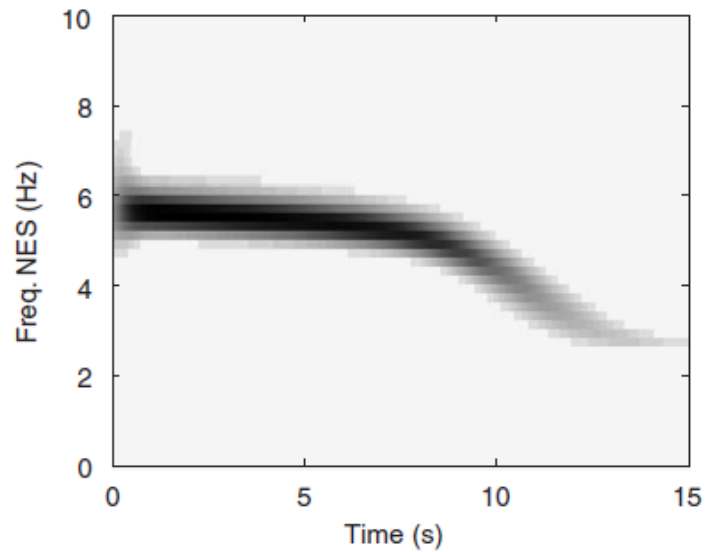
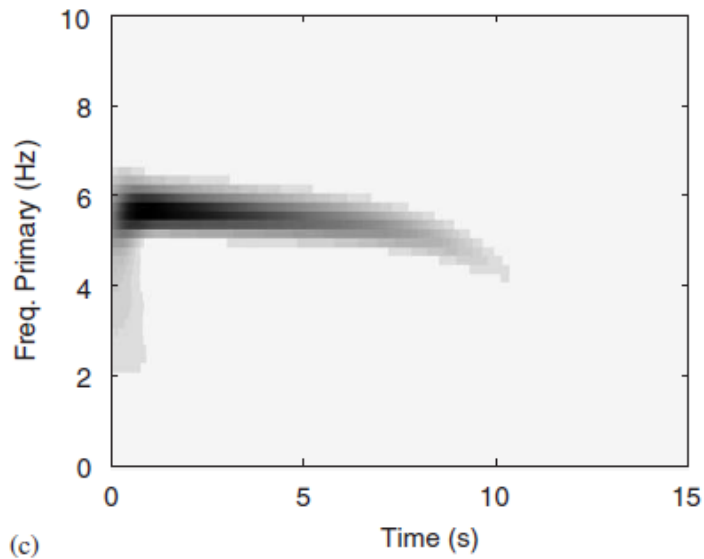
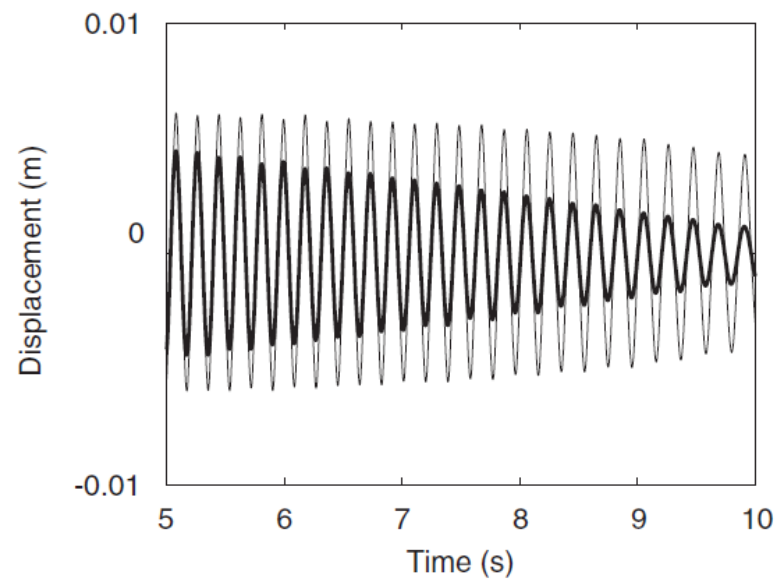
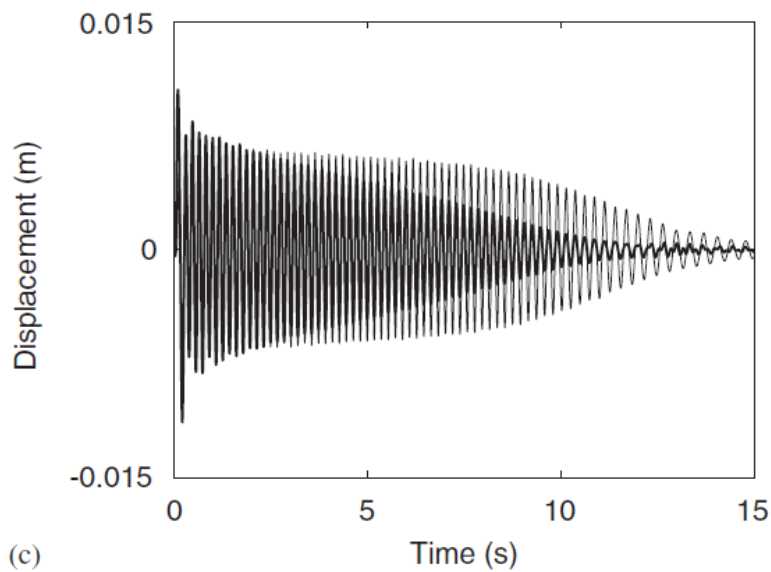
$$m\ddot{v} + \epsilon\lambda_2\dot{v} + \epsilon\lambda(\dot{v} - \dot{y}) + \epsilon(v - y) + Cv^3 = 0$$



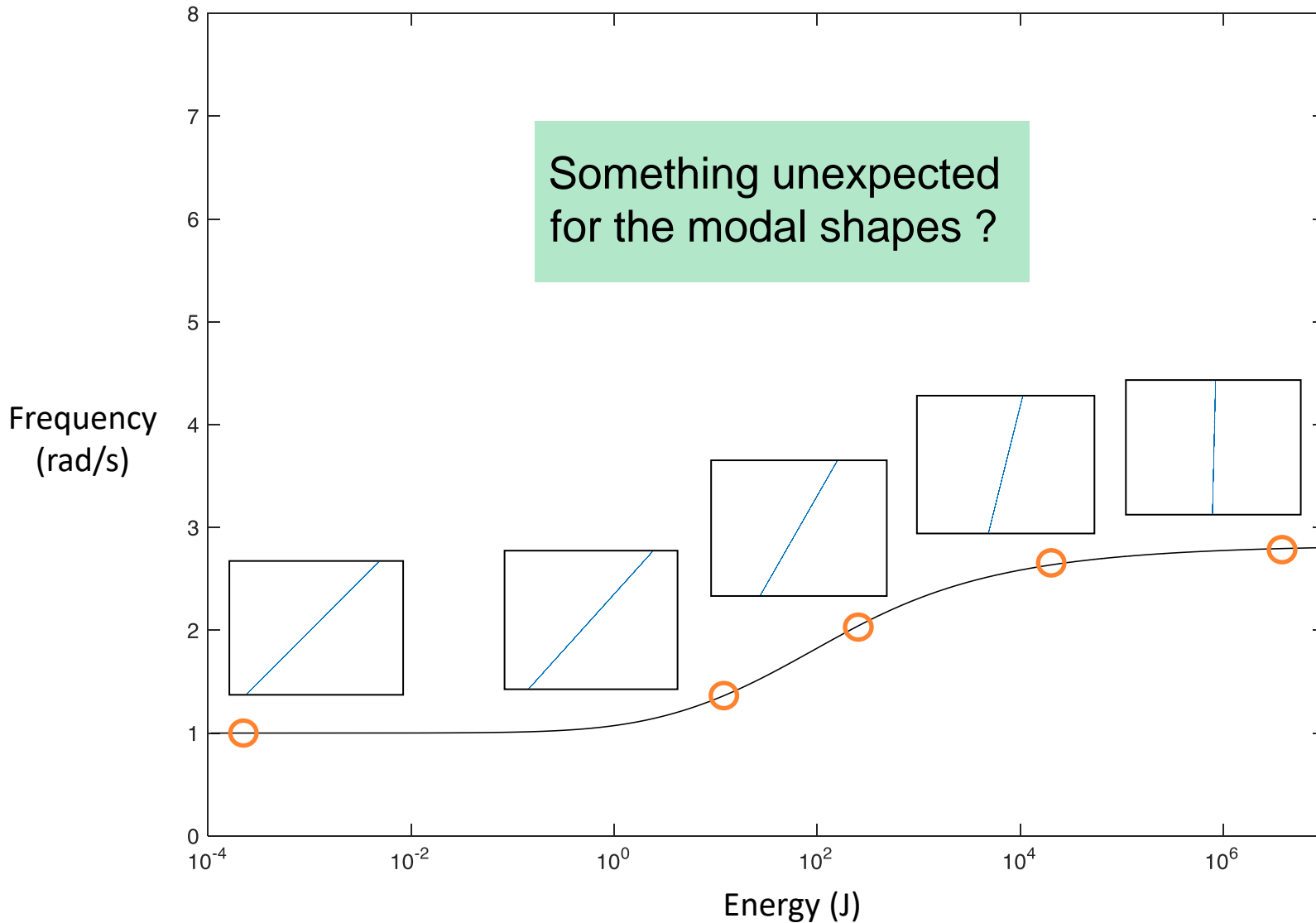
What you see is a nonlinear mode



Time series and time frequency analysis

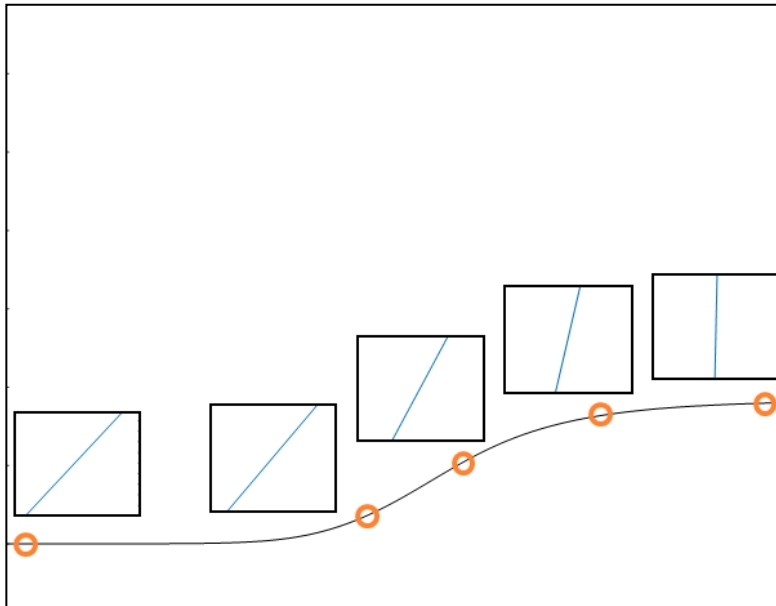


The in-phase NNM (1-term HB)

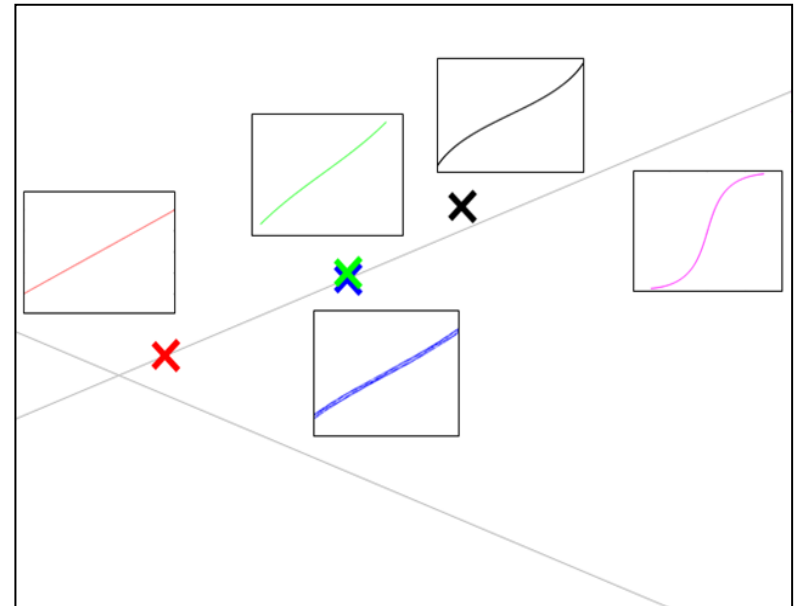


How come ?

HB with 1
harmonics



Numerical
simulation



Limitation of a 1-term harmonic balance method

$$\begin{aligned}\ddot{q}_1 + (2q_1 - q_2) + 0.5q_1^3 &= 0 \\ \ddot{q}_2 + (2q_2 - q_1) &= 0\end{aligned}$$

▼ $q_{1,2} \cong A, B \cos \omega t$

$$A = \pm \sqrt{\frac{8(\omega^2 - 3)(\omega^2 - 1)}{3(\omega^2 - 2)}}$$

$$B = \frac{A}{2 - \omega^2}$$

▼

$$q_1 = \frac{A}{B} q_2 = \frac{8 - \omega^2}{7} q_2$$

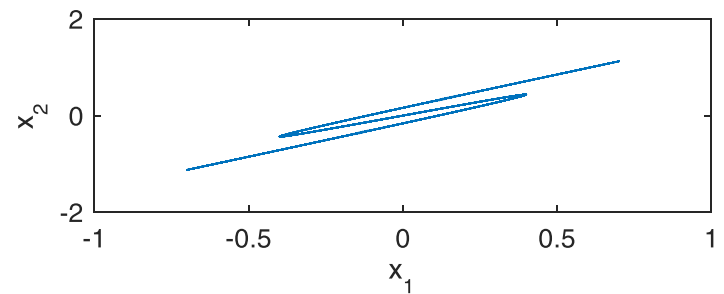
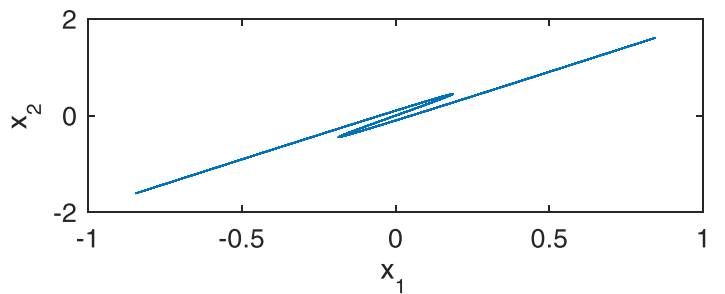
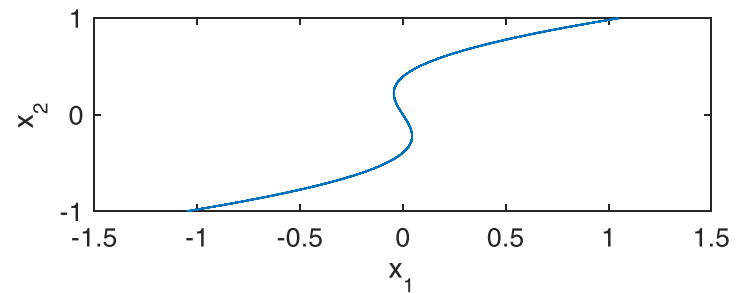
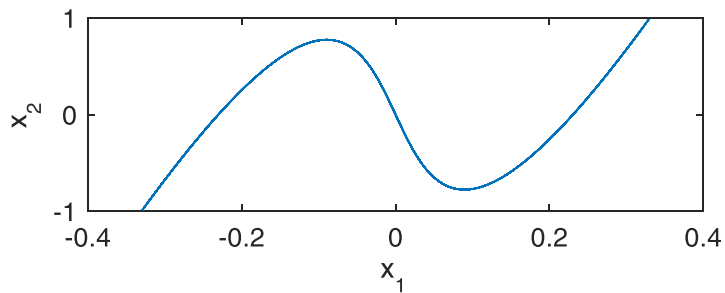
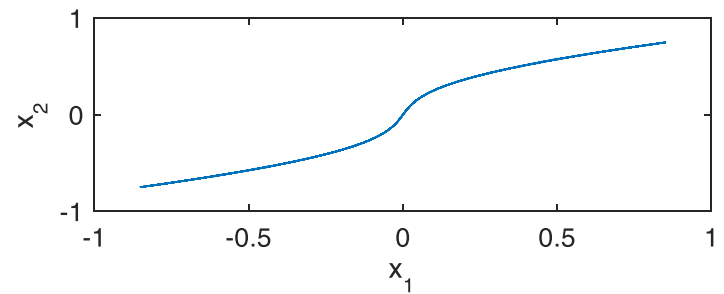
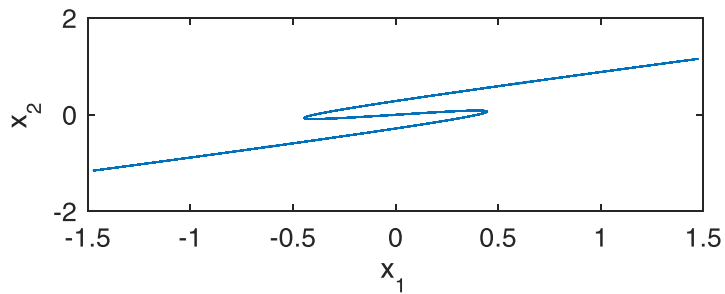
*Frequency-dependent linear relation
imposed between x_1 and x_2*

2. Harmonics

The mode curvature is induced by harmonics

$$x_1 = A\cos\omega t + B\cos 3\omega t$$

$$x_2 = C\cos\omega t + D\cos 3\omega t$$



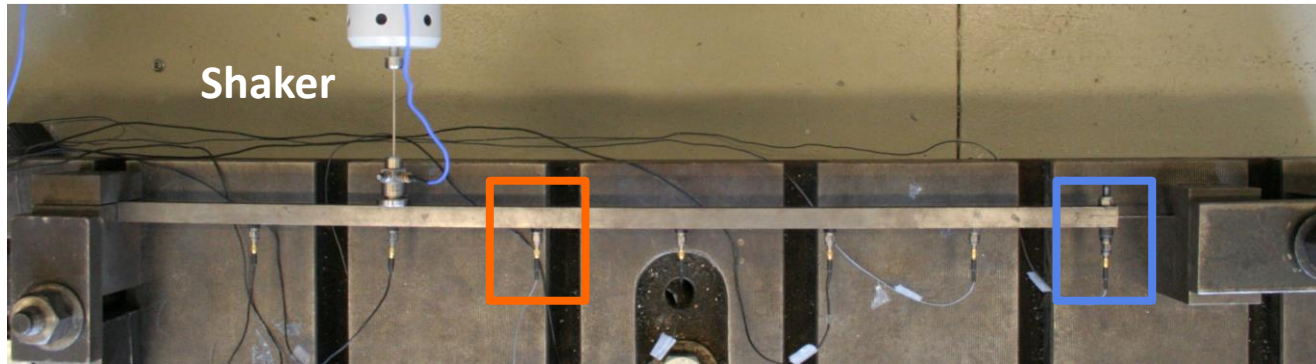
In Matlab

```
f=input('1=sin/sin 2=cos/cos: ');
w1=input('Enter harmonics 1:');
w2=input('Enter harmonics 2:');

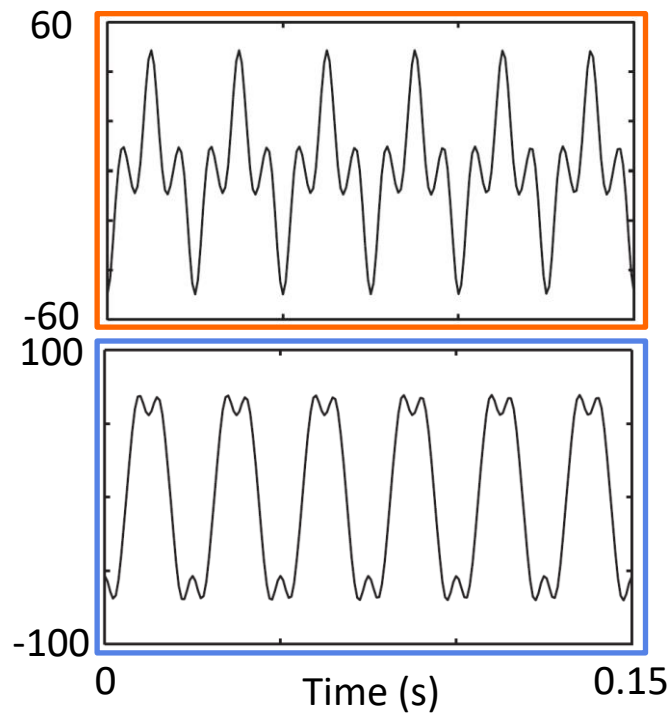
temps=[0:0.01:50];

if f==1
    for k=1:6
        x1=rand(1)*sin(w1*temps)+rand(1)*sin(w2*temps);
        x2=rand(1)*sin(w1*temps)+rand(1)*sin(w2*temps);
        subplot(3,2,k)
        plot(x1,x2)
        xlabel('x_1');
        ylabel('x_2');
        set(gcf,'uni','nor','pos',[0.2 0.2 0.6 0.6])
    end
else
    for k=1:6
        x1=rand(1)*cos(w1*temps)+rand(1)*cos(w2*temps);
        x2=rand(1)*cos(w1*temps)+rand(1)*cos(w2*temps);
        subplot(3,2,k)
        plot(x1,x2)
        xlabel('x_1');
        ylabel('x_2');
        set(gcf,'uni','nor','pos',[0.2 0.2 0.6 0.6])
    end
end
end
```

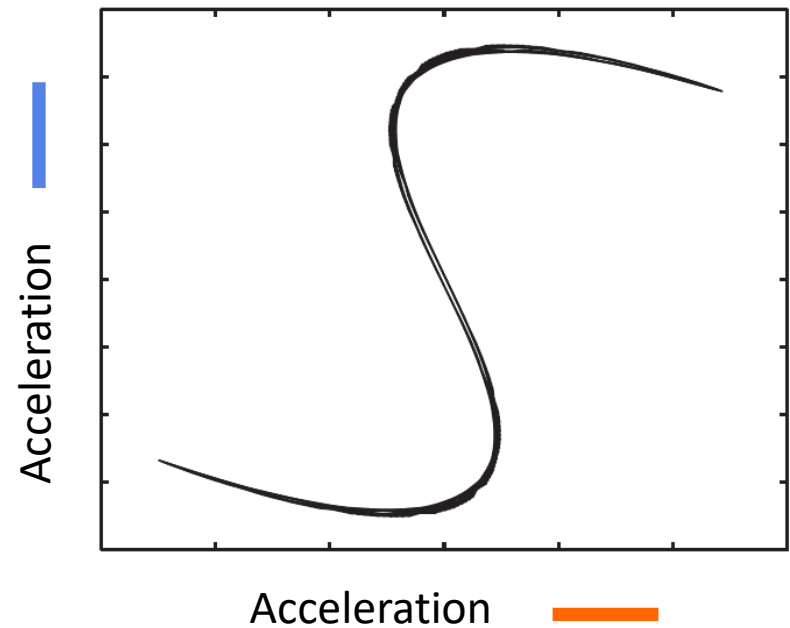

What you see is a *real* nonlinear mode



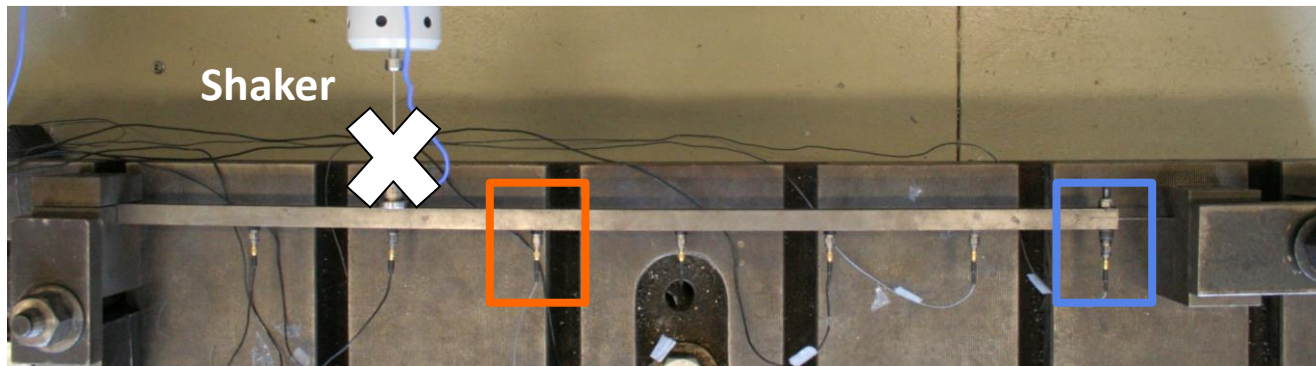
Acceleration (m/s^2)



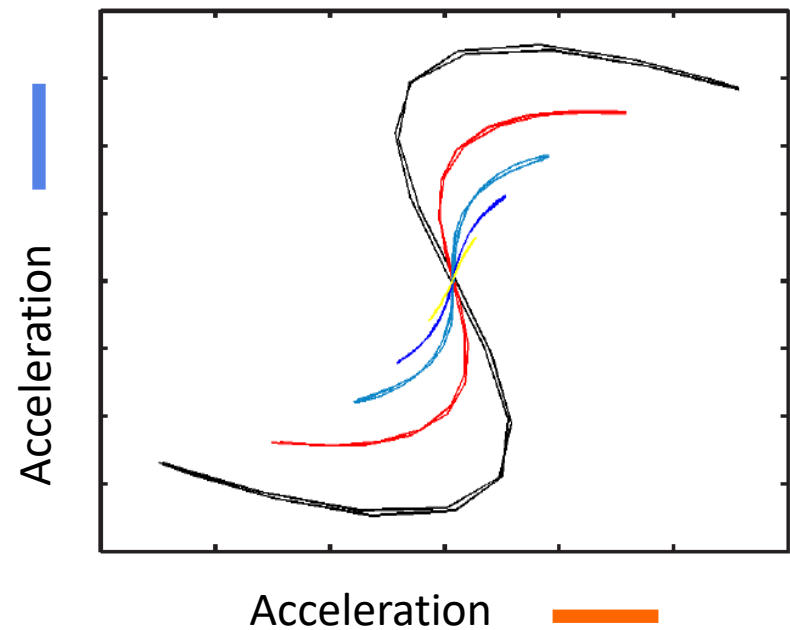
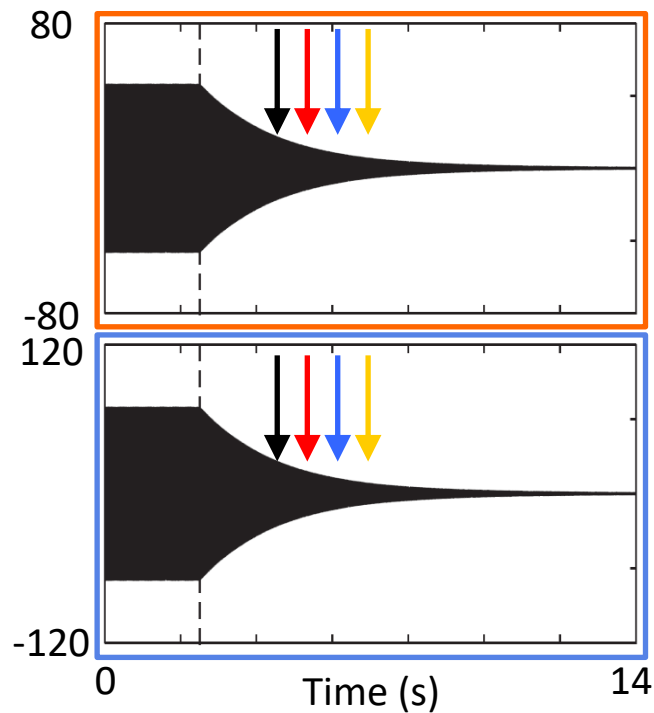
Nonlinear modes exhibit harmonics



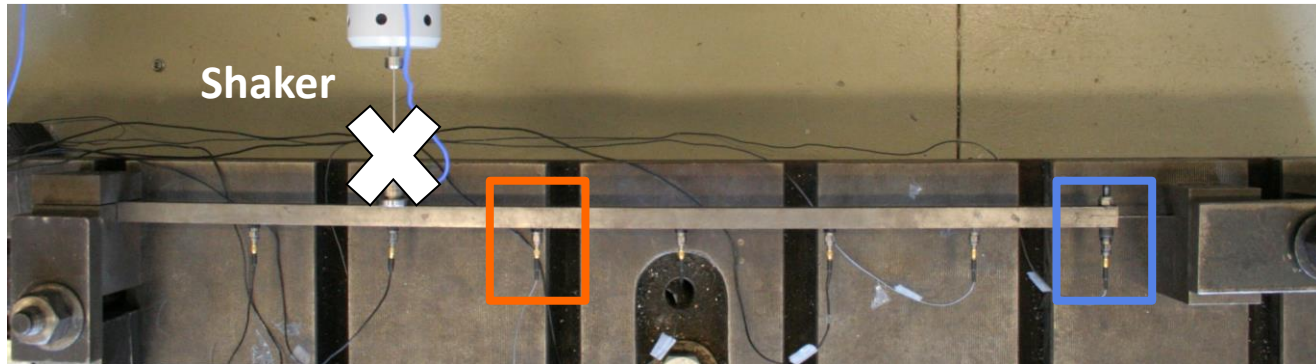
The mode shapes evolve with time



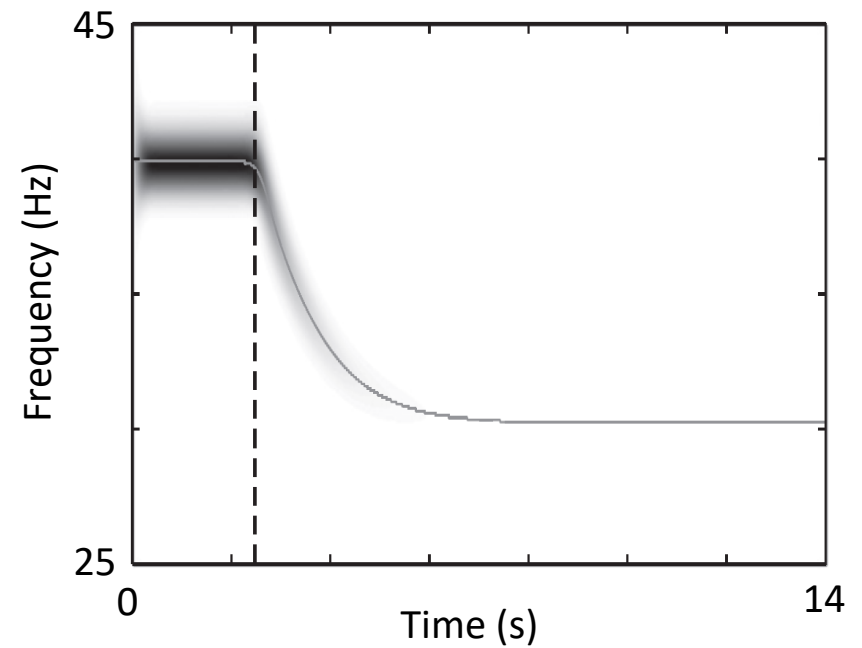
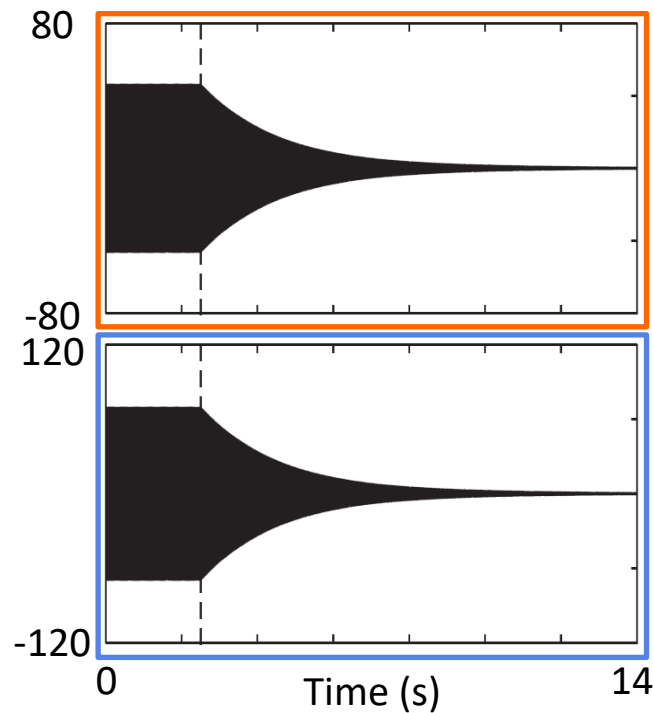
Acceleration (m/s^2)



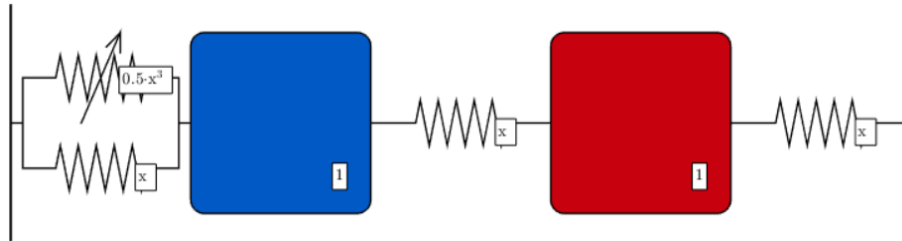
The natural frequency decreases with time



Acceleration (m/s^2)



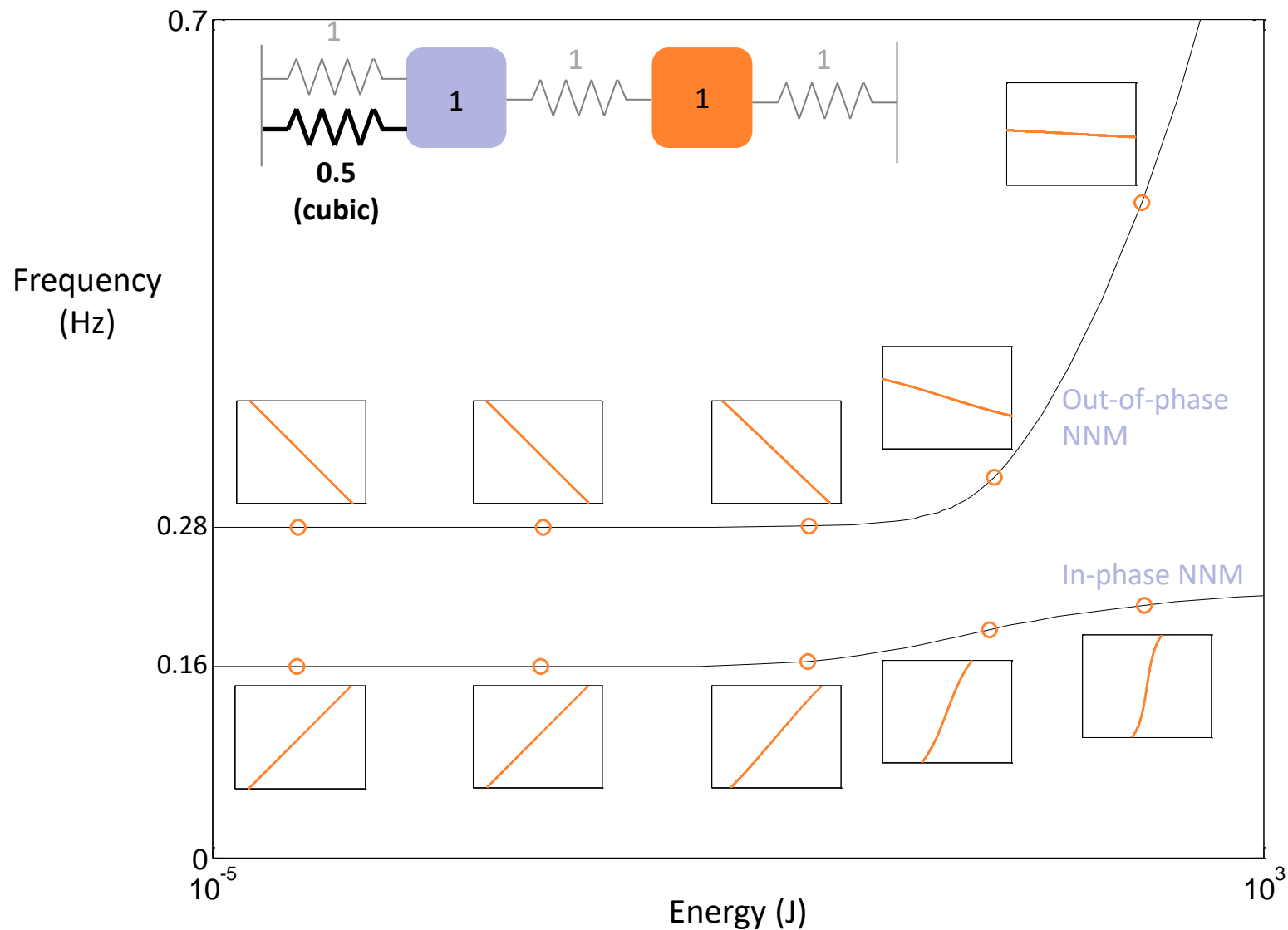
Numerical calculation



NI2D - 2DOF\NNM_ShawSystem

<input checked="" type="checkbox"/> Hz	Starting point: <input type="text" value="0.15915"/> Hz	
	Min: <input type="text" value="0"/> Hz	
	Max: <input type="text" value="Inf"/> Hz	
	Direction: <input type="radio"/> - <input checked="" type="radio"/> +	
<input type="checkbox"/> Stability	<input type="checkbox"/> Half-period	<input checked="" type="checkbox"/> Sensitivity analysis
<input checked="" type="checkbox"/> Adaptive	Stepsize: <input type="text" value="0.01"/>	
	Min: <input type="text" value="1e-06"/>	
	Max: <input type="text" value="10"/>	
	Optimal number of iterations: <input type="text" value="3"/>	
	Max. number of iterations: <input type="text" value="10"/>	
	Precision: <input type="text" value="1e-06"/>	
	Maximum number of points: <input type="text" value="25"/>	
	Beta max. angle: <input type="text" value="90"/> °	
	Scaling factor: <input type="text" value="0.0001"/>	
	Number of points: <input type="text" value="360"/>	

« Curved » nonlinear modes are now obtained



Do it yourself in NI2D: create a 2-DOF model

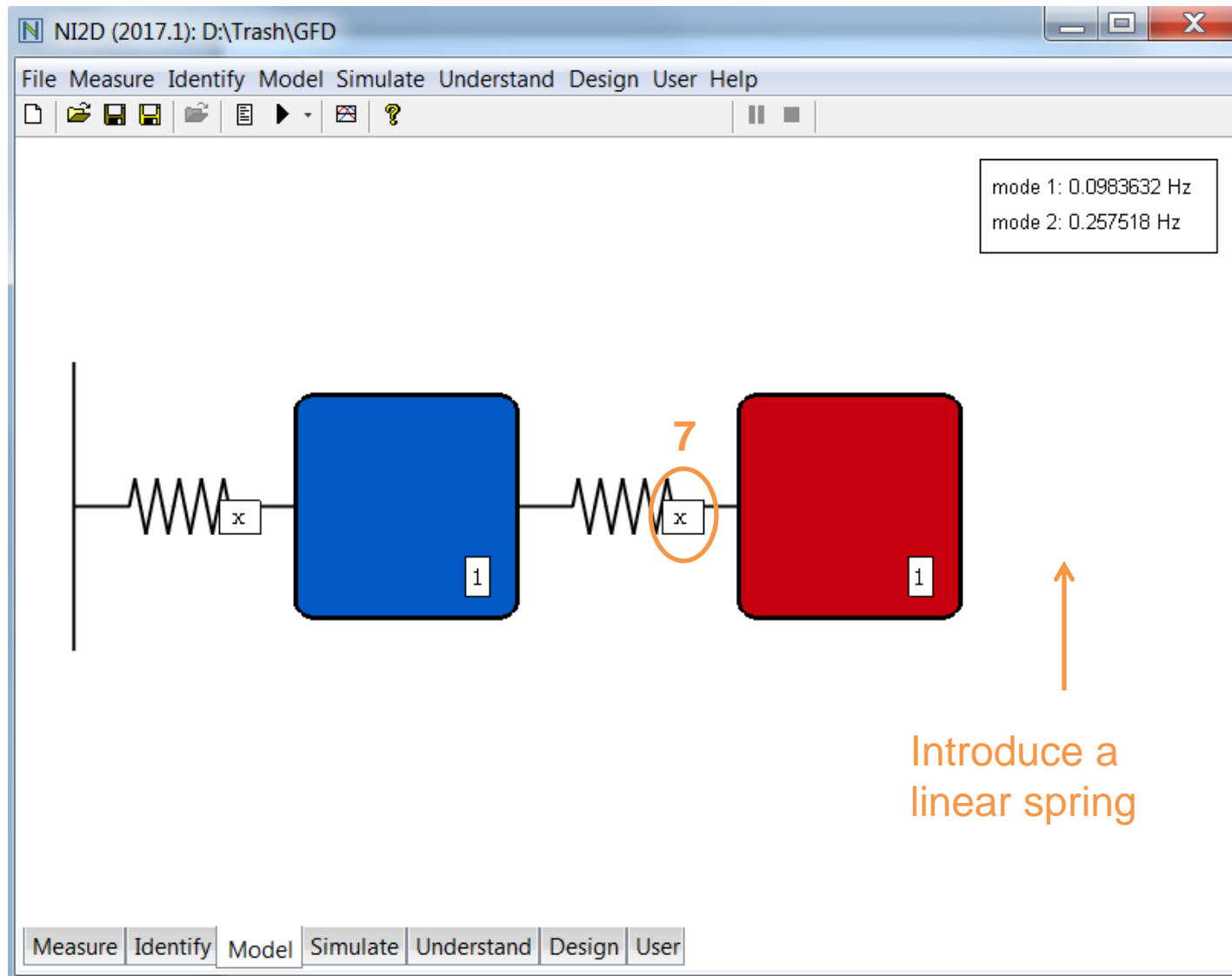
The screenshot shows the NI2D (2017.1) software interface. The main window displays a mechanical system diagram with a blue mass and a spring. A sinusoidal input $\sin(2\pi \cdot t)$ is applied to the mass. A status box in the top right corner indicates "mode 1: 31.0631 Hz / 0.12 %".

The "NI2D: New model" dialog box is open, showing the "Spring/mass system" tab. The "Number of masses" field is set to 3, with a red circle around the number 3 and a red number 2 next to it. The other parameters are:

- Mass: 1 Kg
- Linear damping: 0.1 N.s/m
- Linear stiffness: 1 N/m

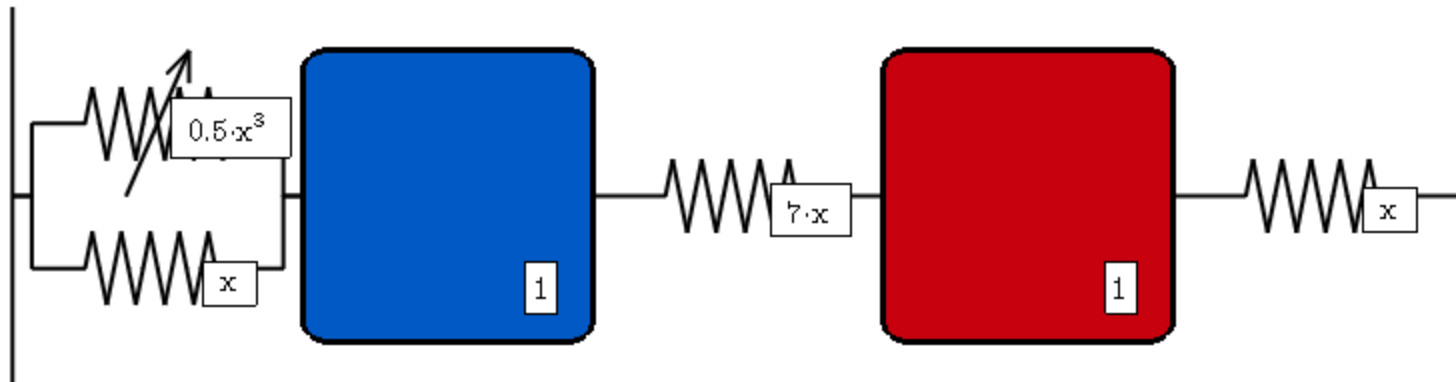
Buttons for "Continue >" and "Abort" are visible at the bottom of the dialog. The main window's menu bar includes File, Measure, Identify, Model, Simulate, Understand, Design, User, and Help. The toolbar contains icons for file operations and simulation control.

Modify the 2-DOF model



The final model

mode 1: 0.159155 Hz
mode 2: 0.616404 Hz



In-phase mode: set appropriate parameters

NNM continuation parameters

Starting point: 0.15915 Hz

Hz

Min: 0 Hz

Max: Inf Hz

Direction: - +

Stability Half-period Sensitivity analysis

Stepsize: 0.01

Adaptative

Min: 1e-006

Max: 10

Optimal number of iterations: 3

Max. number of iterations: 10

Precision: 1e-006

Maximum number of points: 15

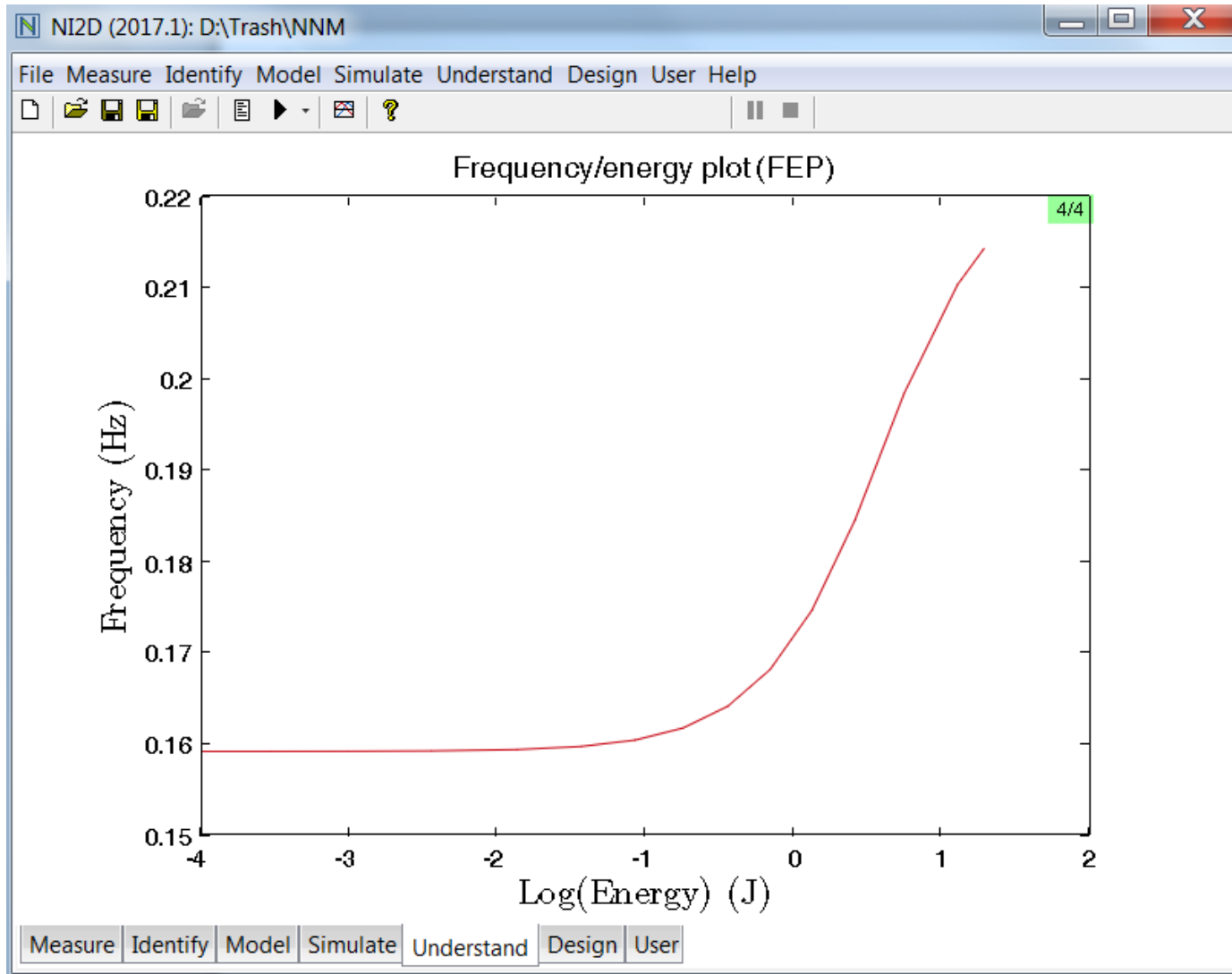
Beta max. angle: 90 °

Scaling factor: 0.0001

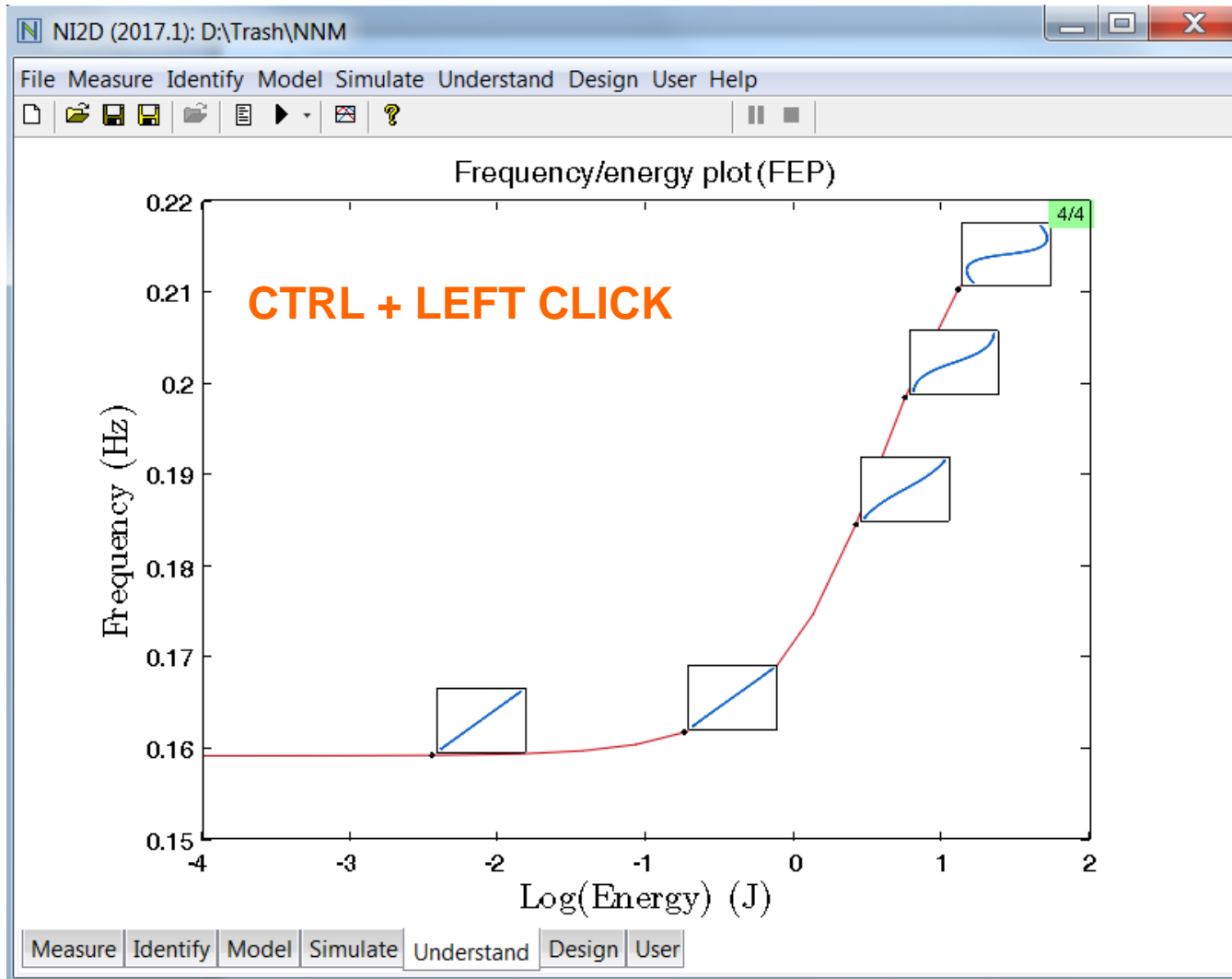
Number of points: 360

Newmark param... Apply Start Cancel

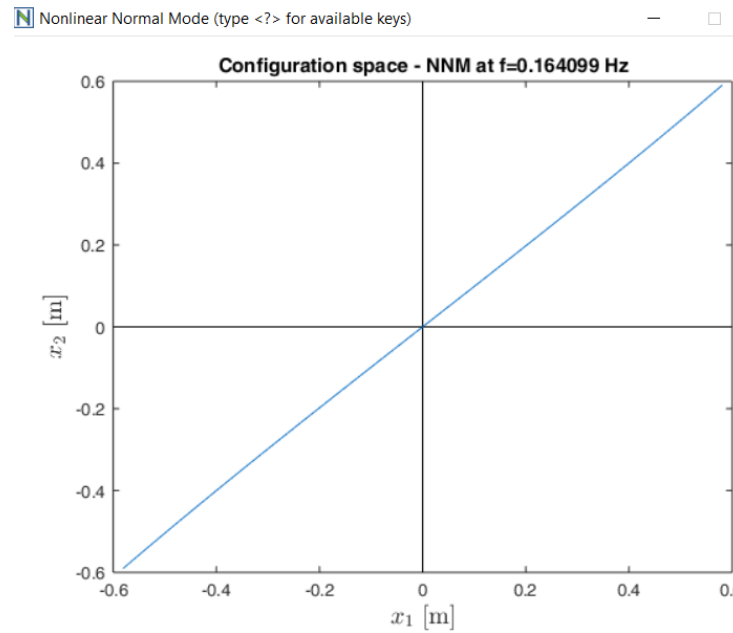
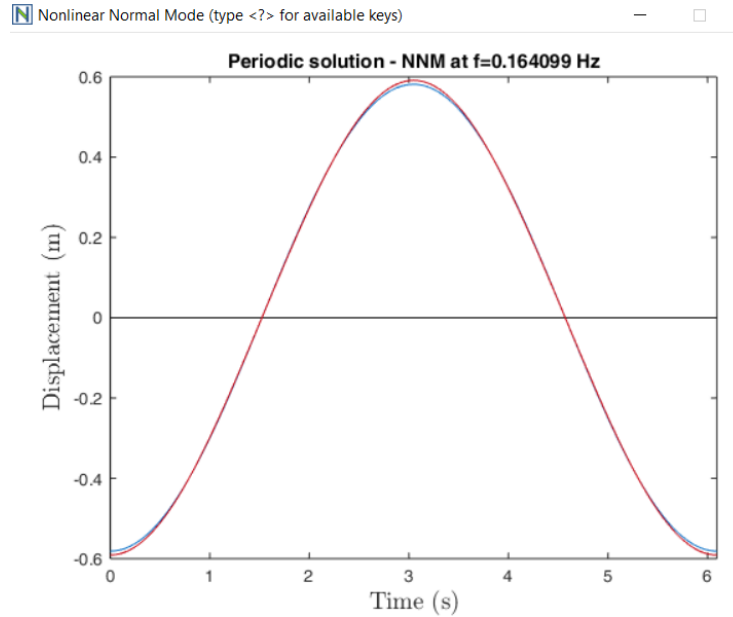
In-phase mode: resonance frequency



In-phase mode: mode shapes

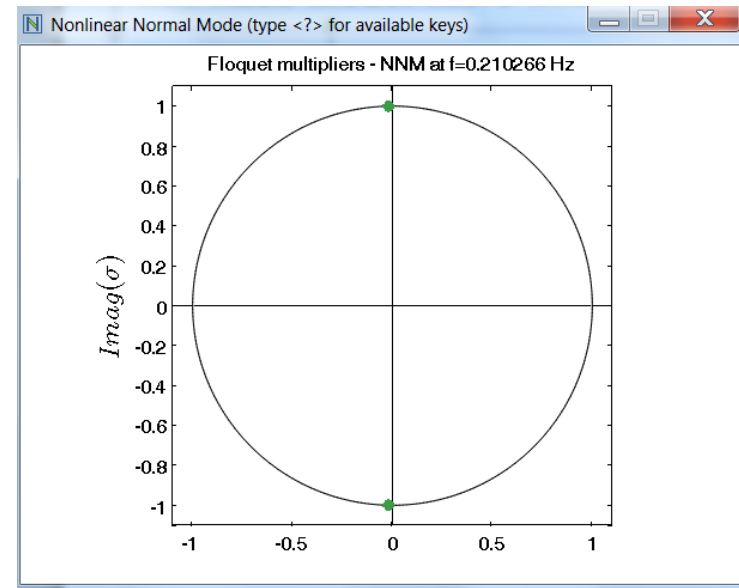
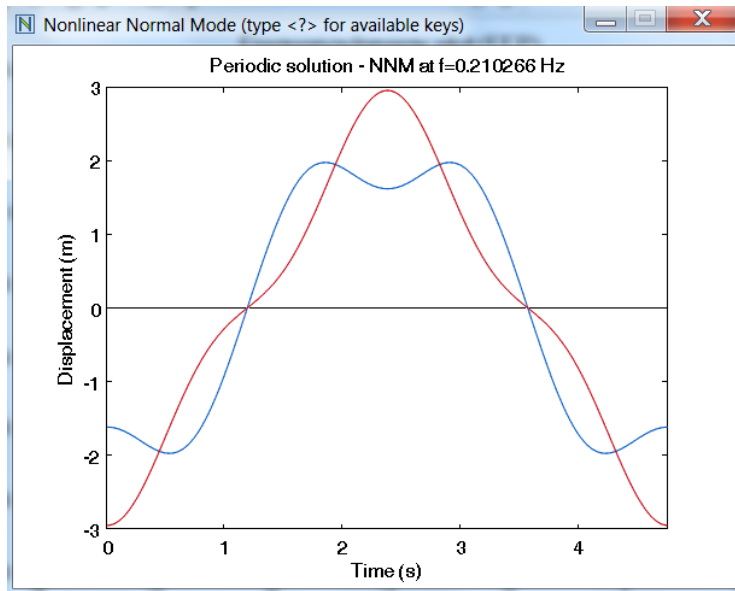


In-phase mode @ low energies

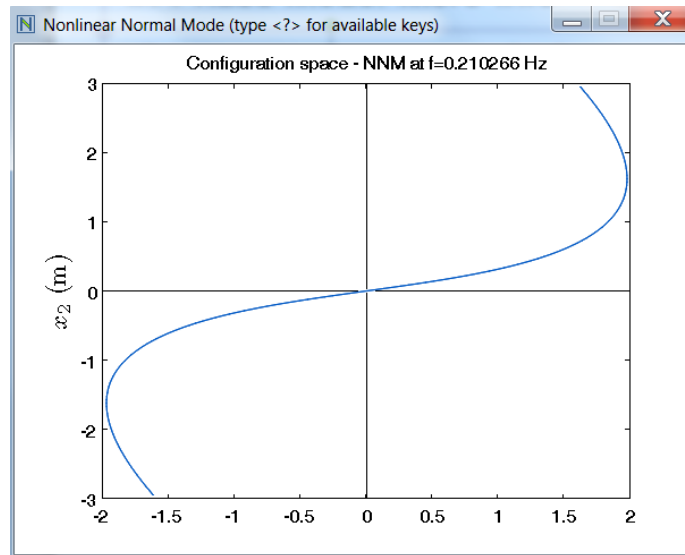


Double click + A

In-phase mode @ high energies



Double click + A



THE MOTION IS NON SYNCHRONOUS !?!

Out-of-phase mode: set the parameters

Starting point: 0.6164 Hz

Hz Min: 0 Hz

Max: Inf Hz

Direction: - +

Stability Half-period Sensitivity analysis

Stepsize: 0.01

Adaptative Min: 1e-006

Max: 10

Optimal number of iterations: 3

Max. number of iterations: 10

Precision: 1e-006

Maximum number of points: 20

Beta max. angle: 90 °

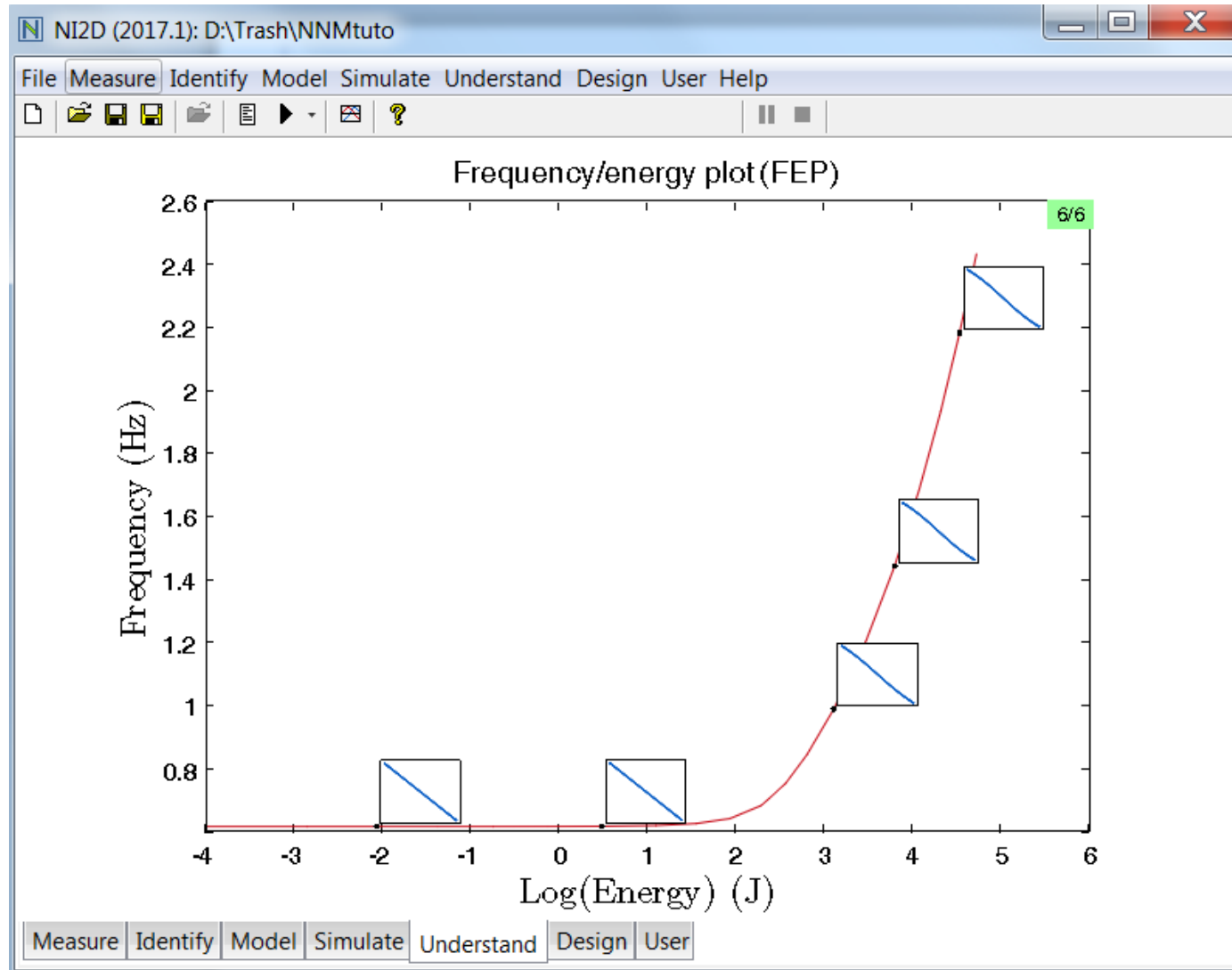
Scaling factor: 0.0001

Number of points: 360

Newmark param... Apply Start Cancel

Right click

Out-of-phase mode: frequency and mode shapes



Let's go back to the in-phase mode

NNM continuation parameters

Starting point: 0.15915 Hz

Hz

Min: 0 Hz

Max: Inf Hz

Direction: - +

Stability Half-period Sensitivity analysis

Adaptive

Stepsize: 0.01

Min: 1e-06

Max: 10

Optimal number of iterations: 3

Max. number of iterations: 10

Precision: 1e-06

Maximum number of points: 50

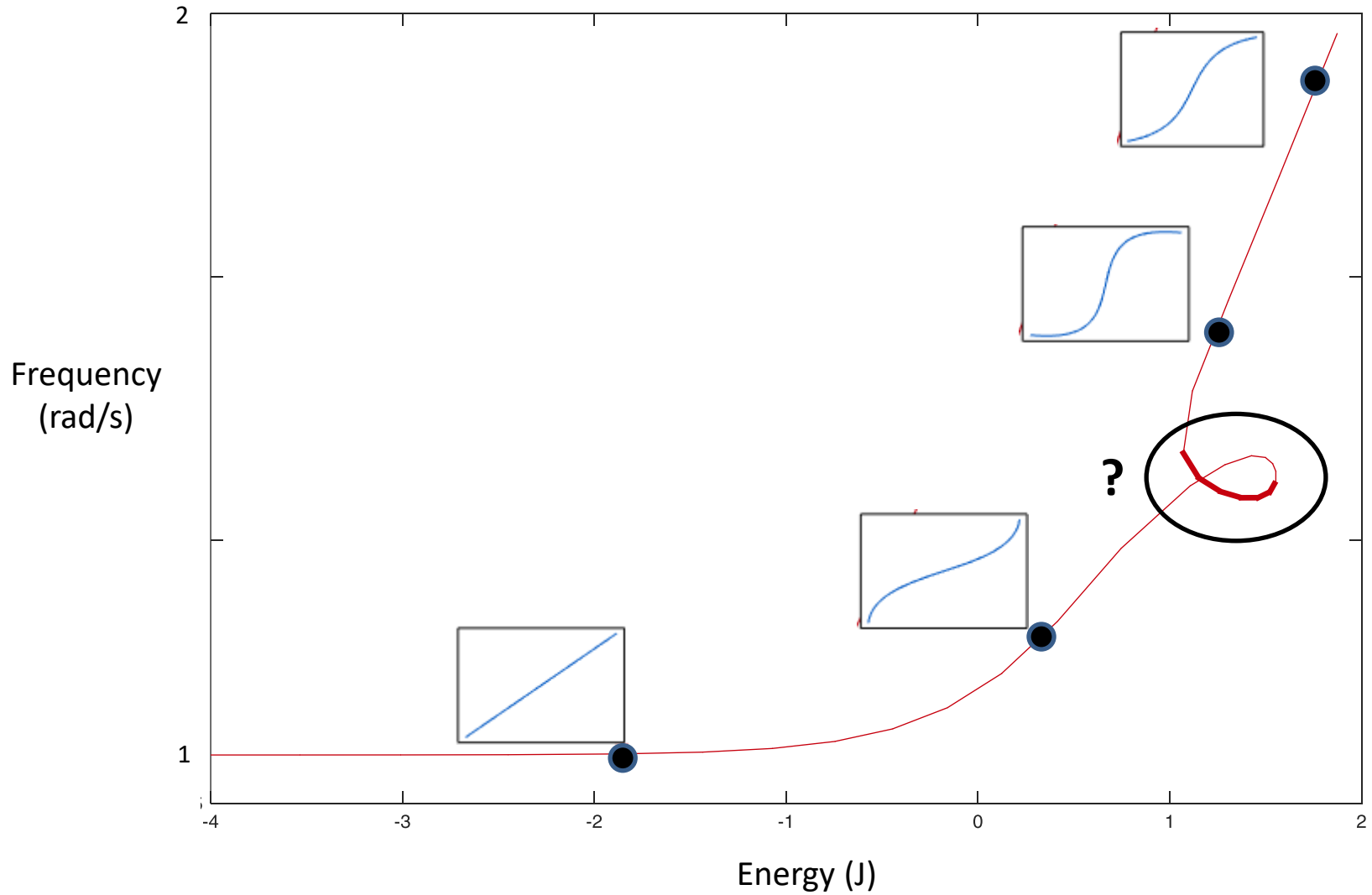
Beta max. angle: 90 °

Scaling factor: 0.0001

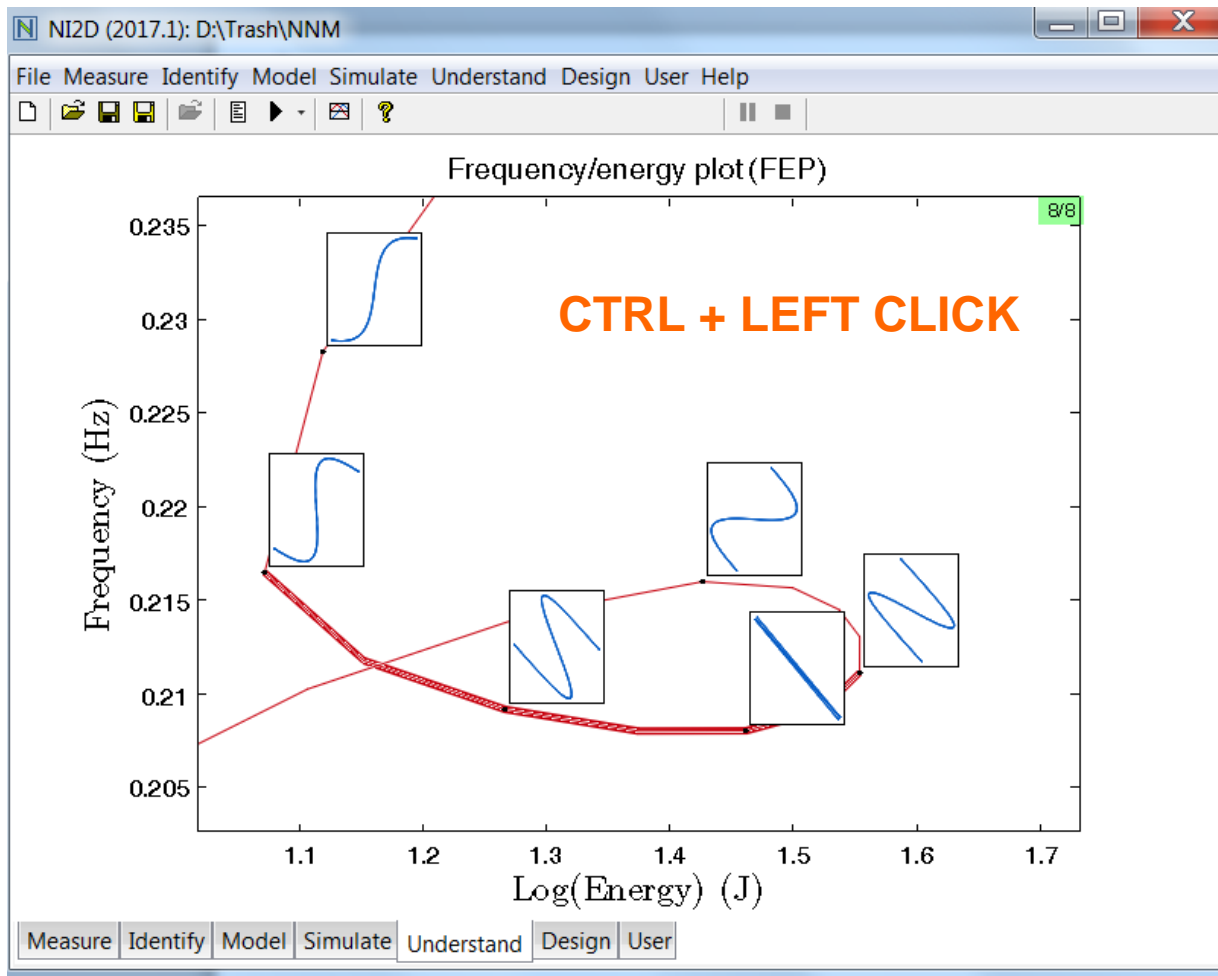
Number of points: 360

Right click
for mode 2

One new feature !



Zoom around the loop



Let's go even further

NNM continuation parameters

Hz

Starting point: Hz

Min: Hz

Max: Hz

Direction: - +

Stability Half-period Sensitivity analysis

Adaptive

Stepsize:

Min:

Max:

Optimal number of iterations:

Max. number of iterations:

Precision:

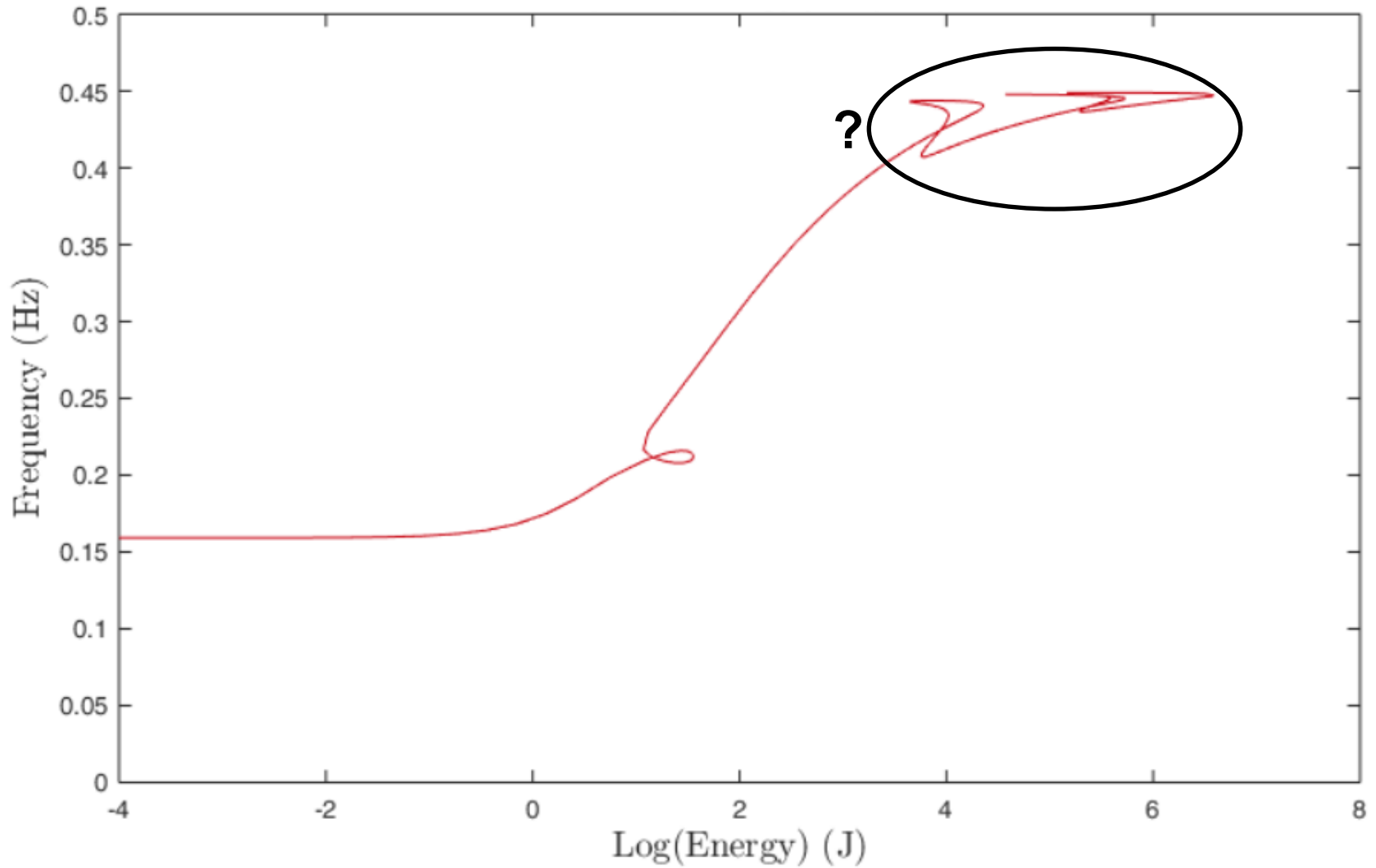
Maximum number of points:

Beta max. angle: °

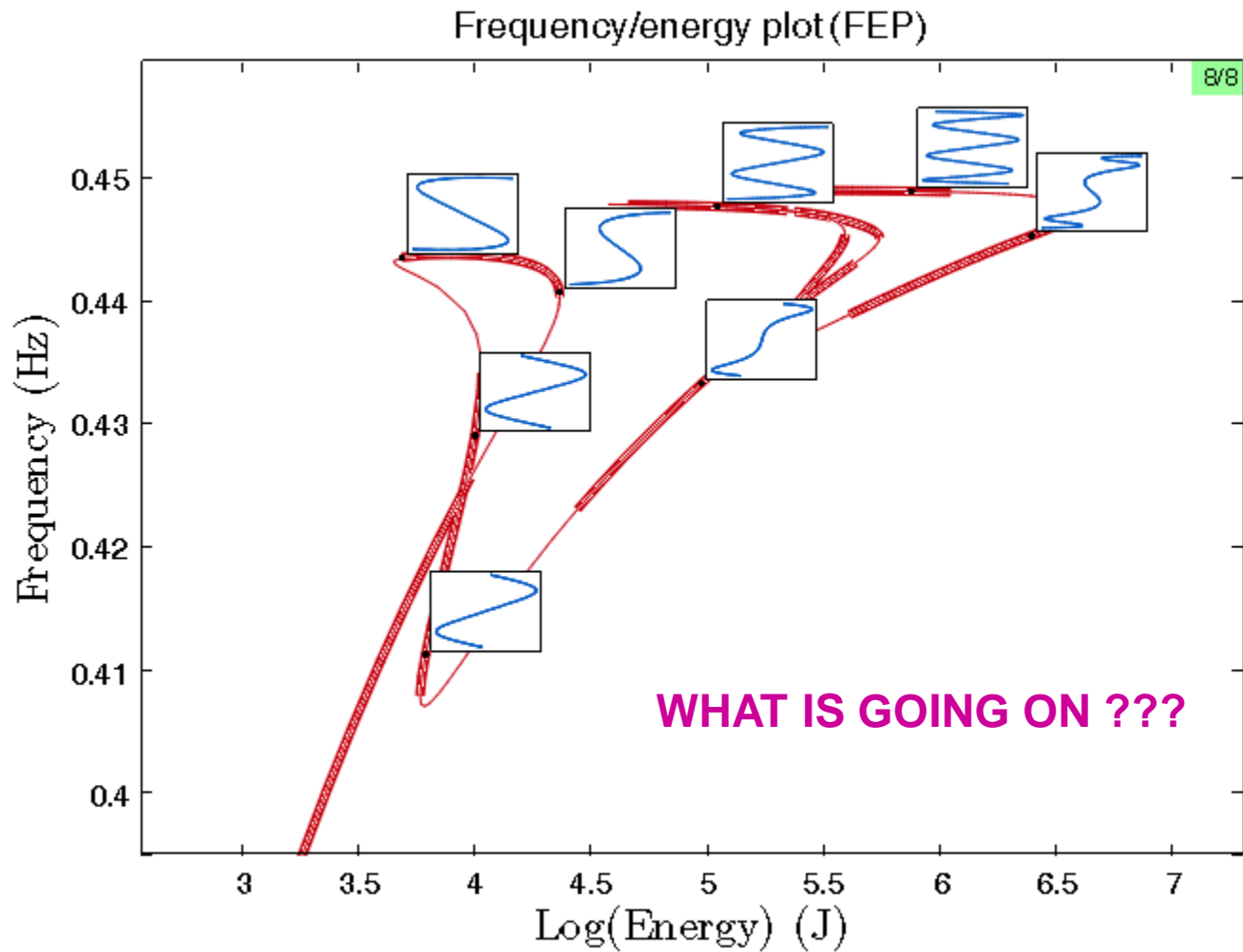
Scaling factor:

Number of points:

Additional loops

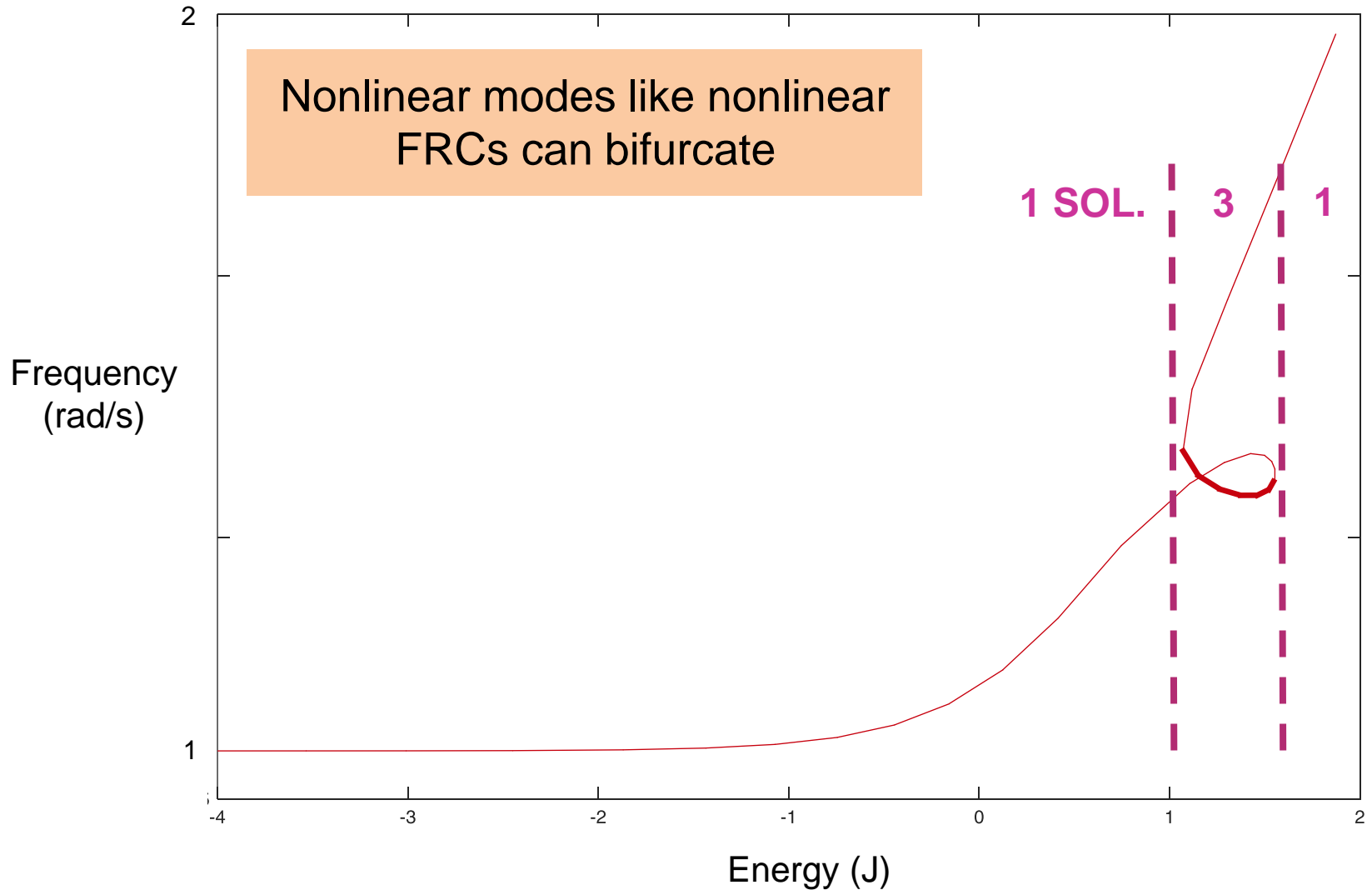


Zoom around the loops

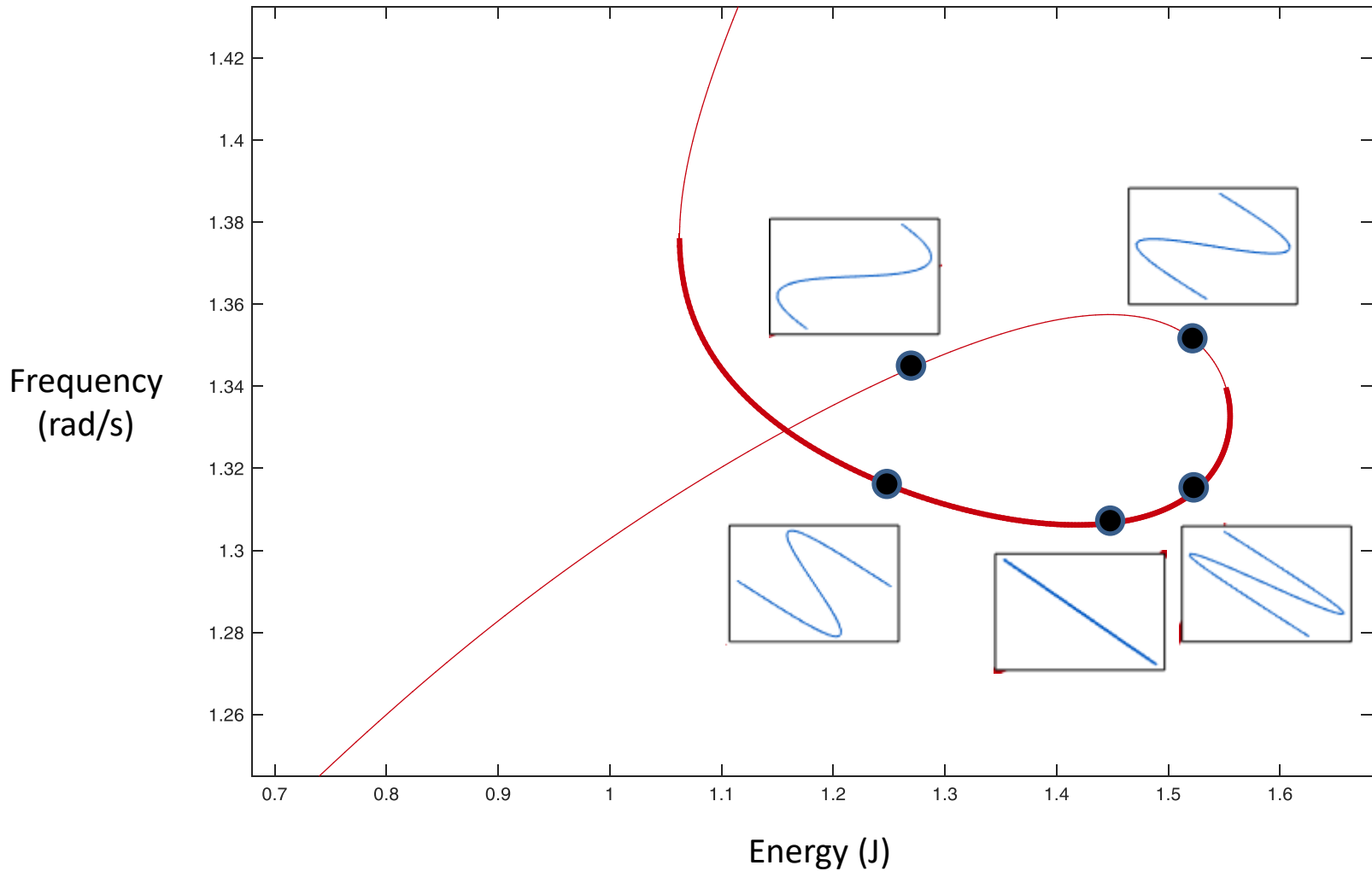


3. Bifurcations

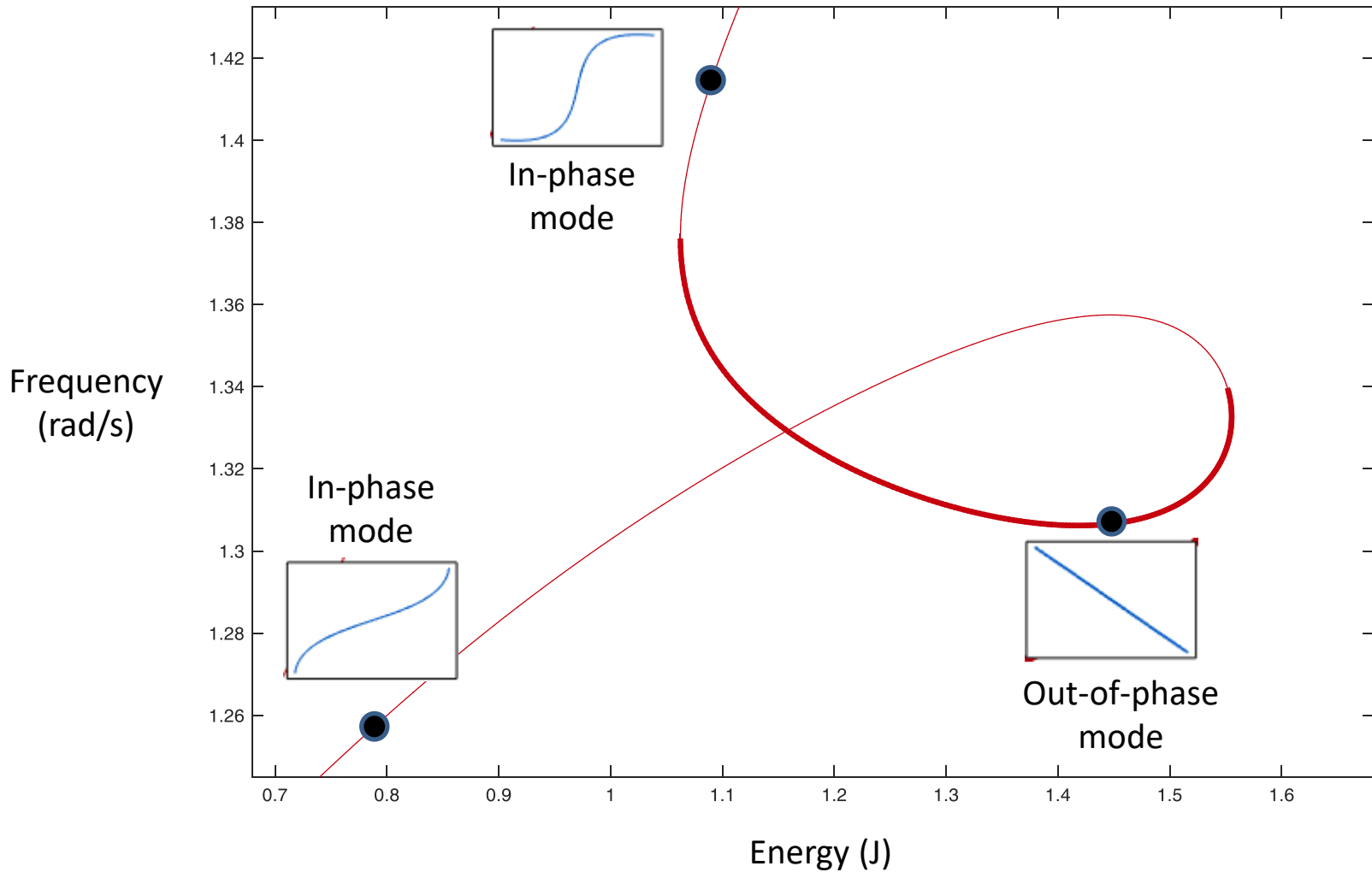
Three in-phase modes at a specific energy



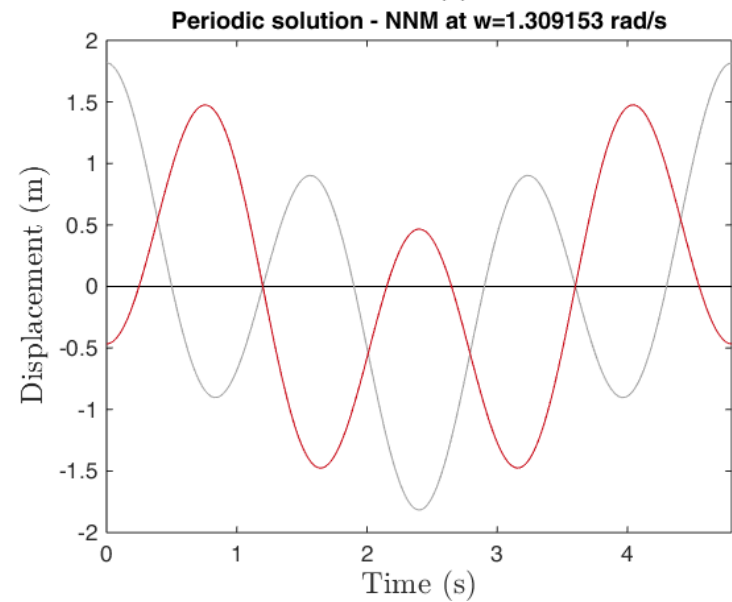
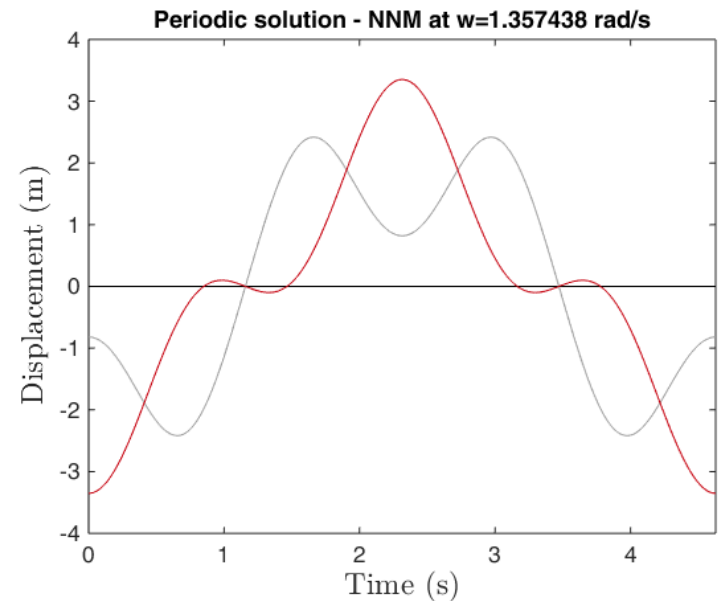
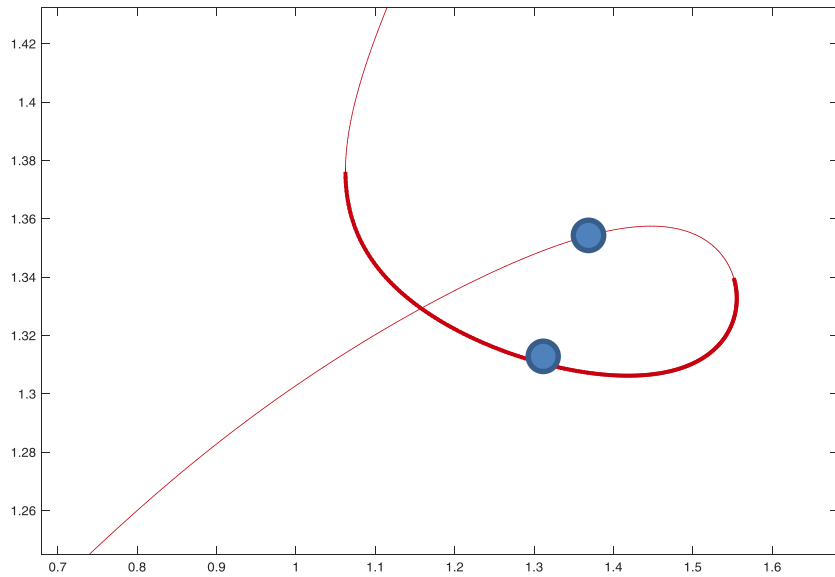
Modes on the branch present a third harmonic



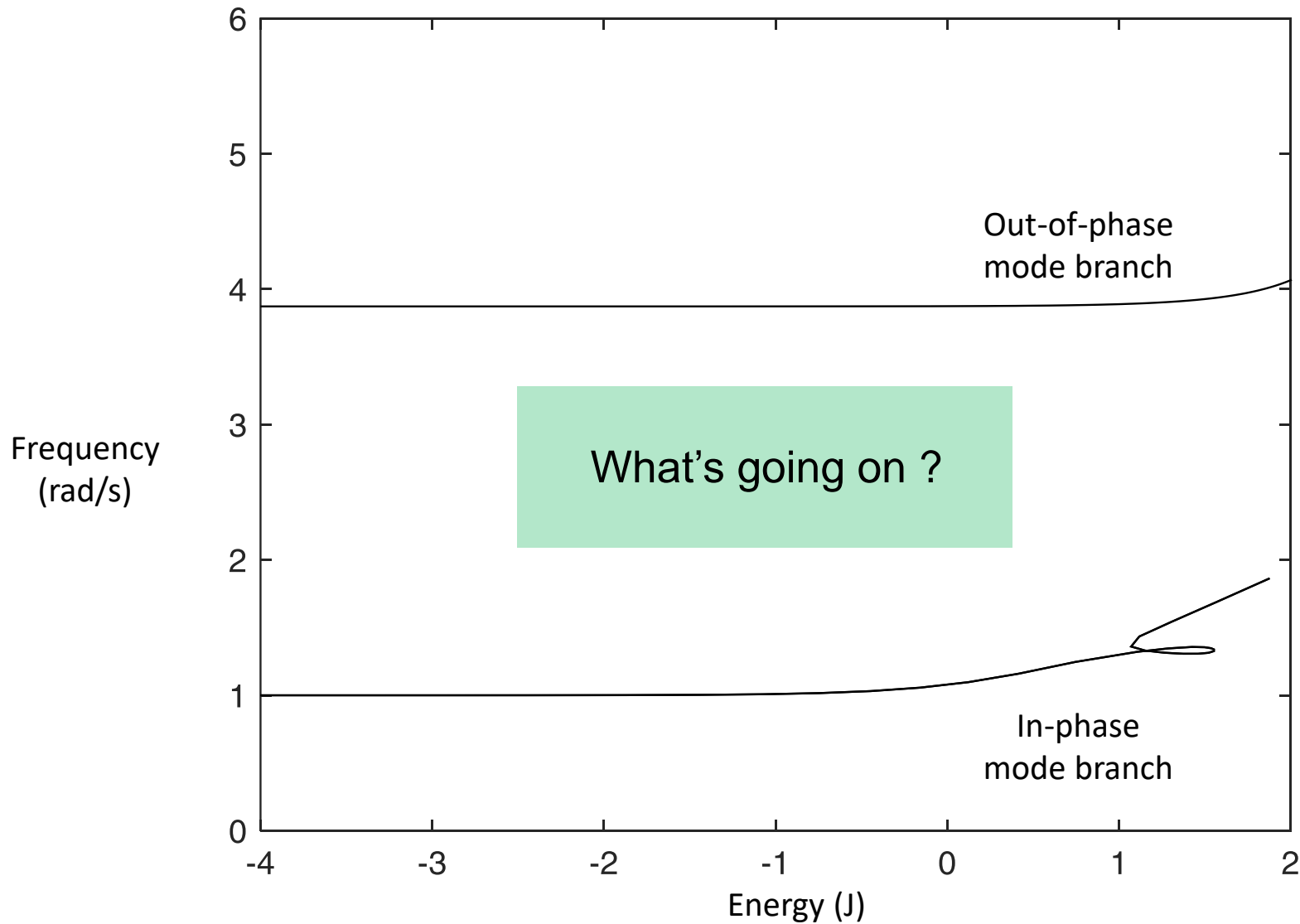
In-phase and out-of-phase modes “connected” !



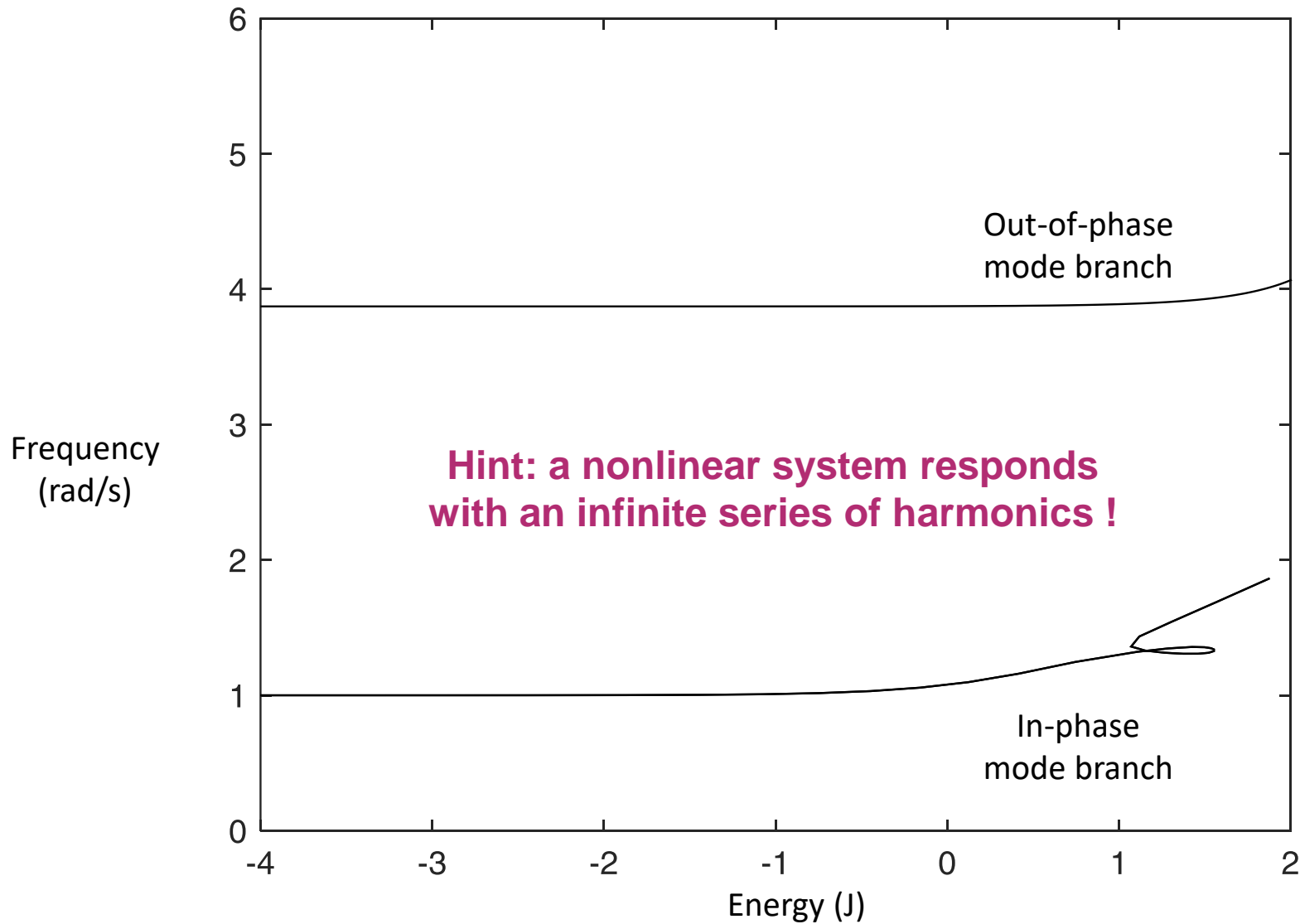
No longer a synchronous motion



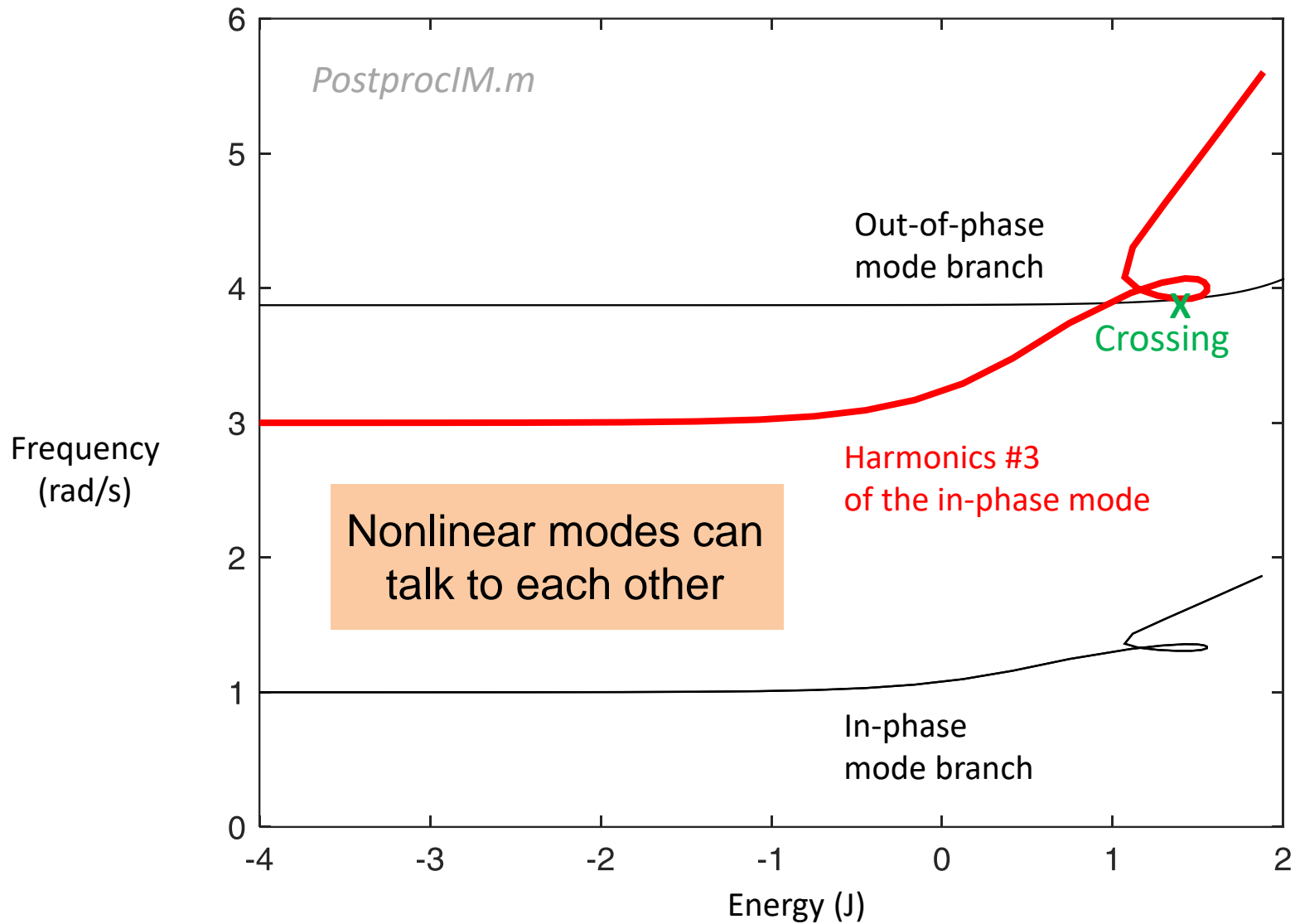
In-phase and out-of-phase modes NOT “connected” !



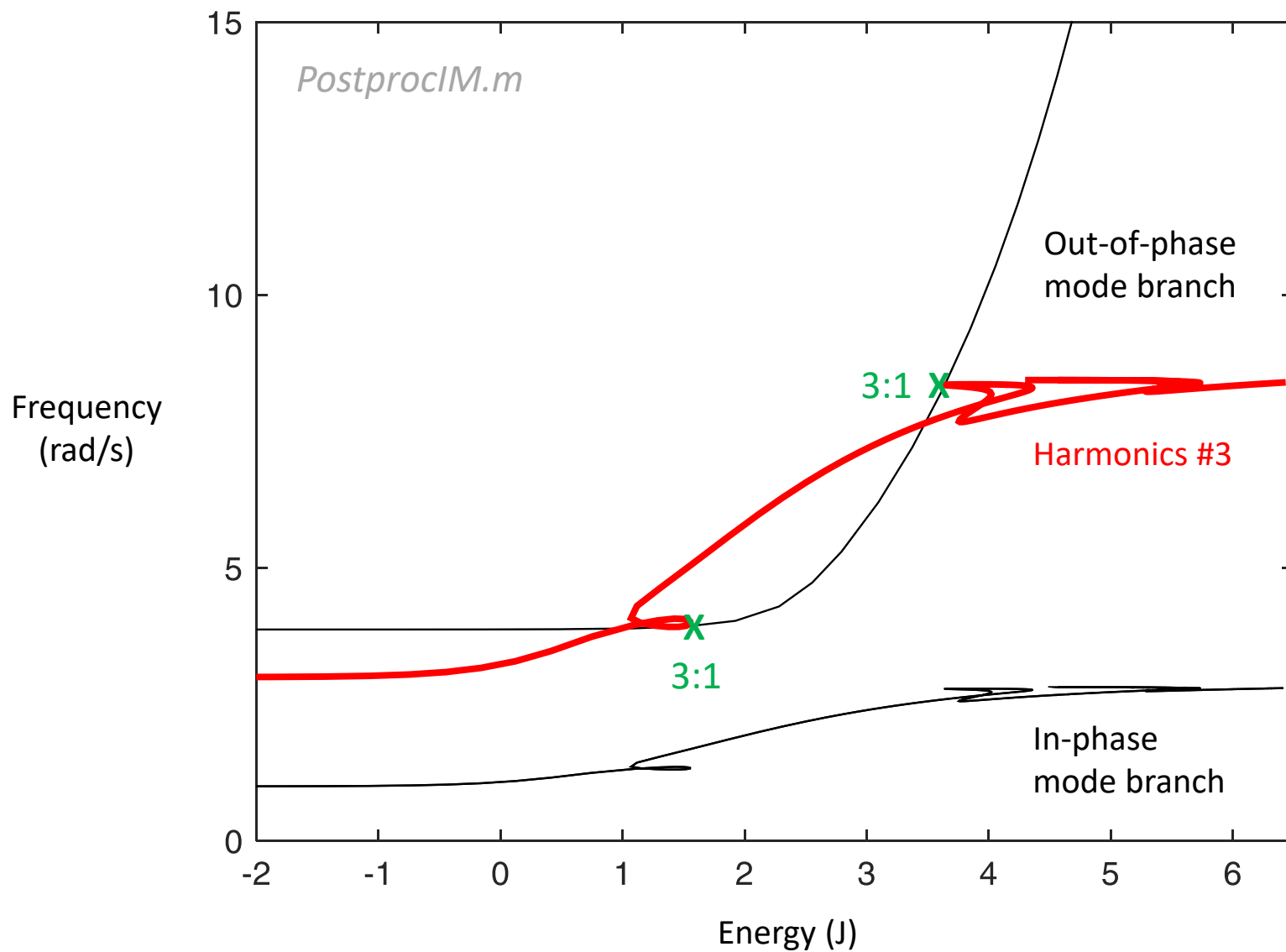
In-phase and out-of-phase modes NOT “connected” !



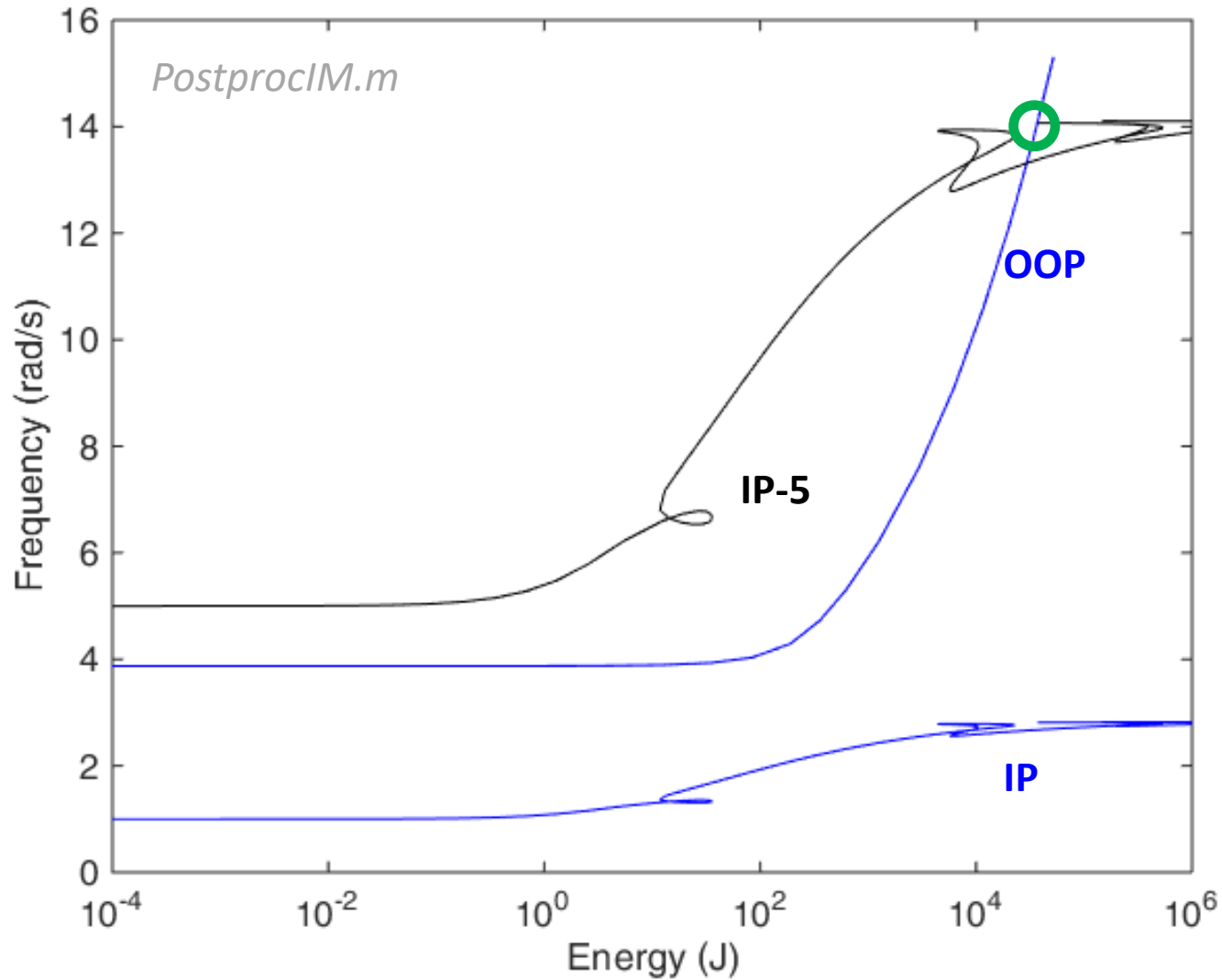
The missing piece of info of the FEP: harmonics



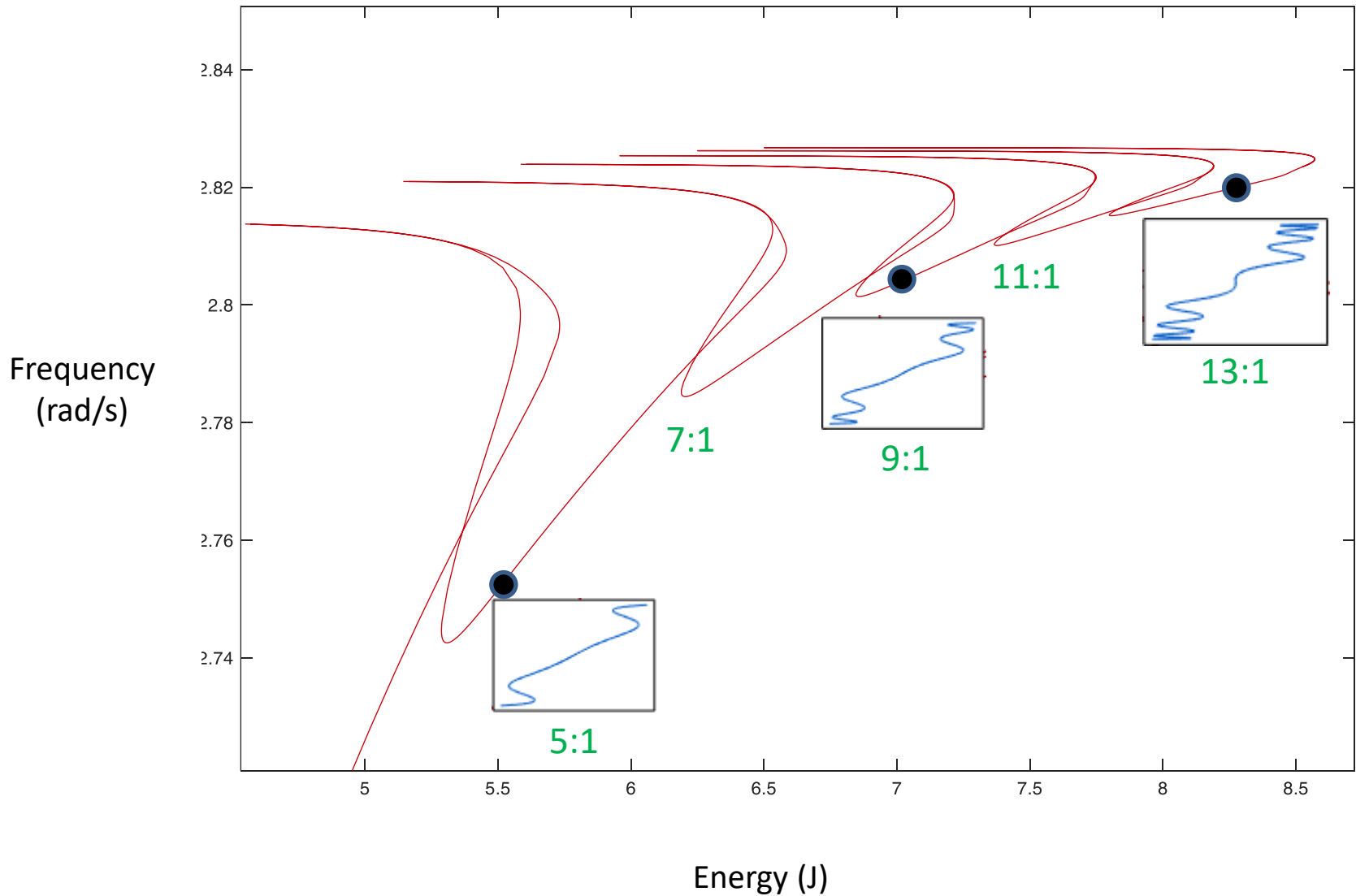
Evidence of another 3:1 modal interaction



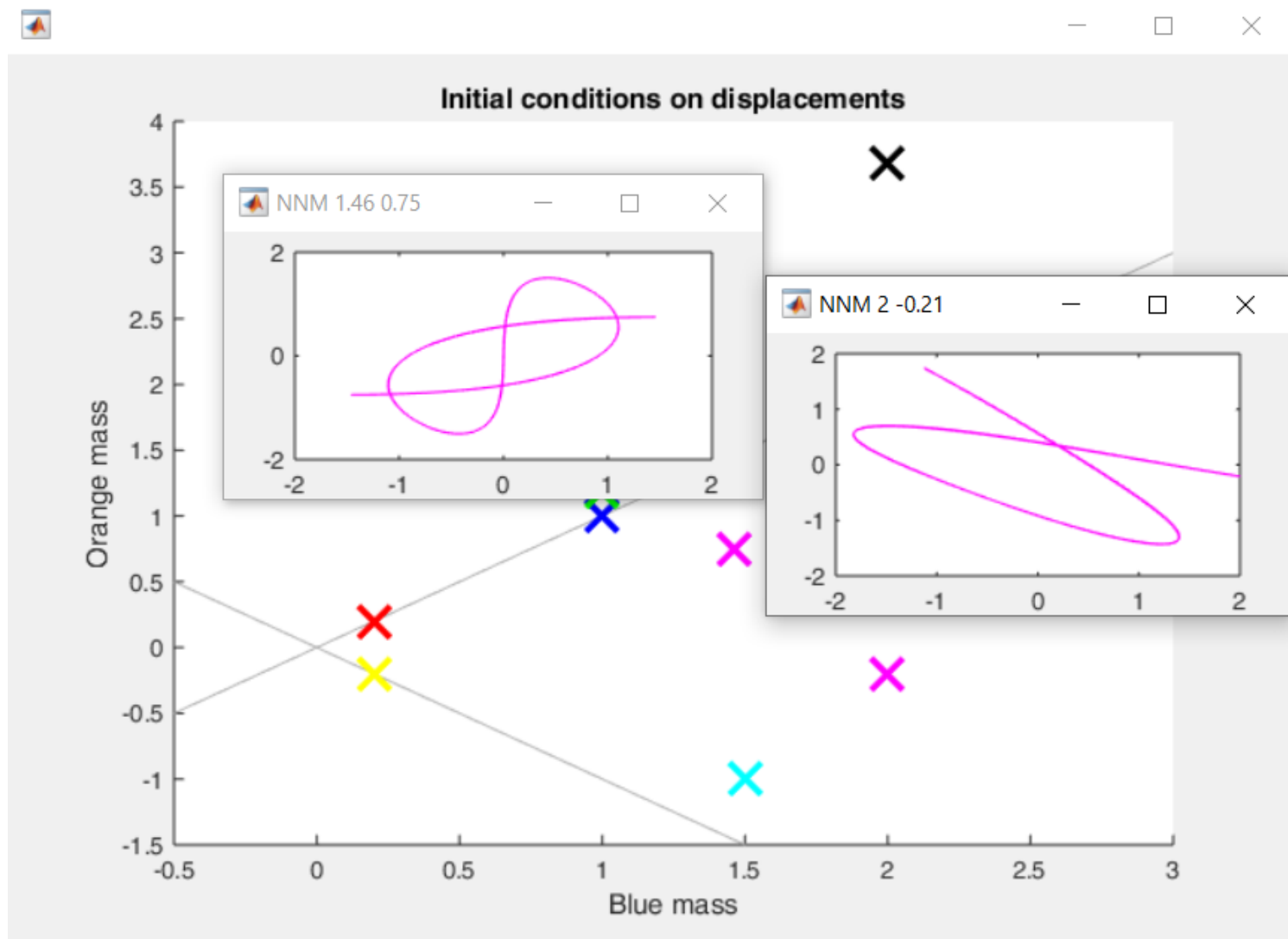
There should be a 5:1 modal interaction as well...



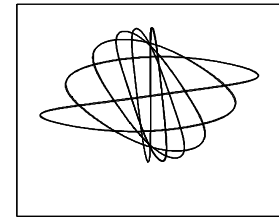
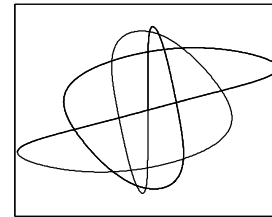
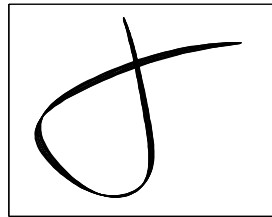
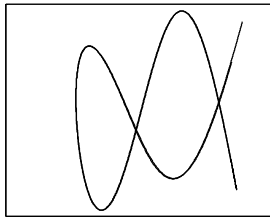
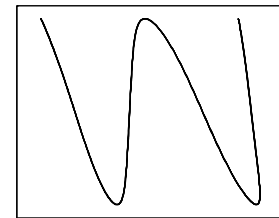
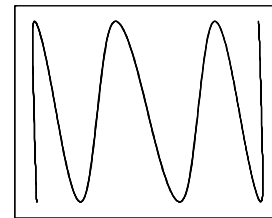
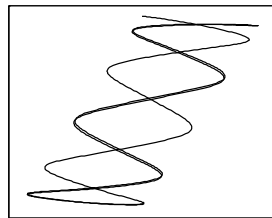
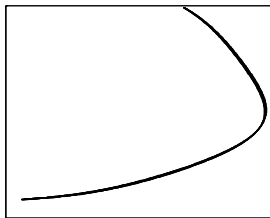
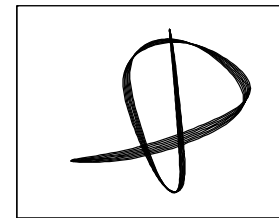
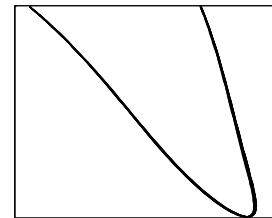
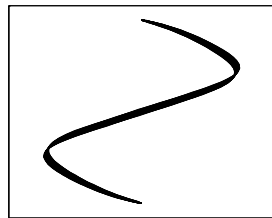
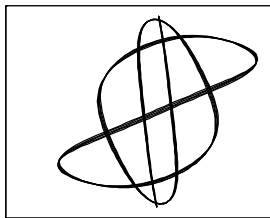
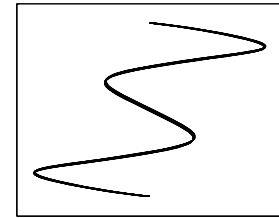
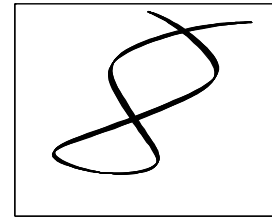
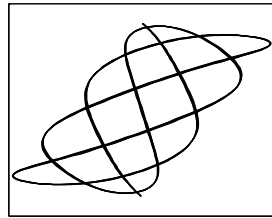
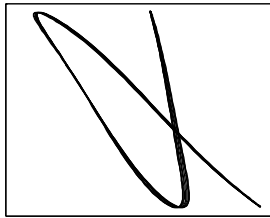
This figure can be explained with modal interactions



This figure can be explained with modal interactions

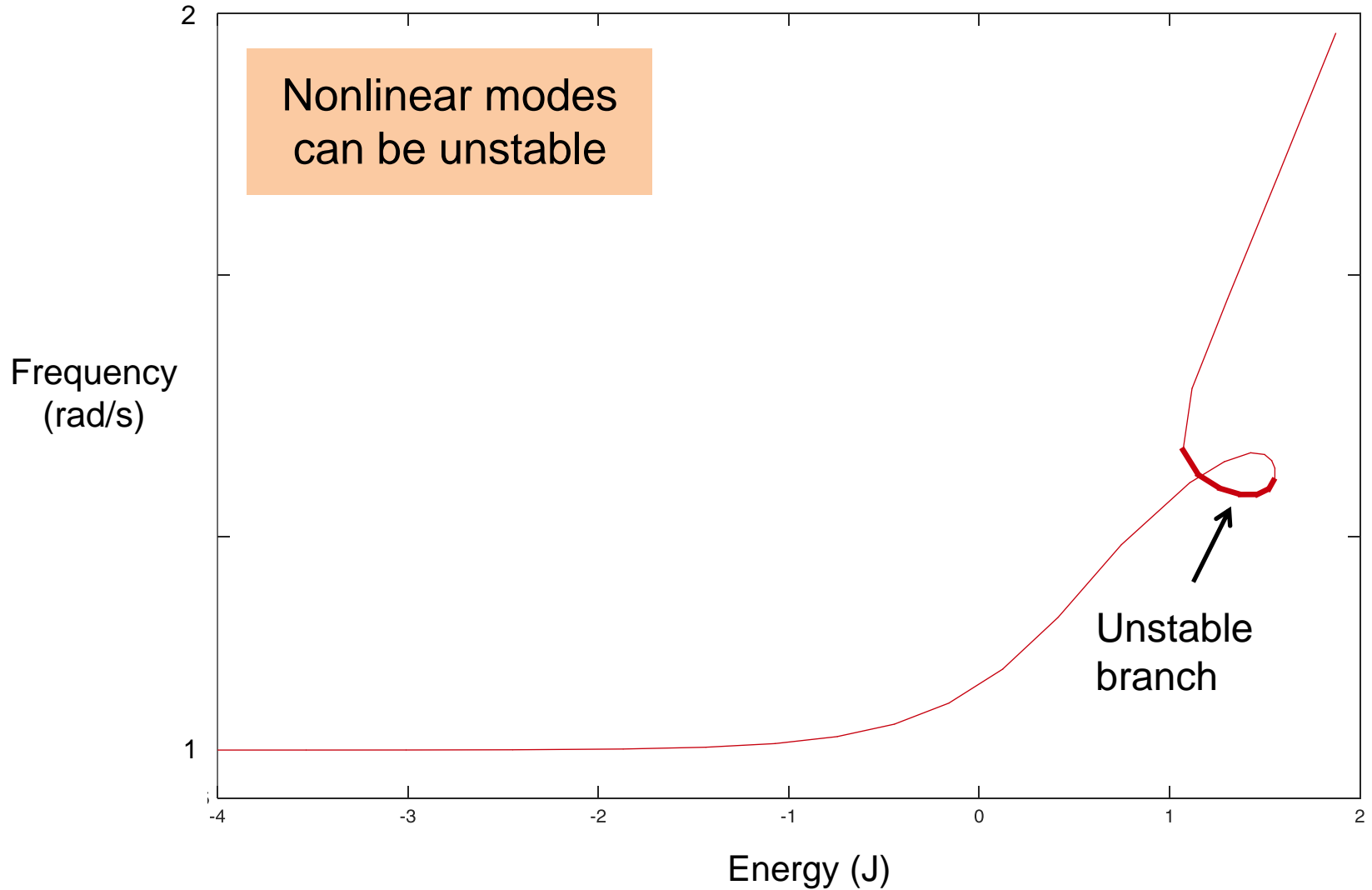


Neither abstract art nor a new alphabet



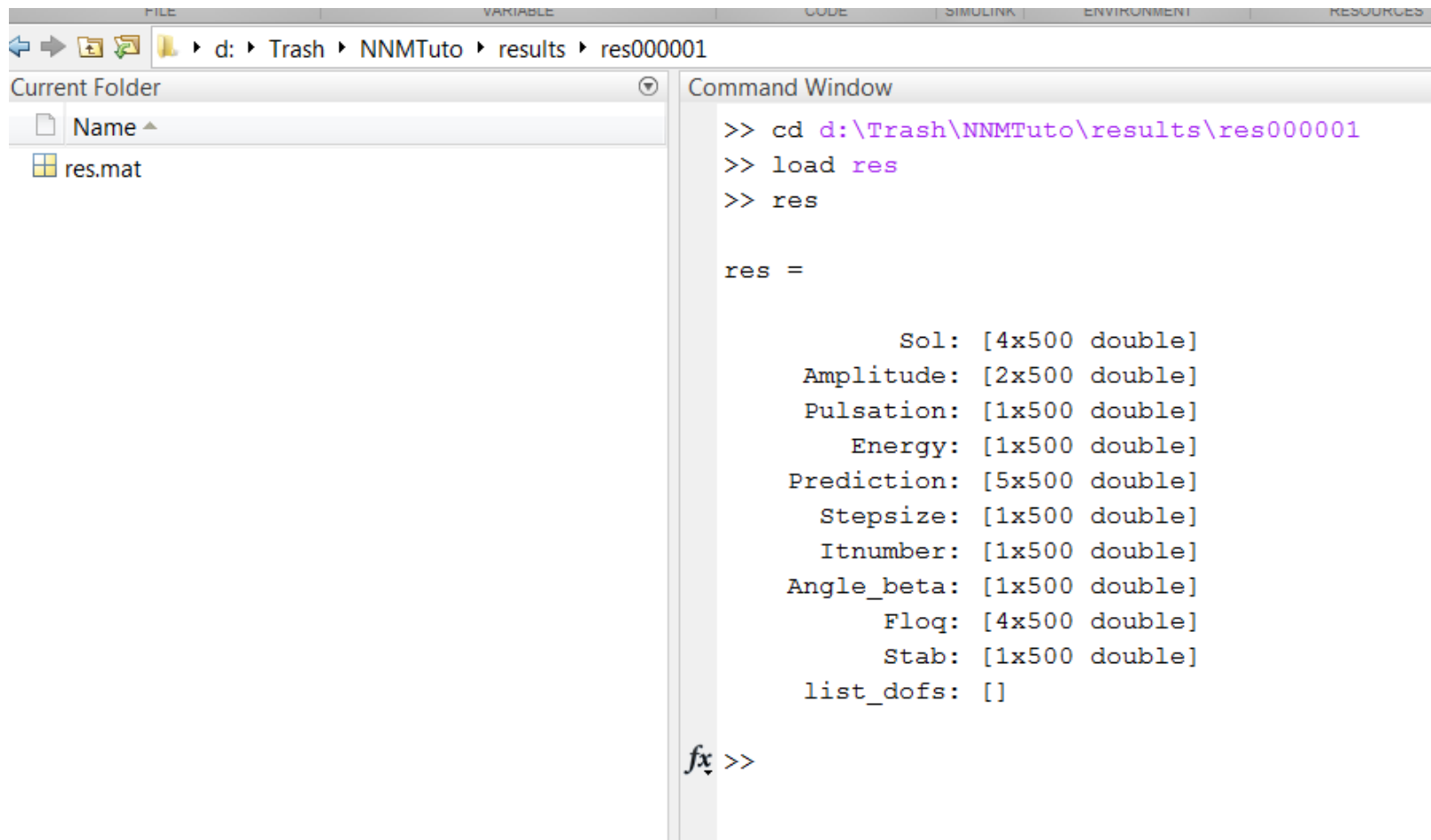
4. Stability

The in-phase mode loses stability



Let's try to investigate what's going on

Open Matlab and load the file that contains the results



The screenshot shows the MATLAB interface with the following components:

- Current Folder:** d:\Trash\NNMTuto\results\res000001. A file named `res.mat` is listed.
- Command Window:** Contains the following commands and output:

```
>> cd d:\Trash\NNMTuto\results\res000001
>> load res
>> res

res =

        Sol: [4x500 double]
  Amplitude: [2x500 double]
  Pulsation: [1x500 double]
        Energy: [1x500 double]
 Prediction: [5x500 double]
   Stepsize: [1x500 double]
   Itnumber: [1x500 double]
 Angle_beta: [1x500 double]
        Floq: [4x500 double]
        Stab: [1x500 double]
 list_dofs: []

fx >>
```

Initial conditions for an unstable mode

```
>> log10(res.Energy)
```

```
ans =
```

```
Columns 1 through 10
```

```
-4.0000 -3.5355 -3.0114 -2.4511 -1.8710 -1.4370 -1.0721 -0.7467 -0.4459 -0.1596
```

```
Columns 11 through 20
```

```
0.1225 0.4141 0.7460 1.1054 1.2869 1.4251 1.4983 1.5359 1.5526 1.5525
```

```
Columns 21 through 30
```

```
1.5215 1.4604 1.3731 1.2651 1.1511 1.0705 1.1176 1.3035 1.5701 1.8719
```

```
Columns 31 through 40
```

```
2.1140 2.3121 2.5284 2.7065 2.8575 2.9883 3.1036 3.2386 3.3569 3.4621
```

```
Columns 41 through 50
```

```
3.5862 3.6958 3.8244 3.9723 4.1396 4.2933 4.3316 4.3422 4.3508 4.3539
```

```
>> res.Sol(:,40)
```

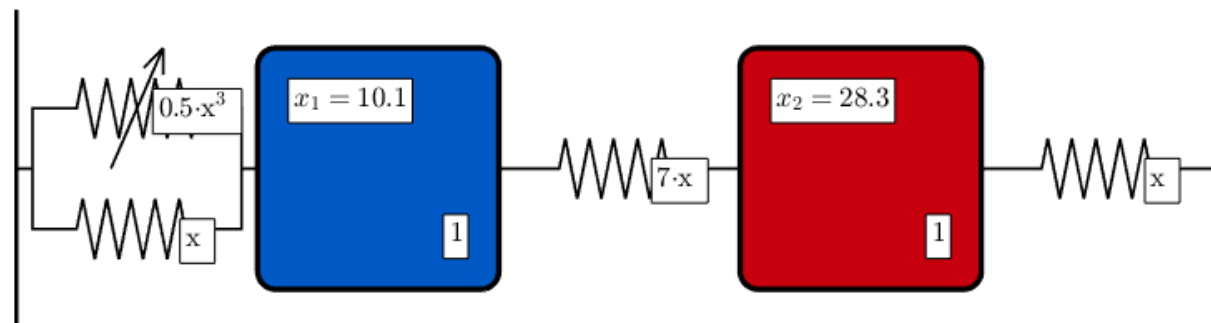
```
ans =
```

```
10.0700
```

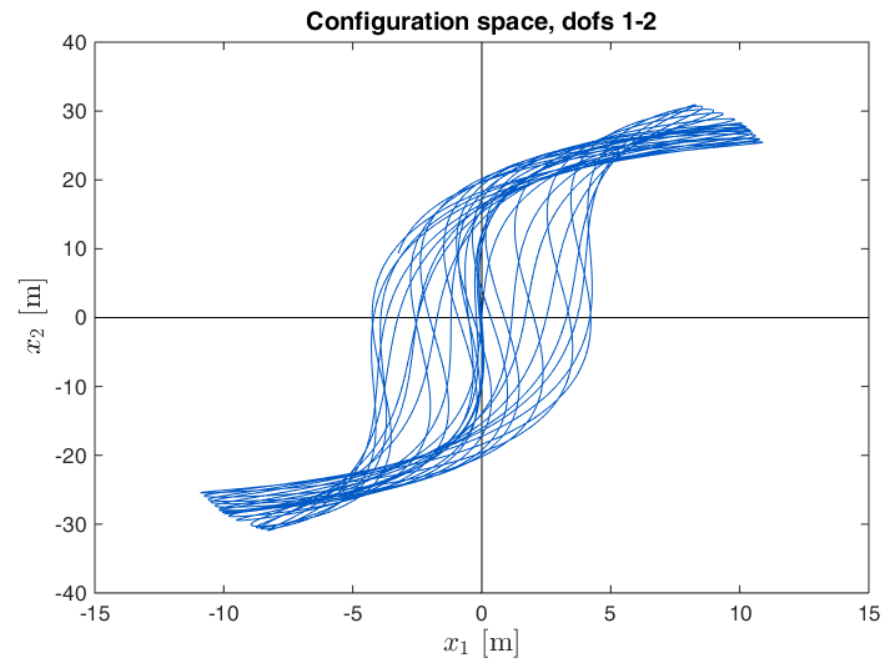
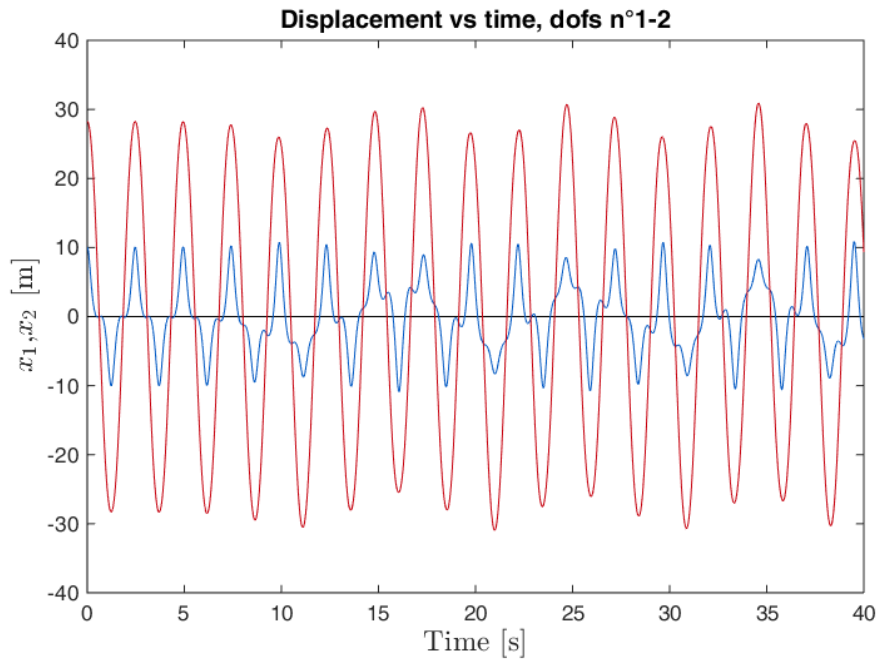
```
28.2892
```

```
0
```

```
0
```



Unstable nonlinear mode



E:\Enseignement\Cours\NonlinearVibrations\Lectures\
Matlab\L04_NNM\Simulation_Stability

Initial conditions for a stable mode

```
>> log10(res.Energy)
```

```
ans =
```

```
Columns 1 through 10
```

```
-4.0000 -3.5355 -3.0114 -2.4511 -1.8710 -1.4370 -1.0721 -0.7467 -0.4459 -0.1596
```

```
Columns 11 through 20
```

```
0.1225 0.4141 0.7460 1.1054 1.2869 1.4251 1.4983 1.5359 1.5526 1.5525
```

```
Columns 21 through 30
```

```
1.5215 1.4604 1.3731 1.2651 1.1511 1.0705 1.1176 1.3035 1.5701 1.8719
```

```
Columns 31 through 40
```

```
2.1140 2.3121 2.5284 2.7065 2.8575 2.9883 3.1036 3.2386 3.3569 3.4621
```

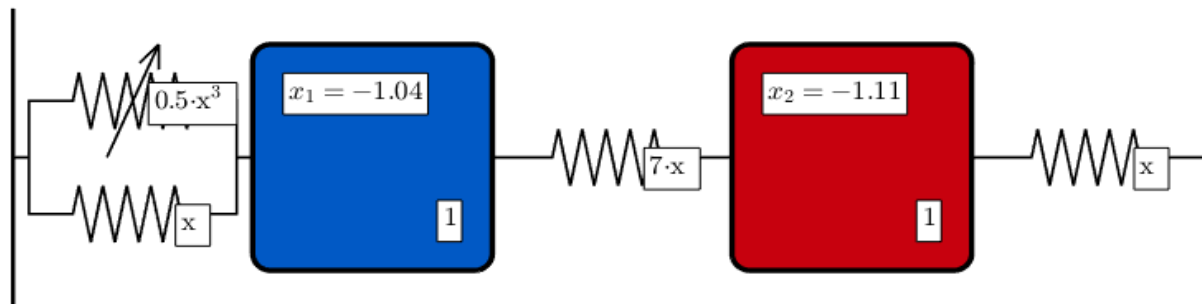
```
Columns 41 through 50
```

```
3.5862 3.6958 3.8244 3.9723 4.1396 4.2933 4.3316 4.3422 4.3508 4.3539
```

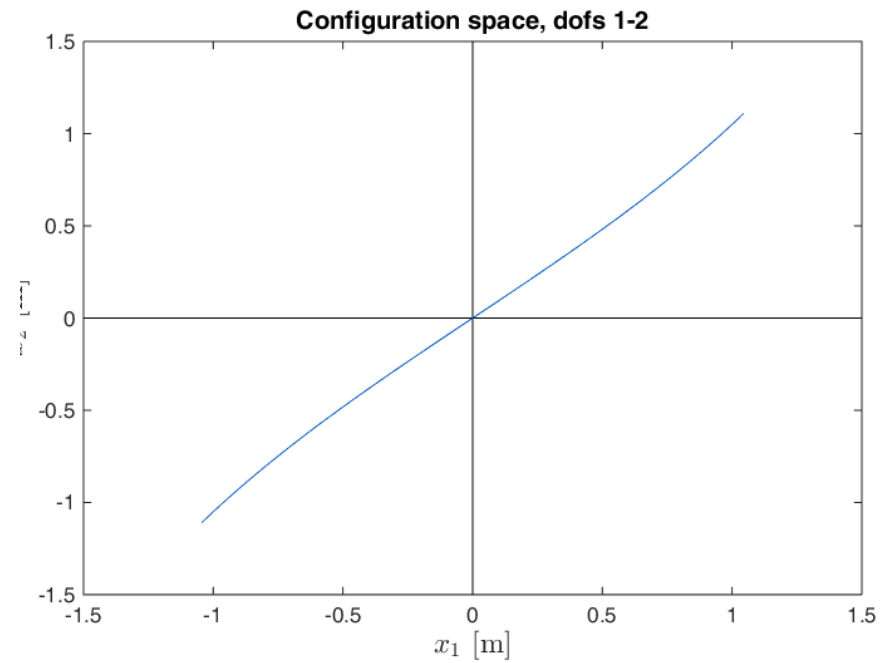
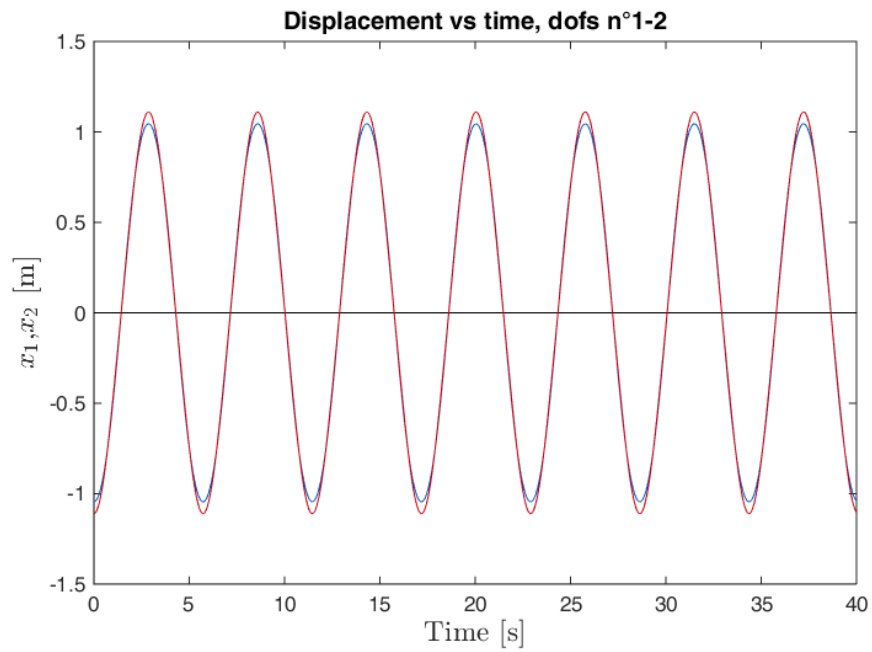
```
>> res.Sol(:,11)
```

```
ans =
```

```
-1.0449  
-1.1101  
0  
0
```



Stable mode



5. Numerical computation ?

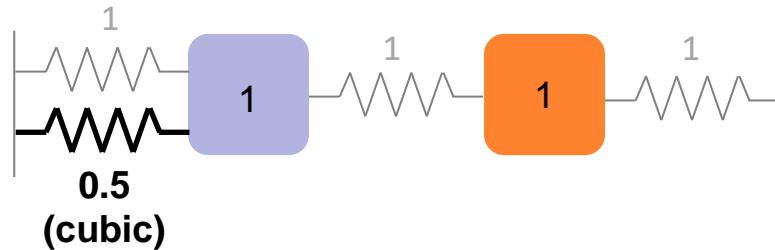
Basic idea

An nonlinear mode is a periodic motion.



1. Look for periodic solutions !

Naive approach

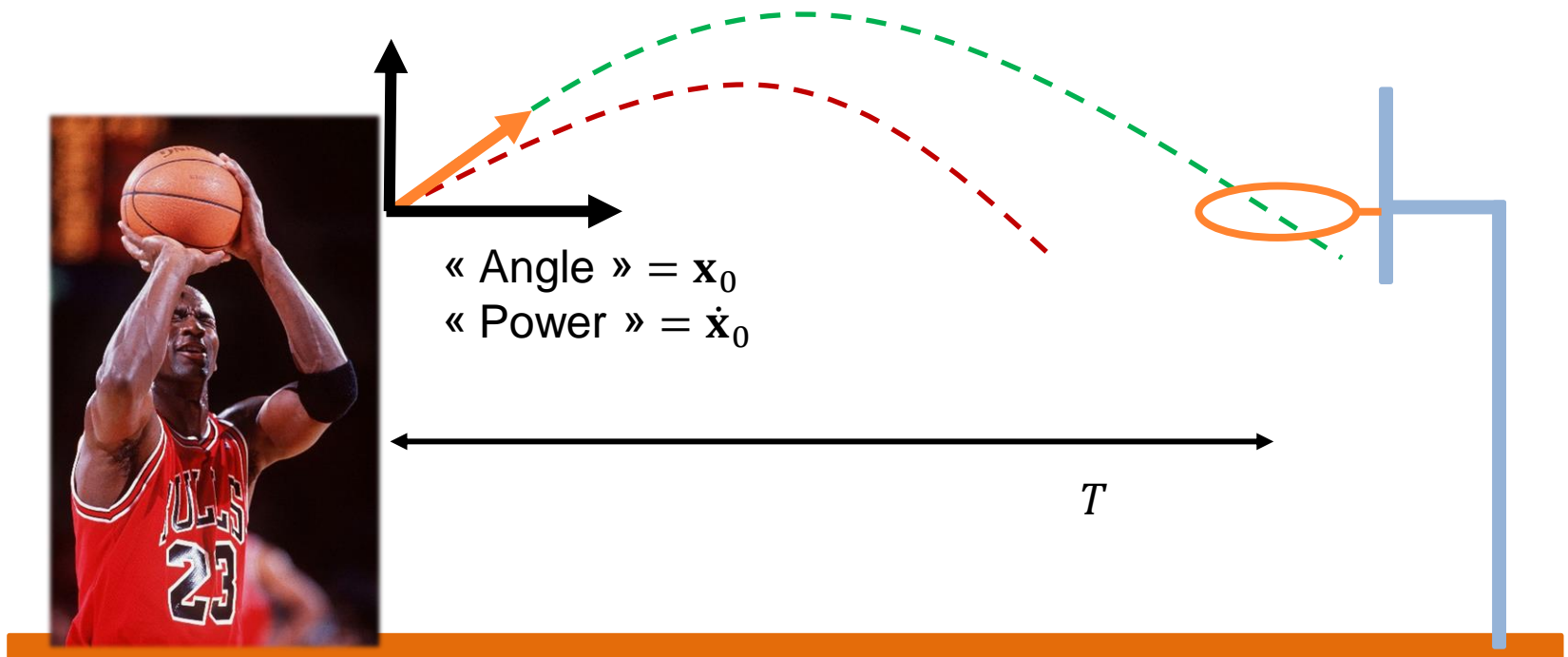


$z_0 \rightarrow z(t, z_0)$
using numerical
time integration

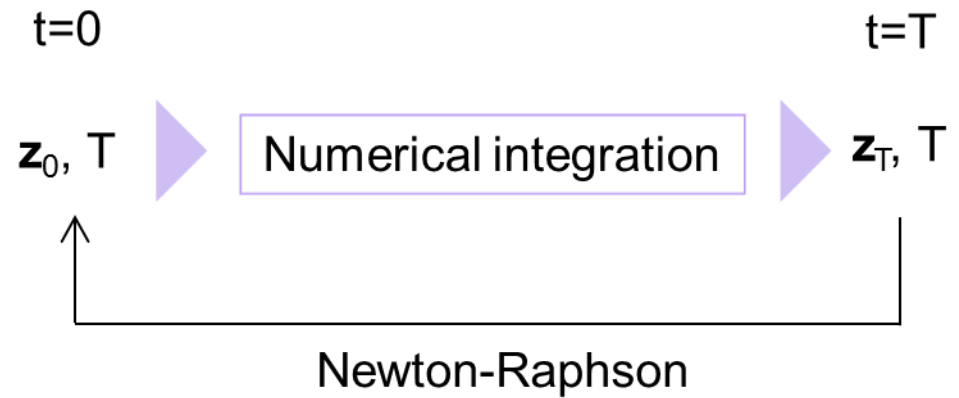
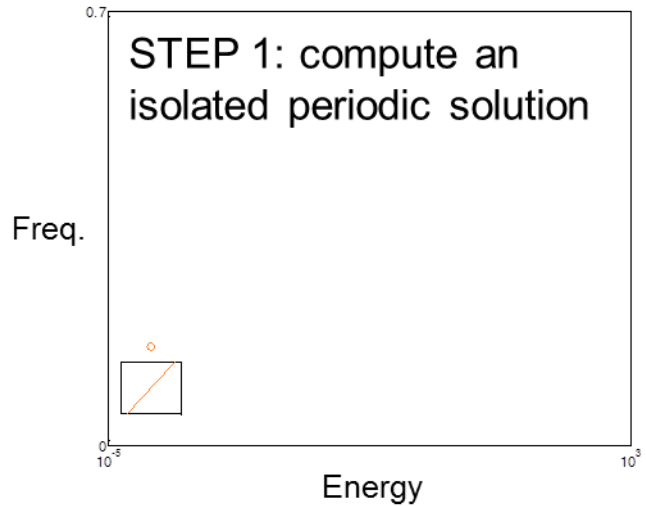
- Case 1: $x_1(0) = 1$ and $x_2(0) = 1$ \longrightarrow ~~Periodic solution~~
- Case 2: $x_1(0) = 1$ and $x_2(0) = 1.08$ \longrightarrow ~~Periodic solution~~
- Case 3: $x_1(0) = 1$ and $x_2(0) = 1.16$ \longrightarrow ~~Periodic solution~~
- Case 4: $x_1(0) = 1$ and $x_2(0) = 1.24$ \longrightarrow ~~Periodic solution~~
- Case 5: $x_1(0) = 1$ and $x_2(0) = 1.19$ \longrightarrow Periodic solution !

Shooting technique

Optimisation of the initial state of a system $[\mathbf{x}_0 \quad \dot{\mathbf{x}}_0]^T$ to obtain a periodic solution after time integration over a period T .



A more robust approach



Newton-Raphson

Example: find the zero of $f(x) = \frac{1}{2}(x - 1)^2$

$$f(x_1) = f(x_0) + \left. \frac{df(x)}{dx} \right|_{x=x_0} (x_1 - x_0) = 0$$

$$\frac{1}{2}(x_0 - 1)^2 + (x_0 - 1)(x_1 - x_0) = 0$$

$$x_1 = x_0 + \frac{-\frac{1}{2}(x_0 - 1)^2}{(x_0 - 1)} = x_0 - \frac{1}{2}(x_0 - 1) = \frac{x_0 + 1}{2}$$

$$x_{j+1} = \frac{x_j + 1}{2}$$

Matlab: homemade or fsolve

```
function NewtonRaphsonIllustration

clear all;close all;clc

plot([-3:0.01:3],0.5*([-3:0.01:3]-1).^2,'k',[-3:3],[0 0 0 0 0 0 0],'k--');hold on;pause

StartingPoint=-2;

while abs(0.5*(StartingPoint-1)^2)>0.0001
    plot([-3:0.01:3],0.5*(StartingPoint-1)^2+(StartingPoint-1)*([-3:0.01:3]-StartingPoint))

    StartingPoint=0.5*(StartingPoint+1),pause
end

SolutionFound=[StartingPoint 0.5*(StartingPoint-1)^2]
```

```
function FsolveIllustration

clear all;close all;clc

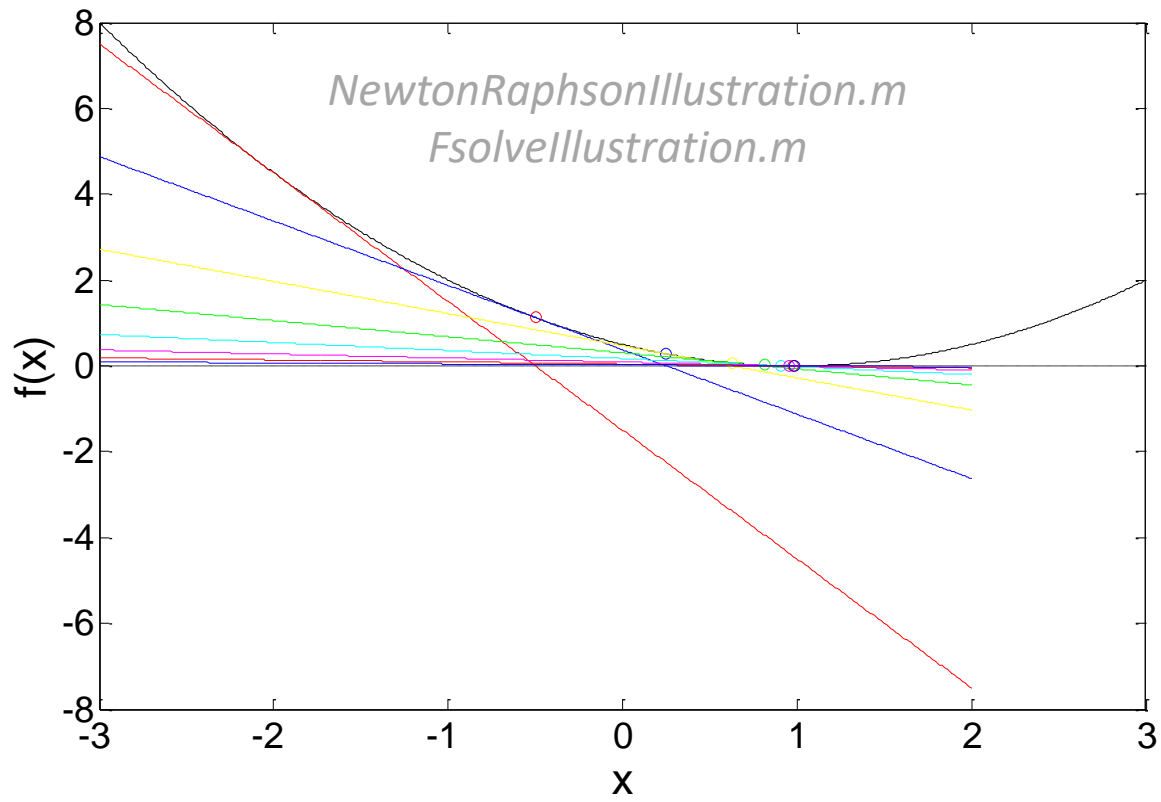
StartingPoint=-2;

SolutionFound=fsolve('Quadratic',StartingPoint)
```

```
function y=Quadratic(x)

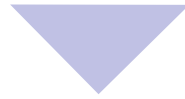
y=0.5*(x-1)^2
```


Result



State space formulation

$$M\ddot{x}(t) + Kx(t) + f_{nl}\{x(t), \dot{x}(t)\} = 0$$



$$\dot{z} = g(z, t)$$

State-space form

$$z^T = [x^T \quad \dot{x}^T]$$

where

$$g(z) = \begin{bmatrix} \dot{x} \\ -M^{-1}[Kx + f_{nl}(x, \dot{x})] \end{bmatrix}$$

Shooting algorithm

$$\mathbf{H}(\mathbf{z}_{p0}, T) \equiv \mathbf{z}_p(T, \mathbf{z}_{p0}) - \mathbf{z}_{p0} = \mathbf{0}$$

Periodicity condition
(2-point BVP)

Numerical solution through iterations:

$$\mathbf{H}(\mathbf{z}_{p0}^{(0)}, T^{(0)}) + \frac{\partial \mathbf{H}}{\partial \mathbf{z}_{p0}} \Big|_{(\mathbf{z}_{p0}^{(0)}, T^{(0)})} \Delta \mathbf{z}_{p0}^{(0)} + \frac{\partial \mathbf{H}}{\partial T} \Big|_{(\mathbf{z}_{p0}^{(0)}, T^{(0)})} \Delta T^{(0)} + \cancel{\mathbf{H}(\mathbf{z}_{p0}^{(0)}, T^{(0)})} = 0$$

$$\frac{\partial \mathbf{H}}{\partial \mathbf{z}_0}(\mathbf{z}_0, T) = \frac{\partial \mathbf{z}(t, \mathbf{z}_0)}{\partial \mathbf{z}_0} \Big|_{t=T} - \mathbf{I}$$

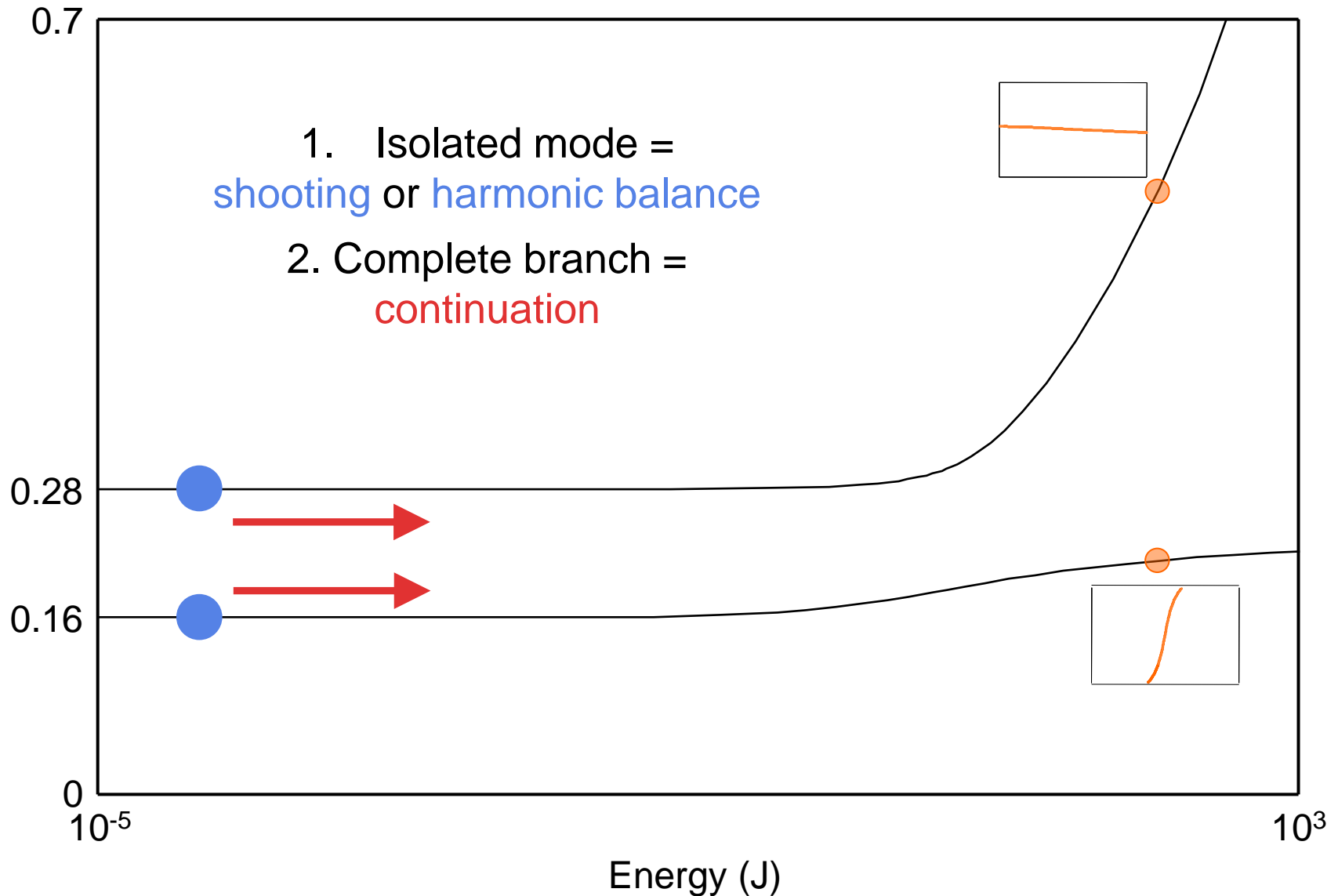
2n x 2n — Monodromy matrix

$$\begin{aligned} \frac{\partial \mathbf{H}}{\partial T}(\mathbf{z}_0, T) &= \frac{\partial \mathbf{z}(t, \mathbf{z}_0)}{\partial t} \Big|_{t=T} \\ &= \mathbf{g}(\mathbf{z}(T, \mathbf{z}_0)) \end{aligned}$$

2n x 1

Combining shooting with continuation

Frequency (Hz)



Nonlinear normal modes, Part II: Toward a practical computation using numerical continuation techniques

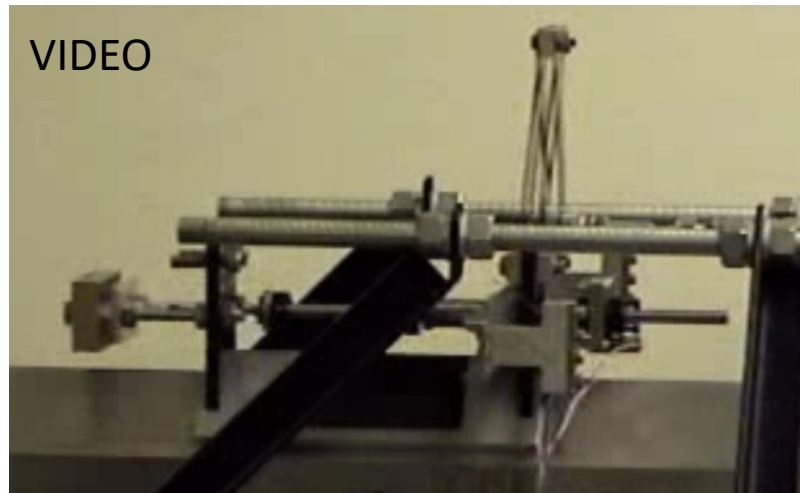
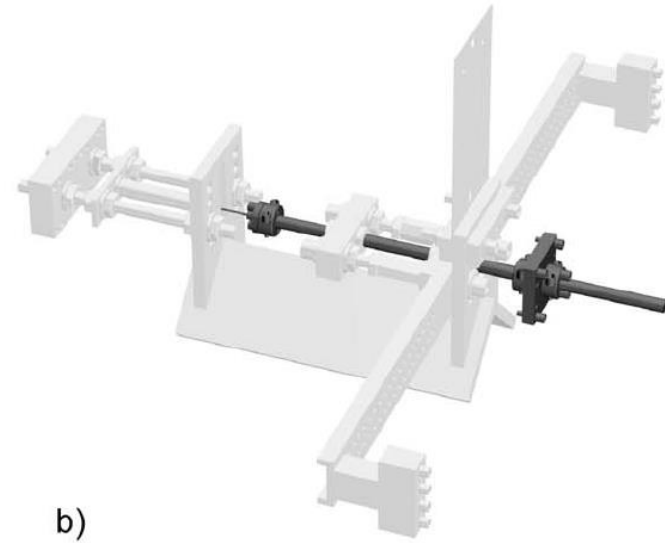
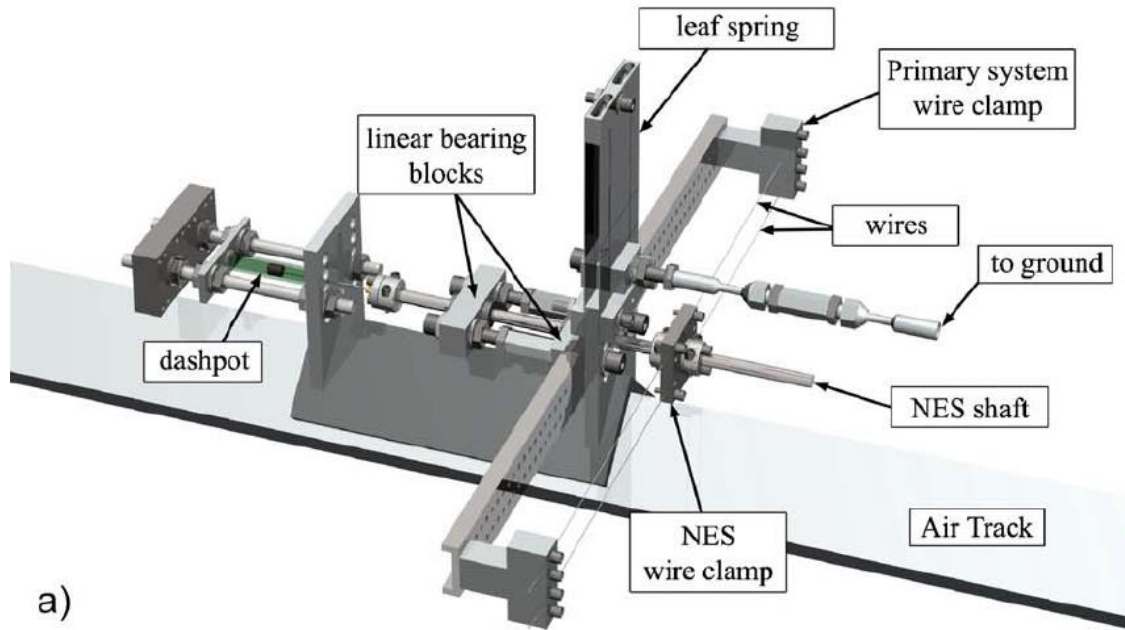
M. Peeters, R. Viguié, G. Sérandour, G. Kerschen *, J.-C. Golinval

*Structural Dynamics Research Group, Department of Aerospace and Mechanical Engineering, University of Liège,
1 Chemin des Chevreuils (B52/3), B-4000 Liège, Belgium*

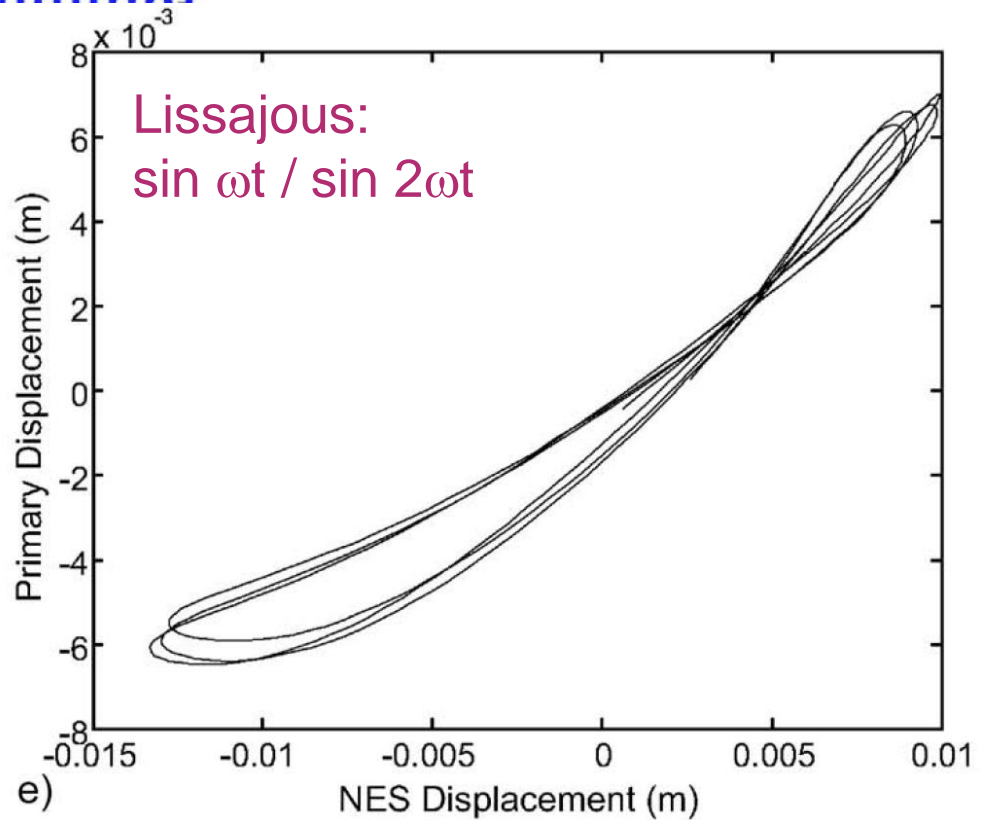
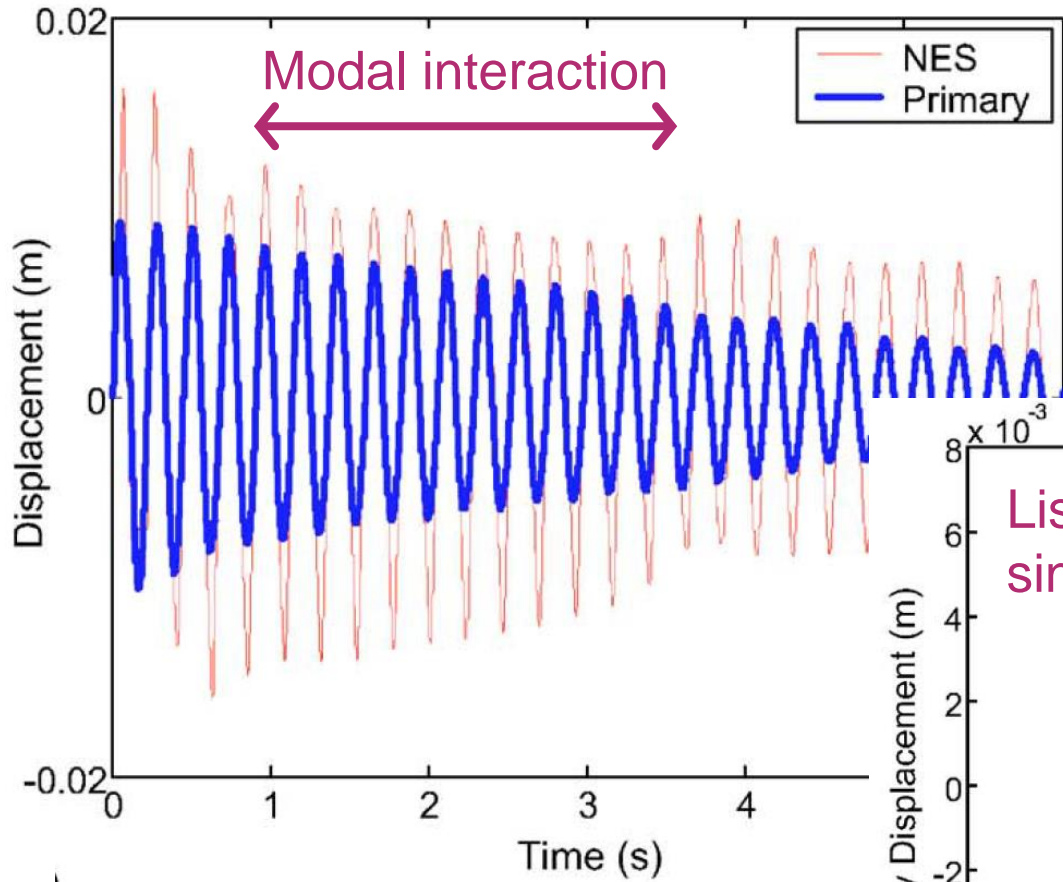
Mechanical Systems and Signal Processing 23 (2009) 195–216

6. Existence ?

Do modal interactions exist in reality ?

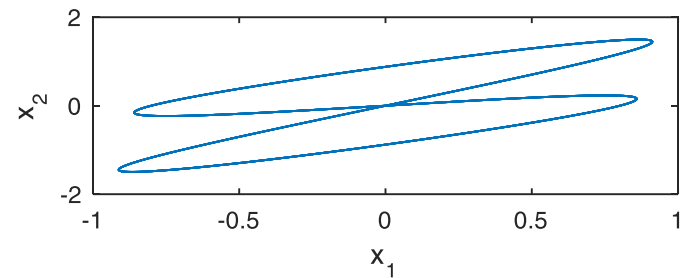
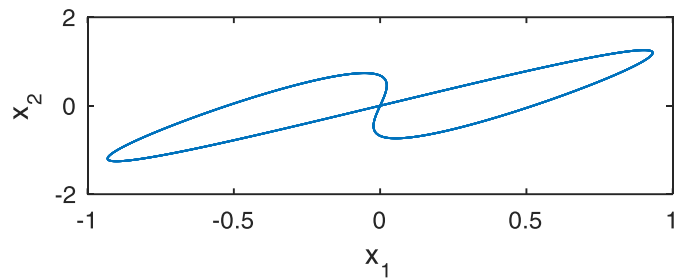
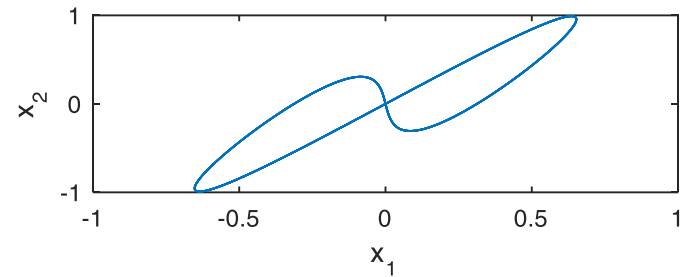
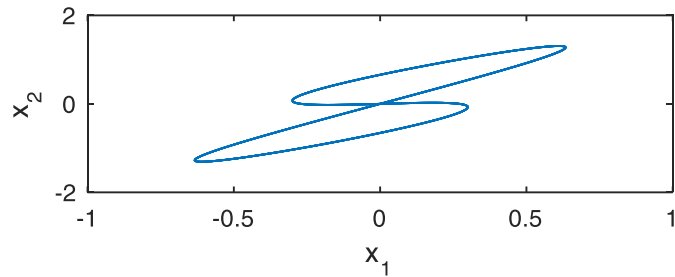
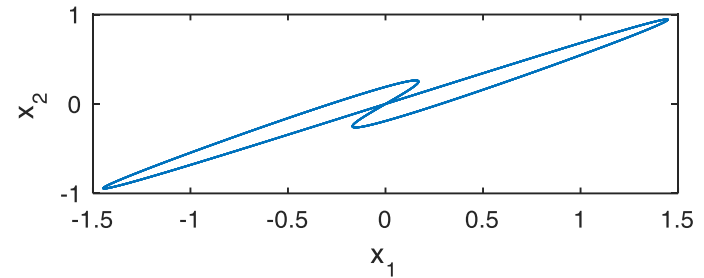
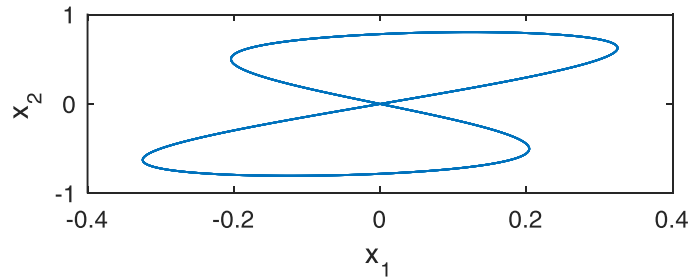


It seems



Lissajous curves...

```
>> LissajousNNM  
1=sin/sin 2=cos/cos: 1  
Enter harmonics 1:1  
Enter harmonics 2:2
```

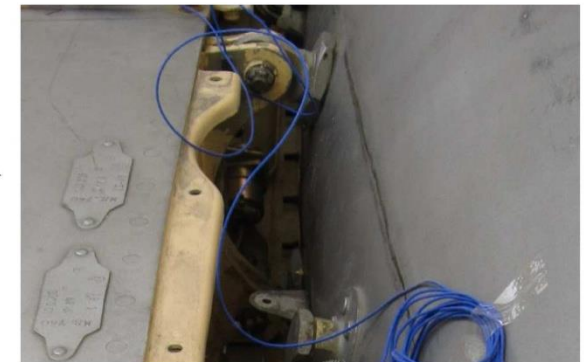
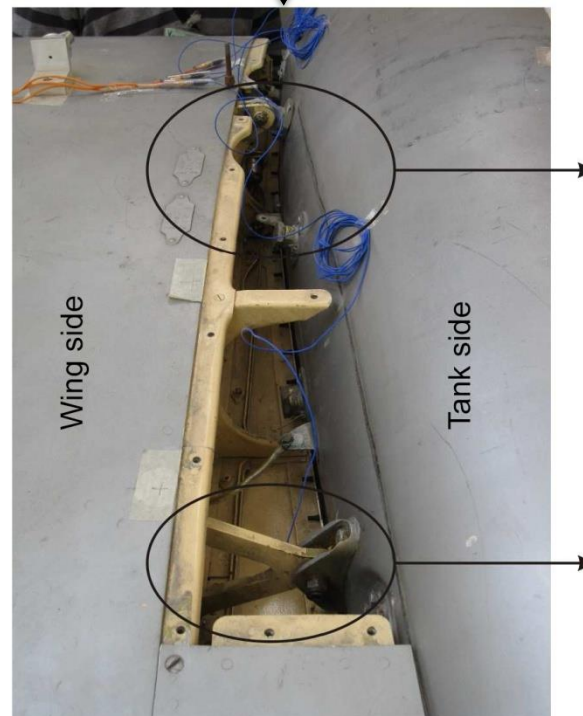


Do they exist in complex systems ?



Bolted connections
between external fuel
tank and wing tip

Front connection



Rear connection



The testing campaign



IMG_1679.avi



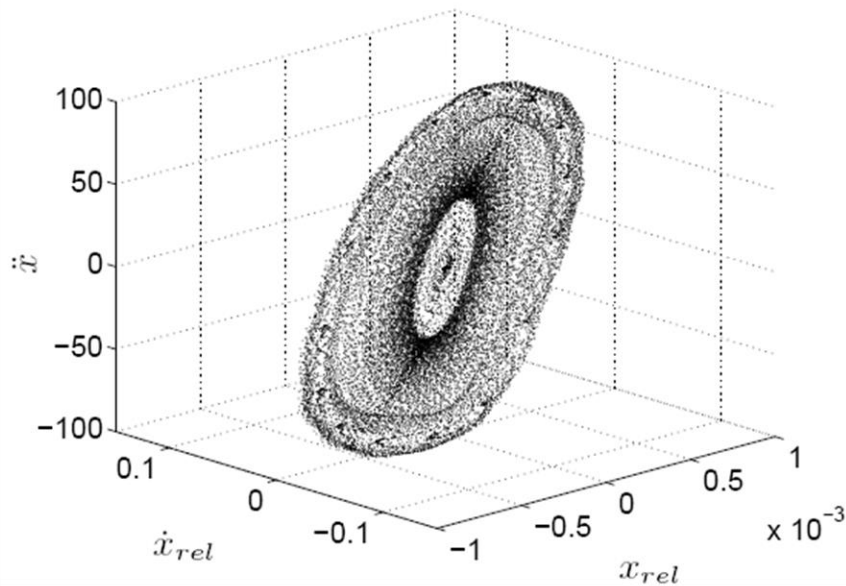
IMG_1680.MOV

Softening nonlinearity in the bolted connections

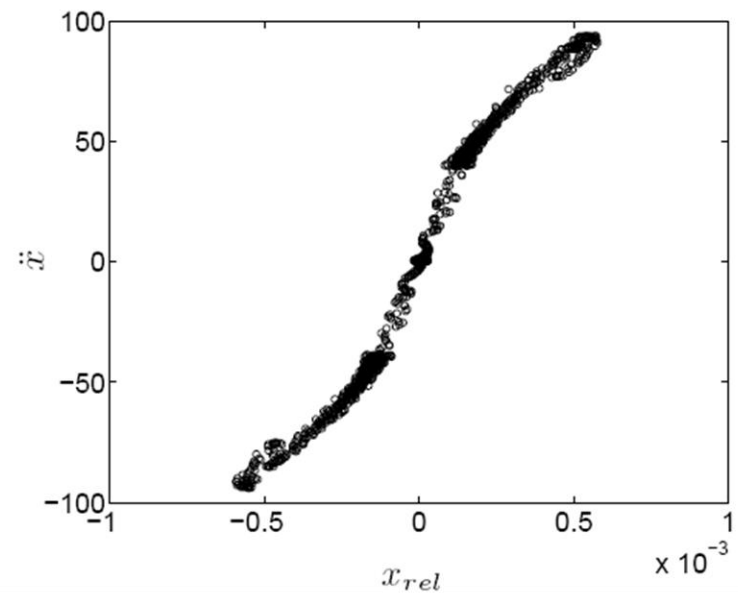


Swept sine testing

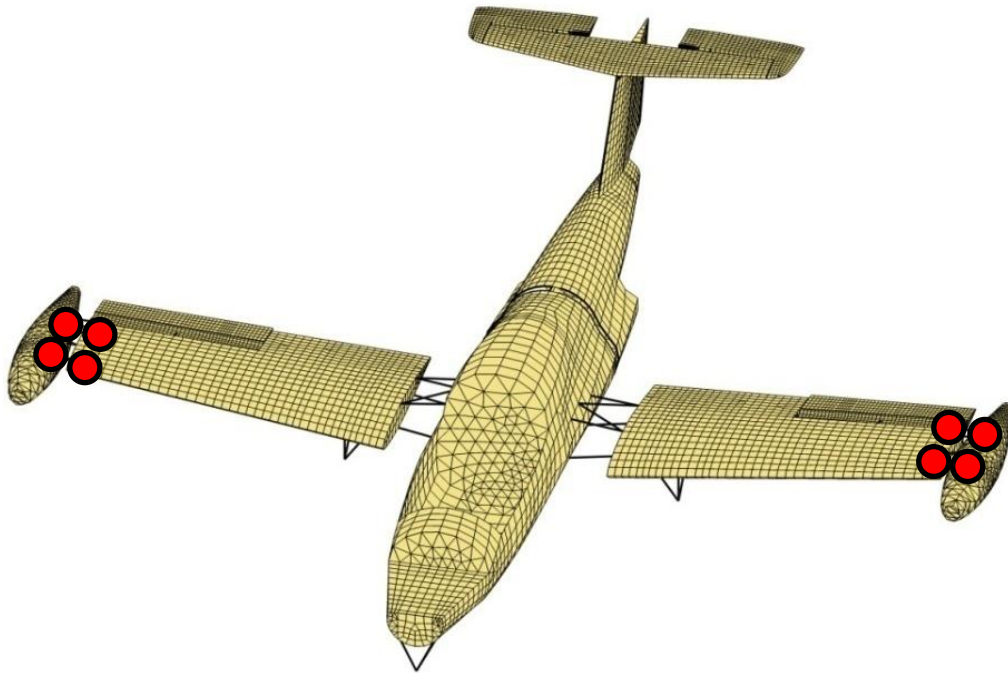
Acceleration surface method



Stiffness curve



Finite element model reduction



Finite element model
(2D shells and beams, 85000 DOFs)

Condensation of the linear components of the model



Craig-Bampton technique

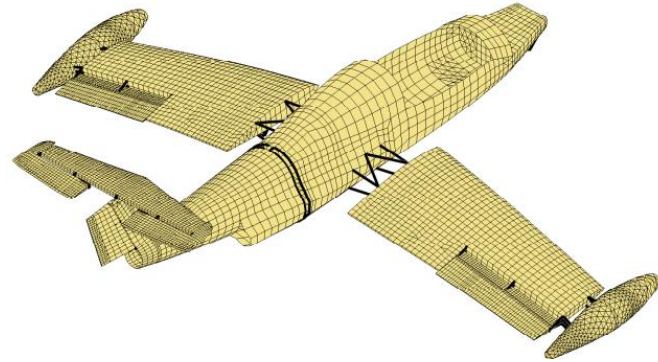
- ▶ 8 remaining nodes
- ▶ 500 internal modes



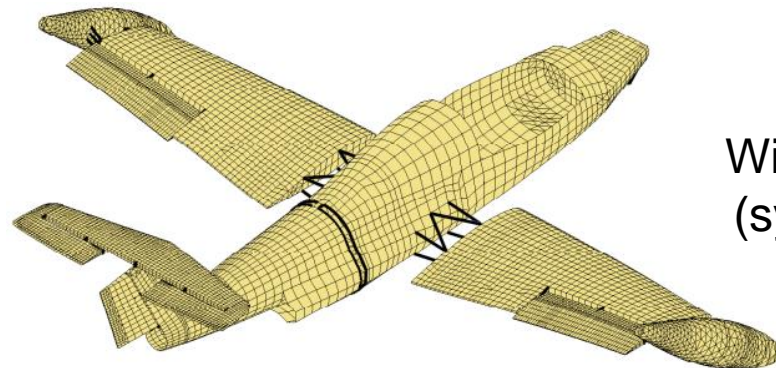
Reduced model accurate
in [0-100] Hz, 548 DOFs

A close look at two modes

Mode	Freq. (Hz)	Mode	Freq. (Hz)
1	0.0936	13	21.2193
2	0.7260	14	22.7619
3	0.9606	15	23.6525
4	1.2118	16	25.8667
5	1.2153	17	28.2679
6	1.7951	18	29.3309
7	2.1072	19	31.0847
8	2.5157	20	34.9151
9	3.5736	21	39.5169
10	8.1913	22	40.8516
11	9.8644	23	47.3547
12	16.1790	24	52.1404



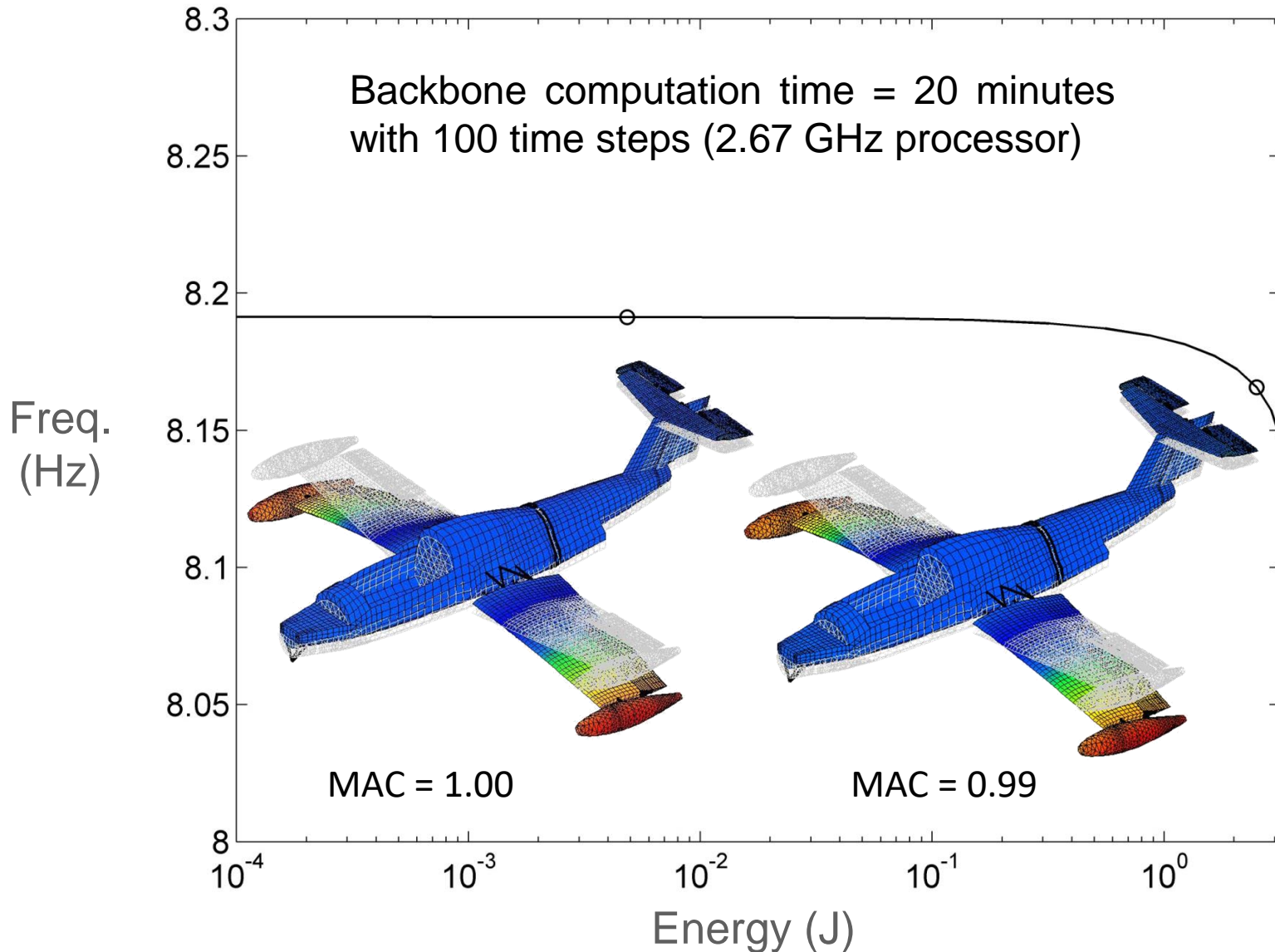
Wing bending



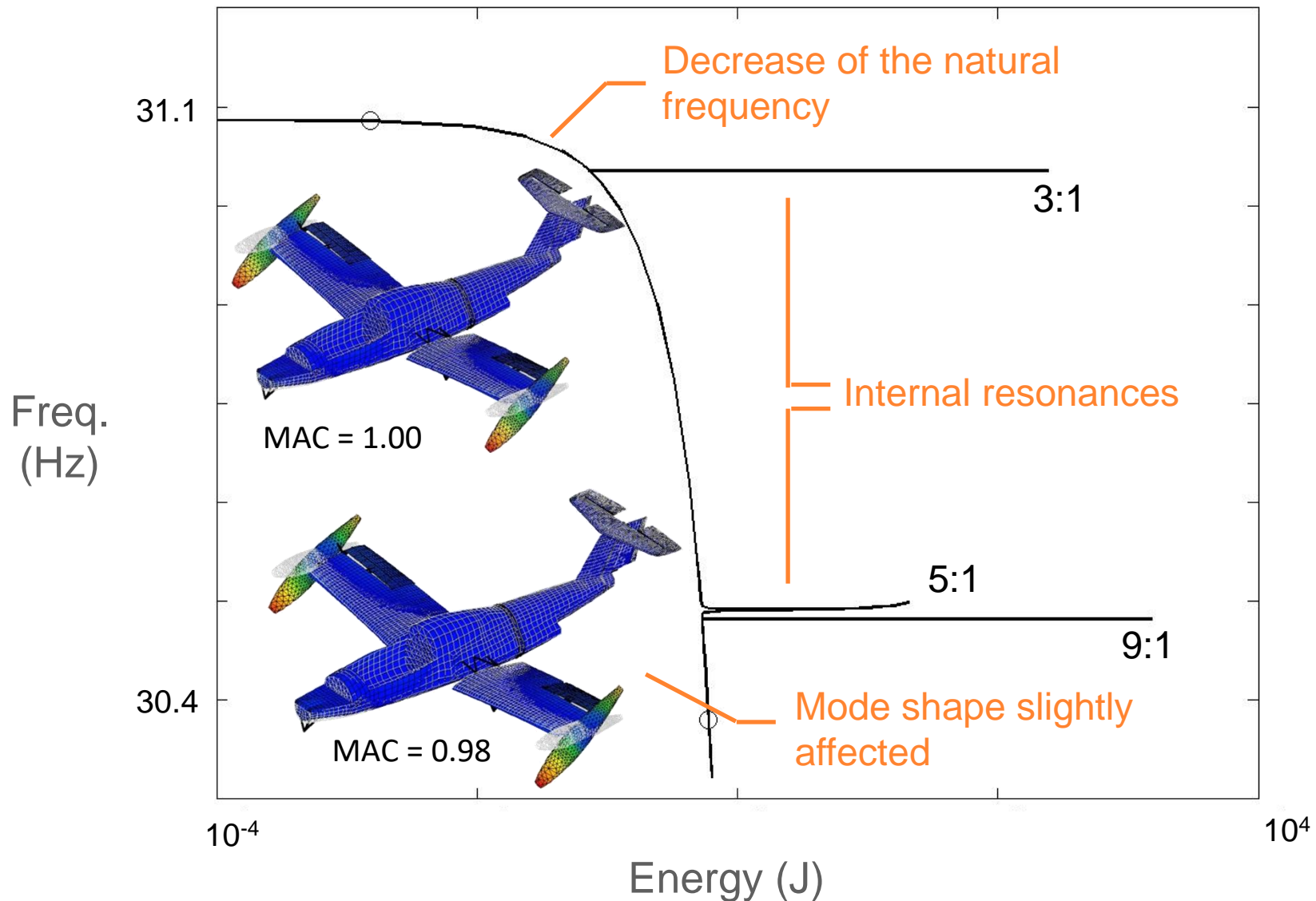
Wing torsion (symmetric)

The first wing bending mode is not affected

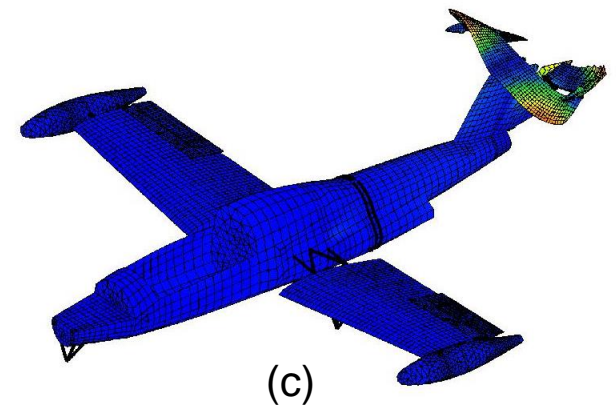
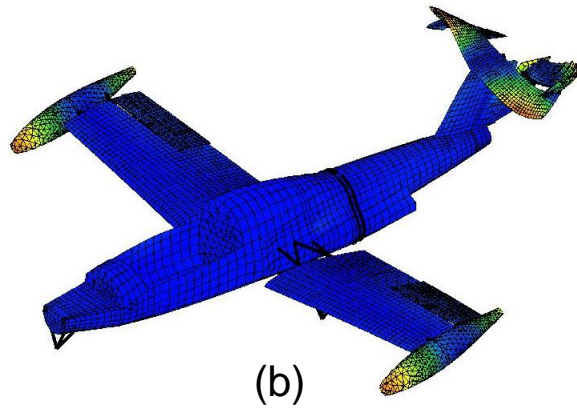
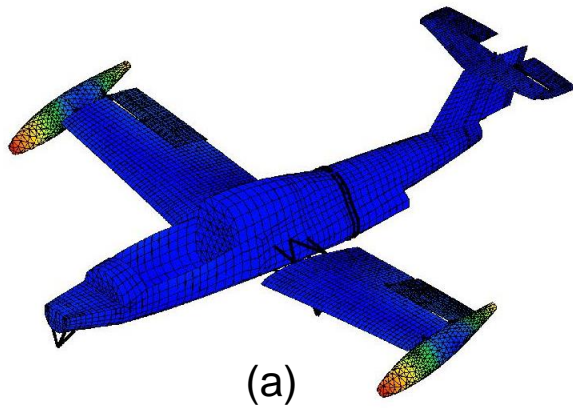
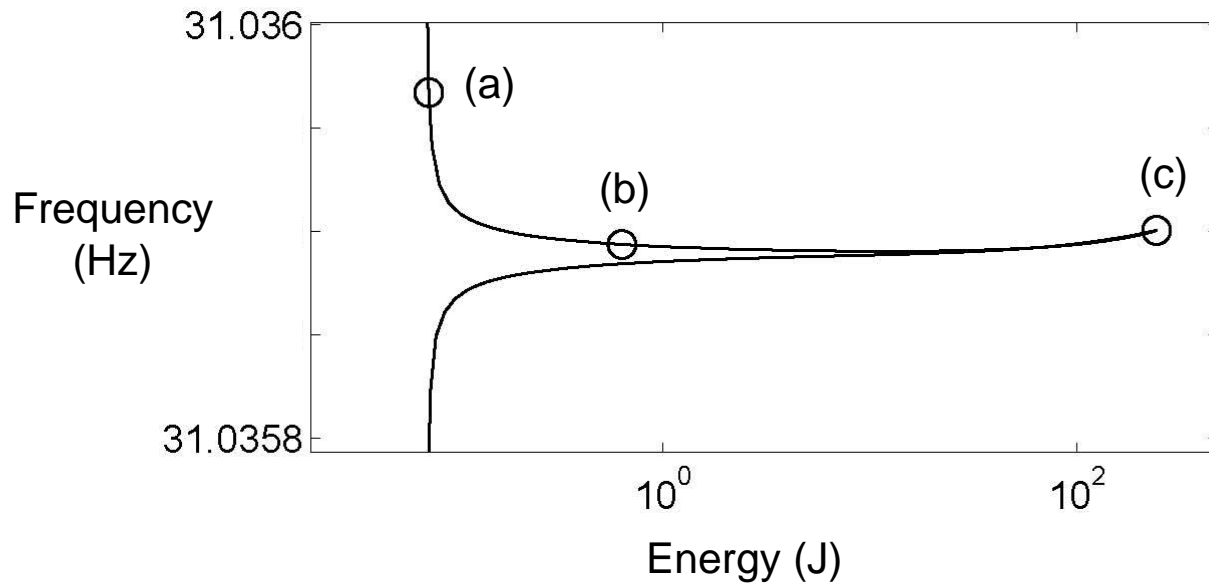
E:\NI2D\Marketing\DemosToolbox\Aircraft_ONERA\NNMcont



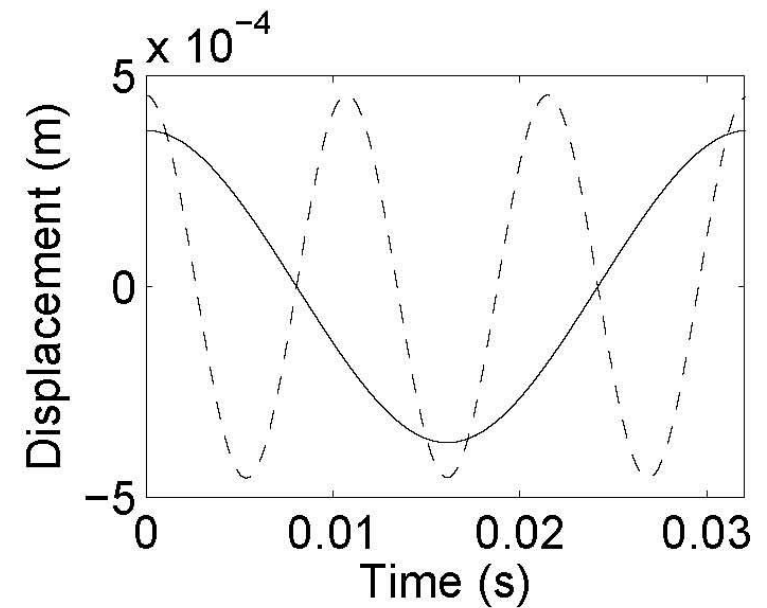
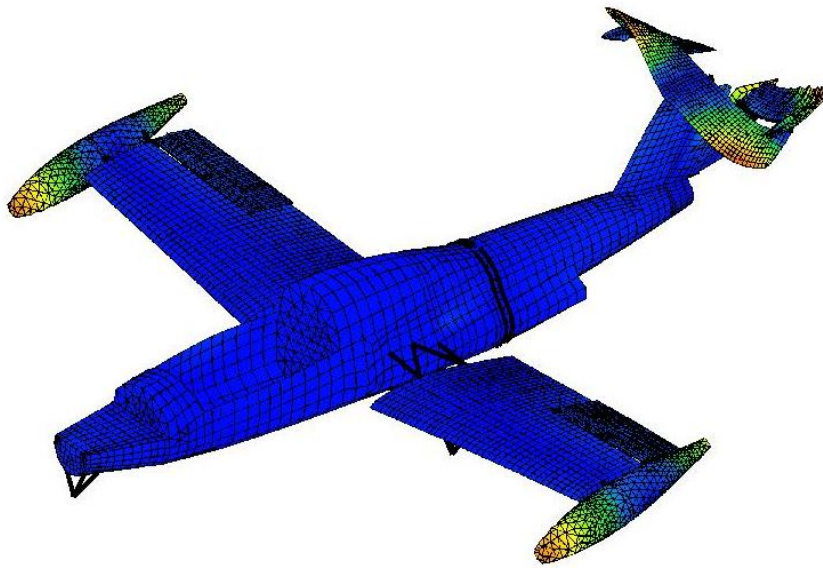
The first wing torsional mode is nonlinear



Close-up of the 3:1 modal interaction

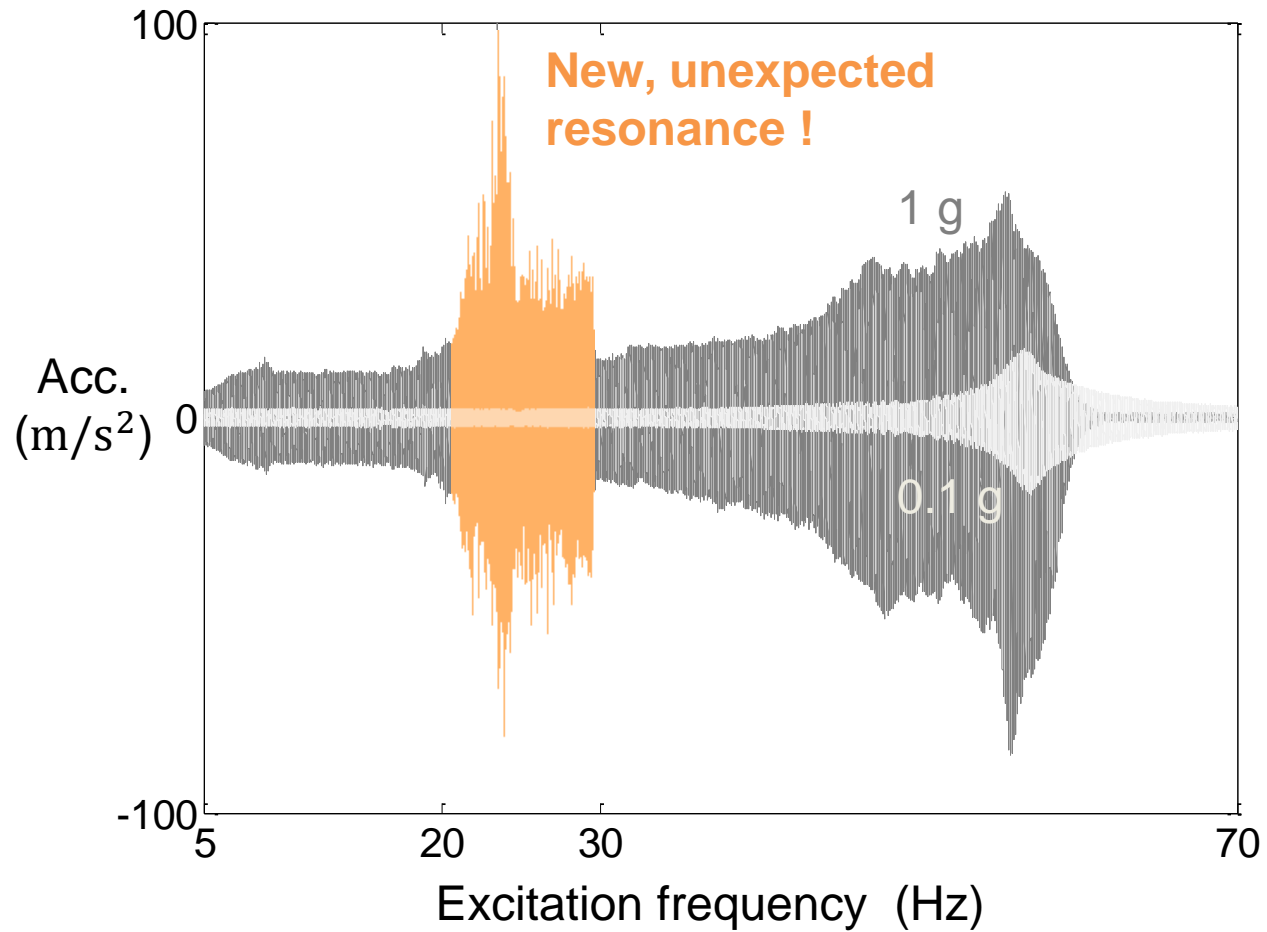
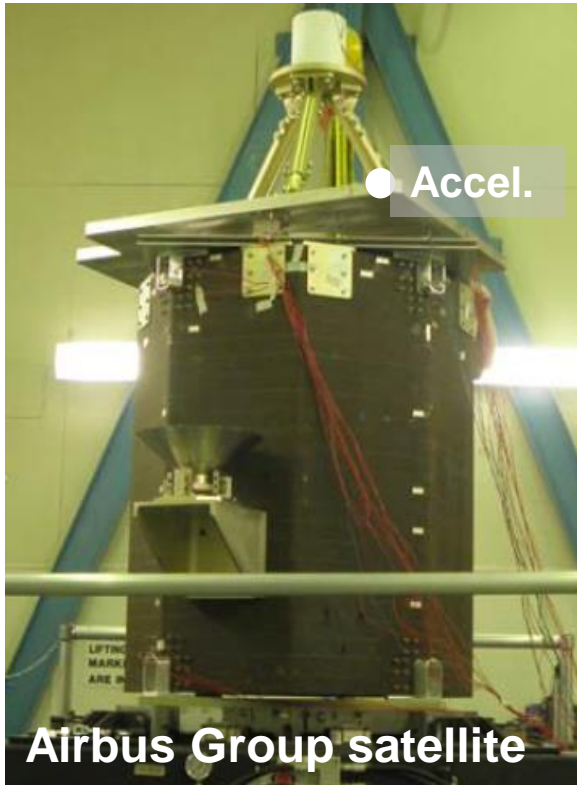


No resemblance with any linear mode

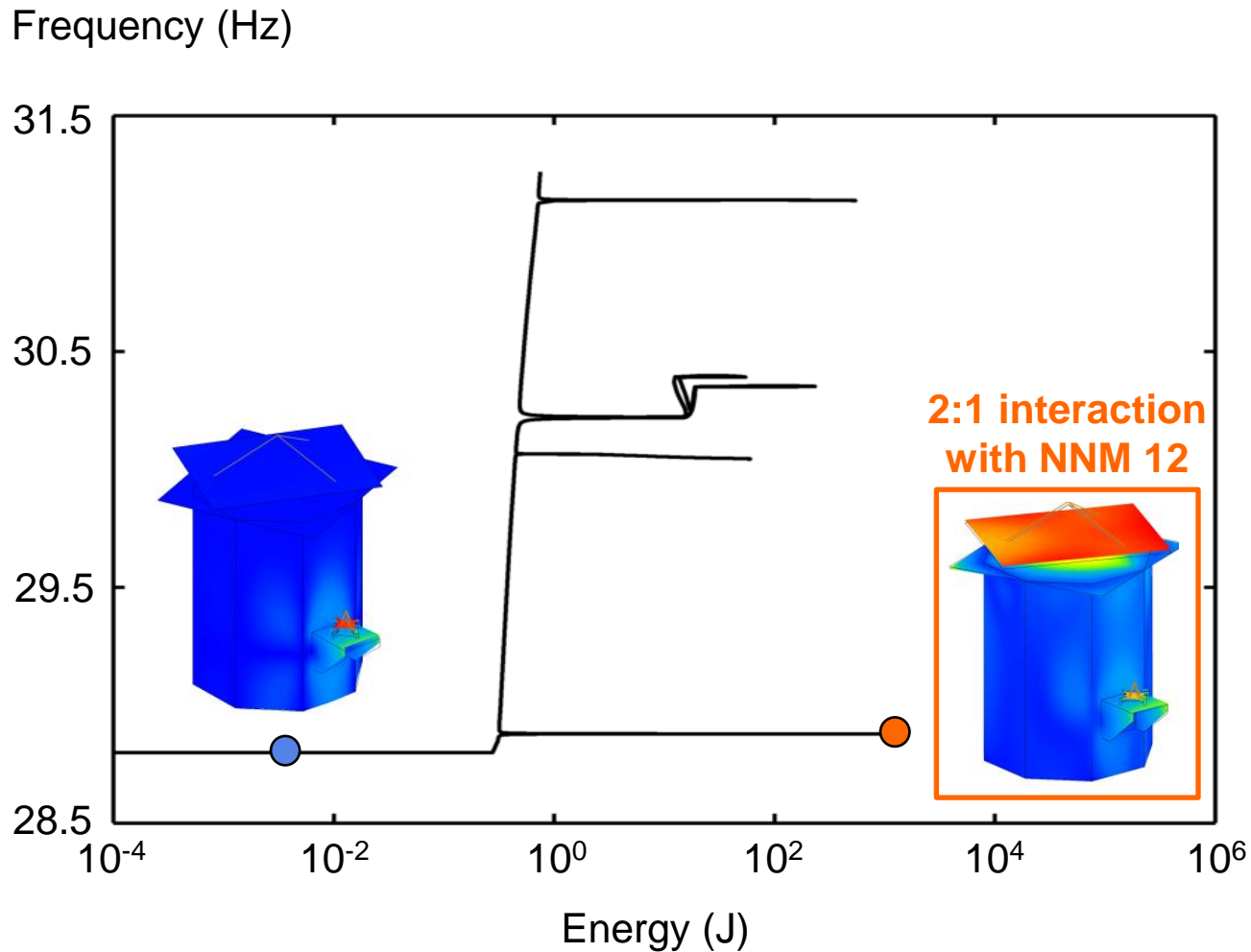


—— Tank tip - - - - Horizontal tail

A dangerous nonlinear resonance



It can be predicted using an updated FEM



In summary

Clear physical meaning

LNMs

NNMs

Structural deformation at resonance

YES

YES

Synchronous vibration of the structure

YES

YES, BUT...

Important mathematical properties

Orthogonality

YES

NO

Modal superposition

YES

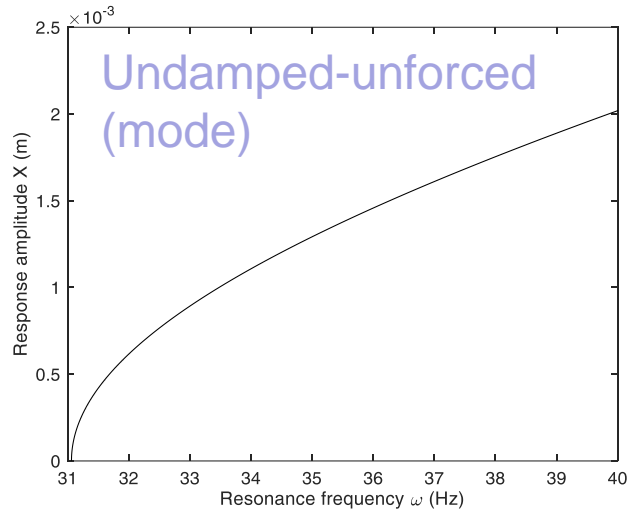
NO

Key lessons learned

1. Frequency-amplitude/energy dependence
2. Harmonics
3. Bifurcations (additional resonances)
4. Stability

! Both for FRCs and modes !

Nonlinear modes and FRFs



+

=

