Nonlinear Vibrations of Aerospace Structures

University of Liège, Belgium

L01 Introduction

Course objectives

Review of linear theory

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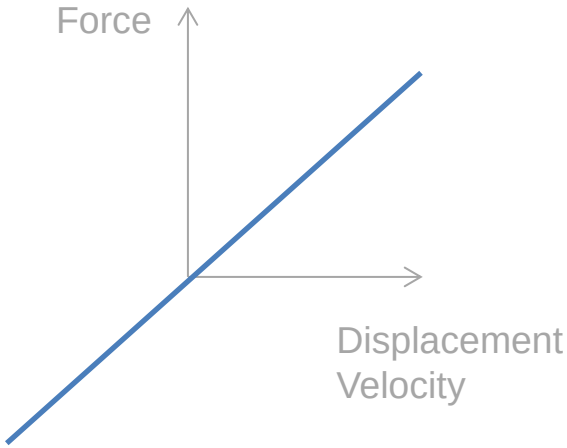
Course details:

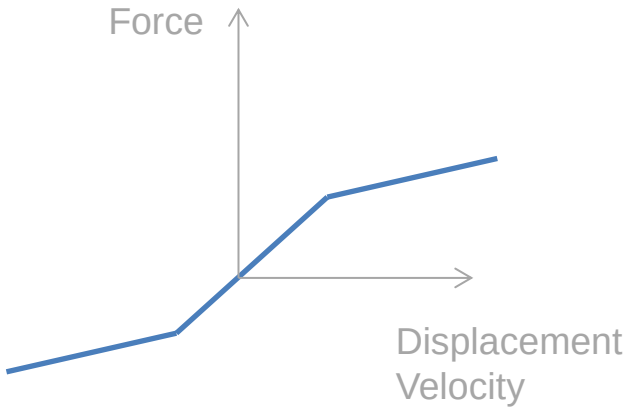
- http://www.s3l.be

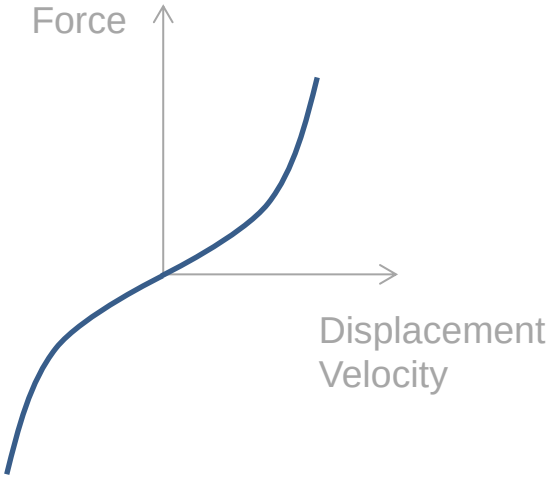
What Is a Nonlinearity ?

LINEAR

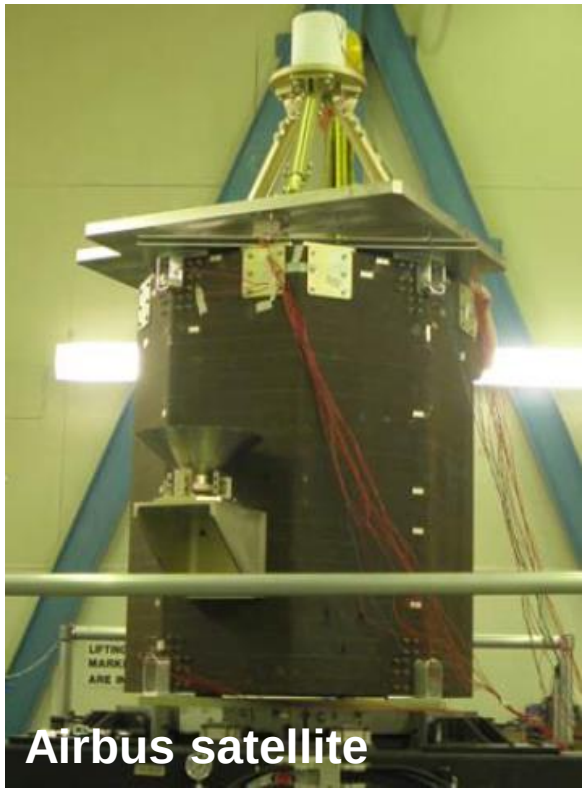


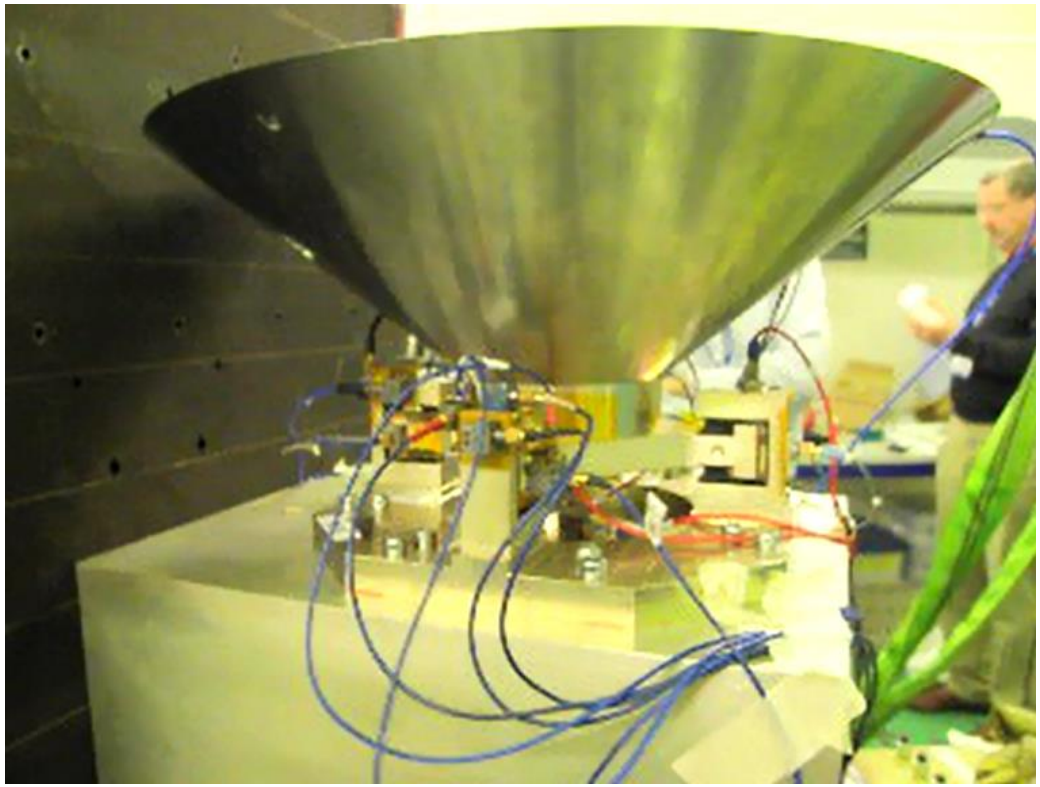
NONLINEARITY





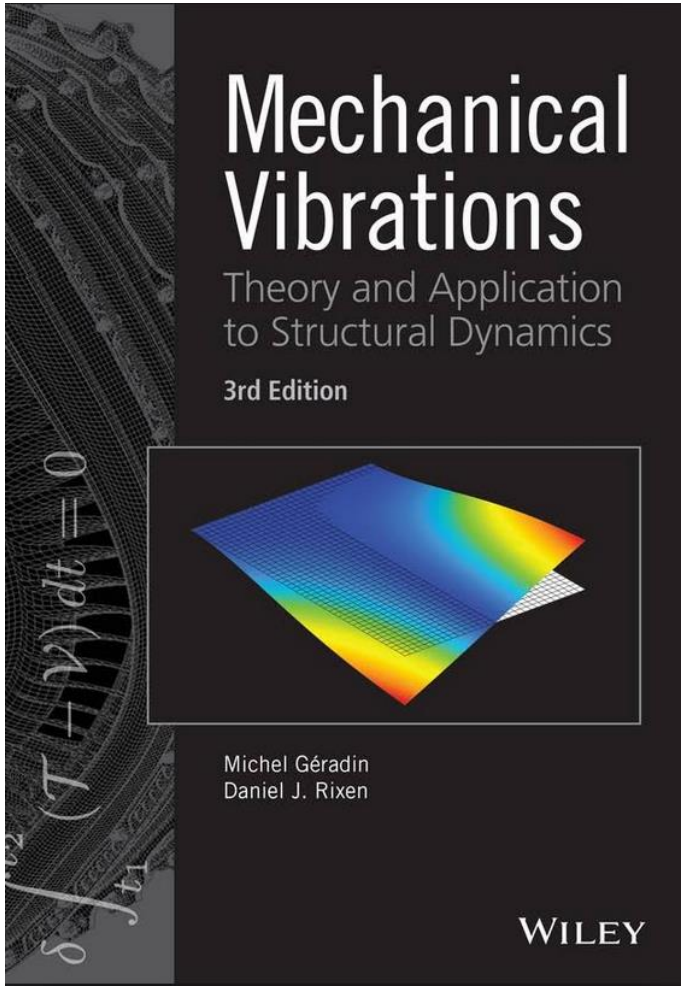
What Is a Nonlinear Vibration ?



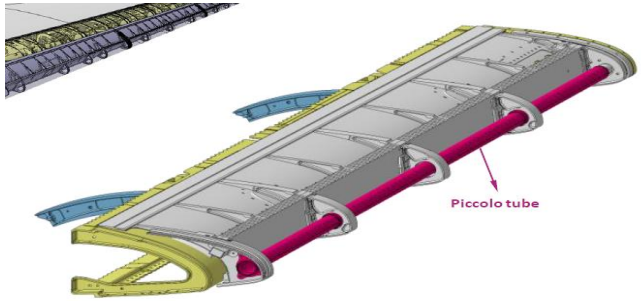


Course Motivation

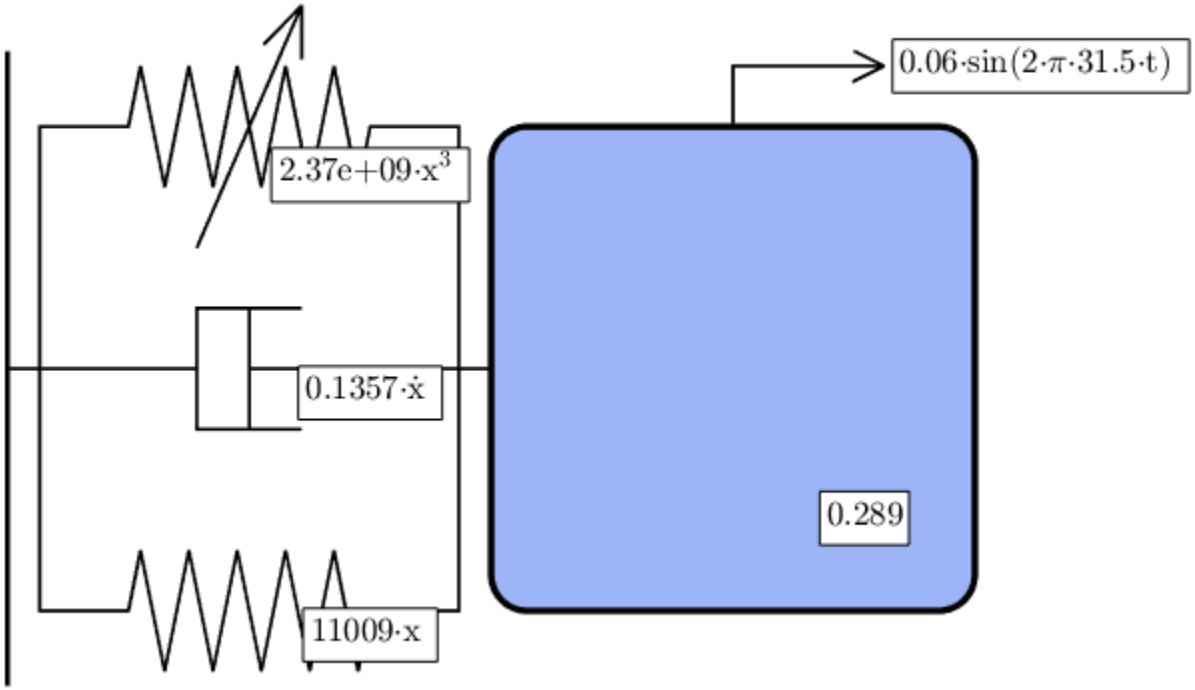
THEORETICAL STANDPOINT



PRACTICAL STANDPOINT



It Is Nonlinear, So What ?



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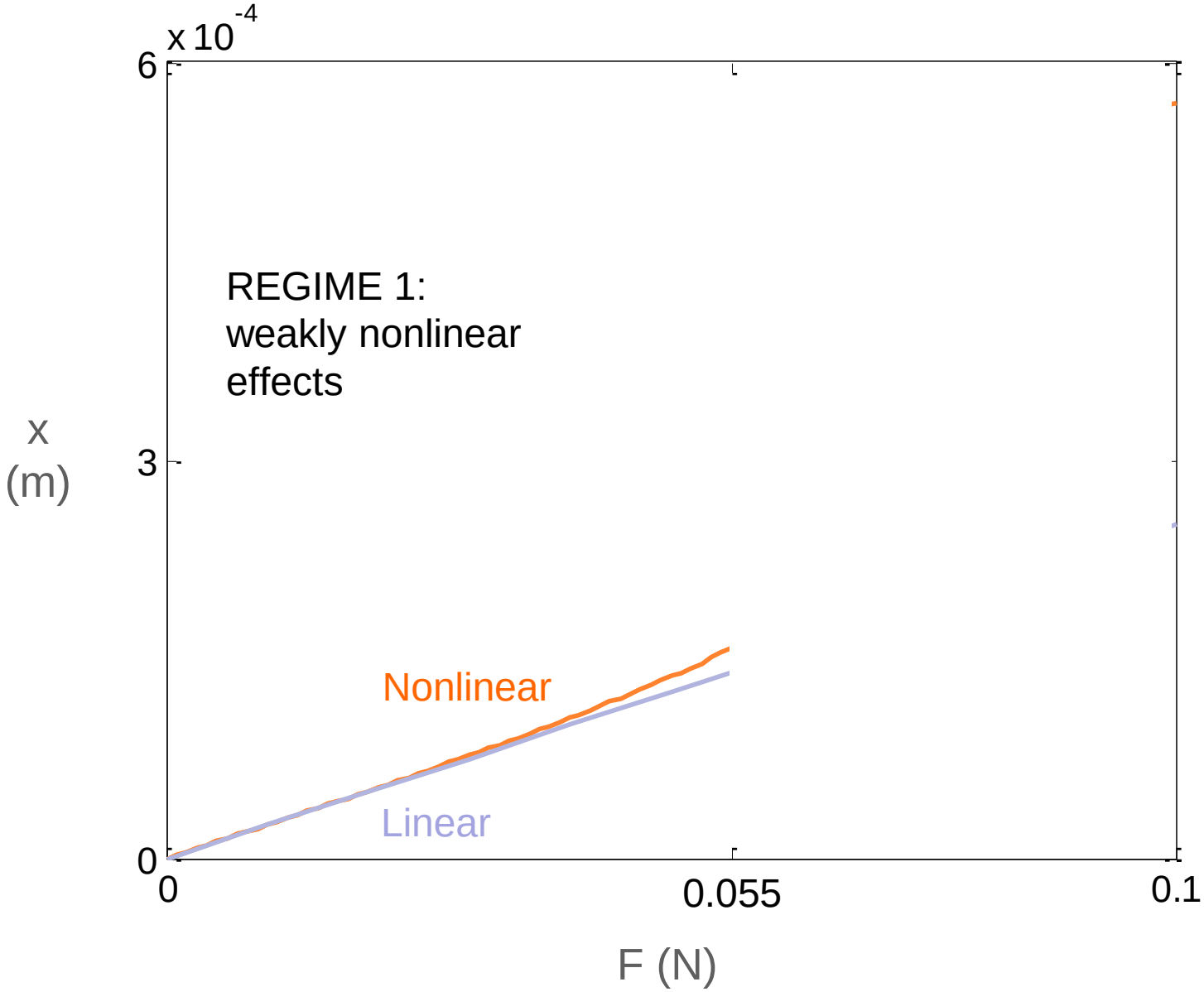

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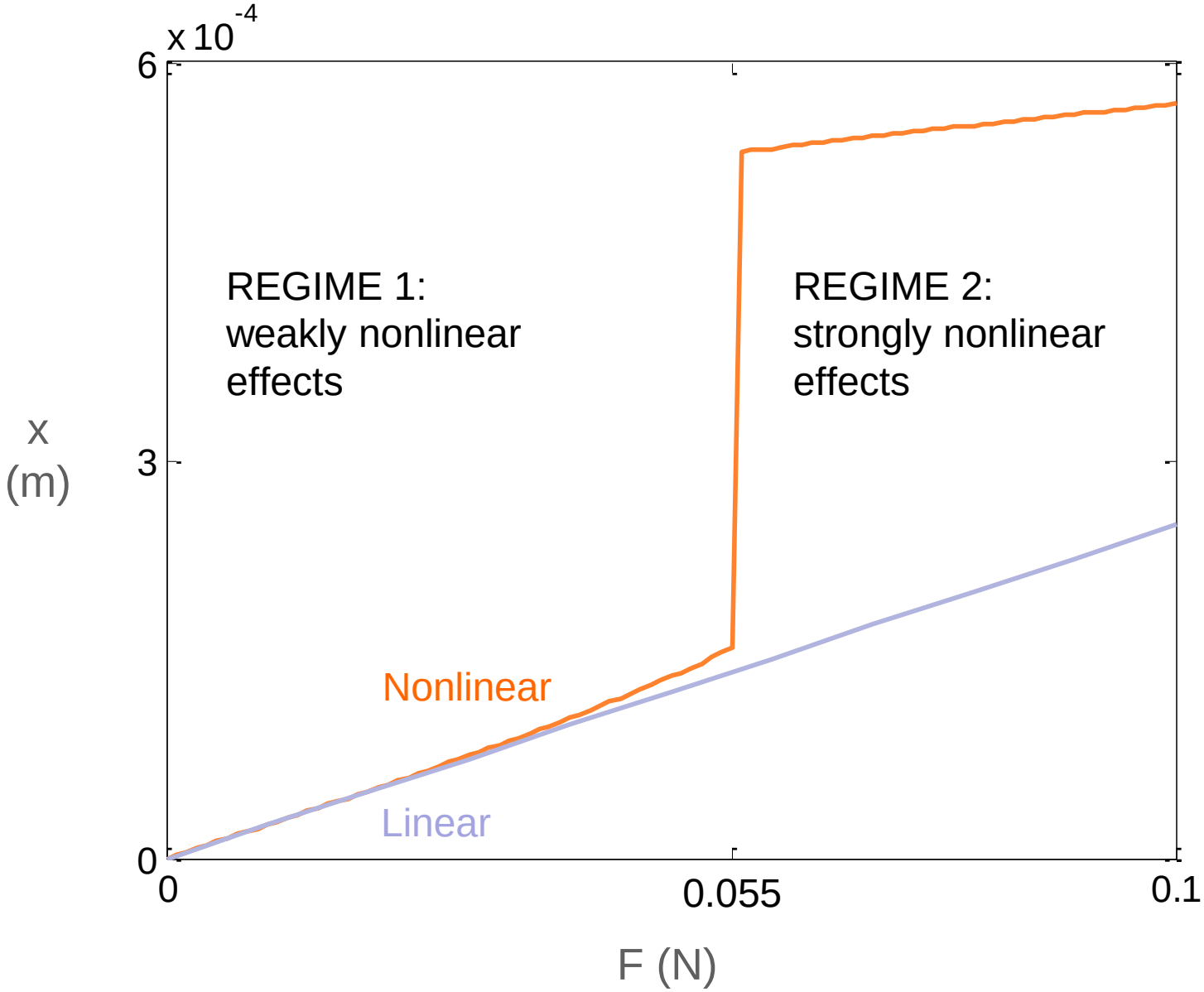


Course Objectives

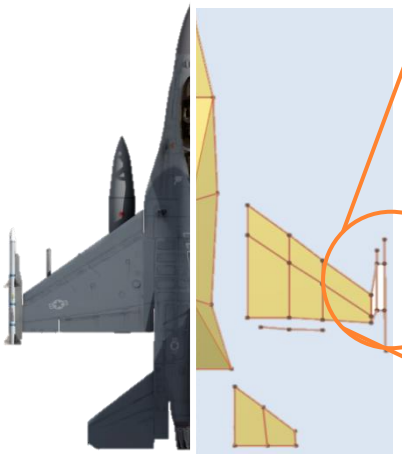
At the end of this course, you will

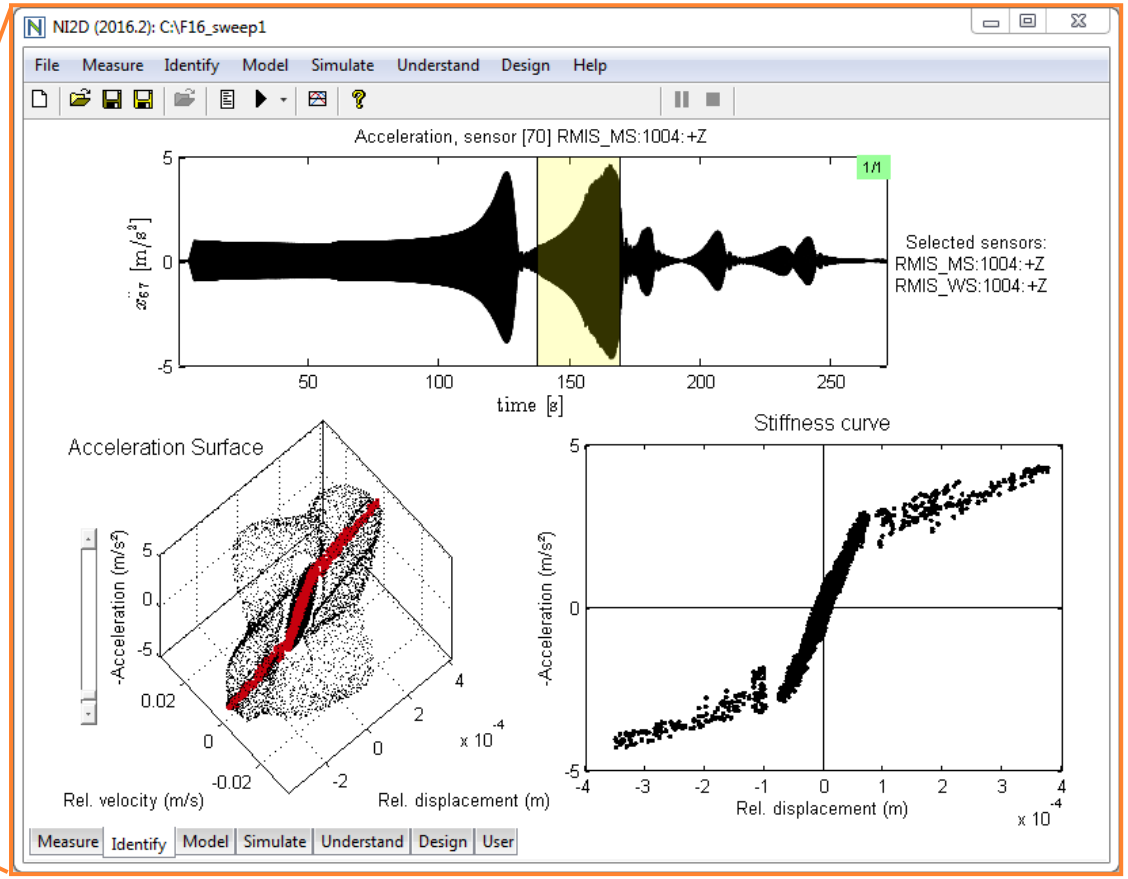
- Understand the impact of nonlinearity on system dynamics.
- Master the concepts of mode shape, resonance frequency and frequency response function of nonlinear systems.
- Be familiar with new nonlinear concepts incuding stability and bifurcations.
- Recognize nonlinearity in real-world (aerospace) structures.
- Know how to use the NI2D software.

You will be exposed to new theoretical concepts, advanced computational methods and practical experimental techniques

The Nonlinear Identification to Design Software

Nonlinear Identification to Design
Software





Course Outline

1. Brief review of linear theory
2. Impact of nonlinearity, nonlinear FRFs and 4 new concepts
3. Mathematical modeling and numerical computation
4. Nonlinear modes
5. Introduction to system identification and nonlinearity detection
6. Nonlinearity characterization
7. Nonlinear parameter estimation
8. Advanced concepts: bifurcations , modal interactions, isolas.
9. Industrial case study

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L01 Introduction

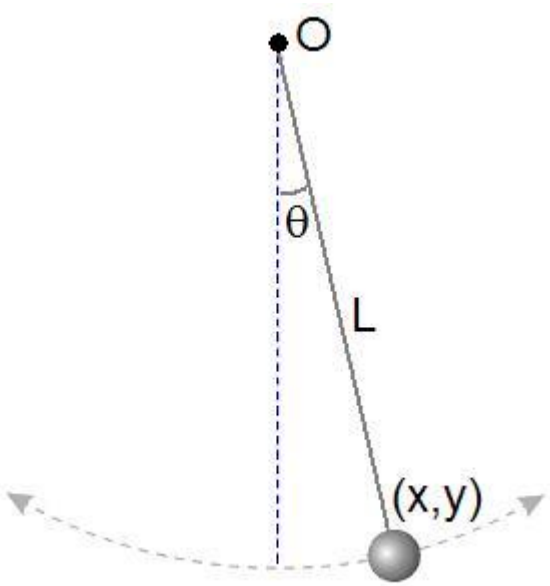
Course objectives

Review of linear theory

How To Write the Governing Equations ?

$$-\frac{d}{dt}\left(\frac{\partial T}{\partial \dot{q}_s}\right)+\frac{\partial T}{\partial q_s}-\frac{\partial V}{\partial q_s}-\frac{\partial D}{\partial q_s}+Q_s(t)=0, s=1,\dots n.$$

Lagrange equations for n generalized coordinates



$$T=\frac{1}{2}mL^2\dot{\theta}^2, \qquad V=mgL(1-cos\theta)$$

$$\ddot{\theta}+\frac{g}{L}\sin\theta=0$$

Let's Calculate the Period of the Motion

$$T + V = E$$

$$\frac{1}{2}mL^2\dot{\theta}^2 + mgL(1 - cos\theta) = mgL(1 - cos\theta_0)$$

$$\dot{\theta} = \frac{d\theta}{dt} = \pm\sqrt{\frac{2g}{L}(cos\theta - cos\theta_0)}$$

$$dt = \frac{d\theta}{\dot{\theta}} = \sqrt{\frac{L}{2g(cos\theta - cos\theta_0)}}d\theta$$

$$Period = 4\sqrt{\frac{L}{2g}}\int_0^{\theta_0}\frac{d\theta}{\sqrt{cos\theta - cos\theta_0}} = 2\pi\sqrt{\frac{L}{g}}\left[1 + \frac{{\theta_0}^2}{16} + \cdots\right]$$

The Linearization Around an Equilibrium

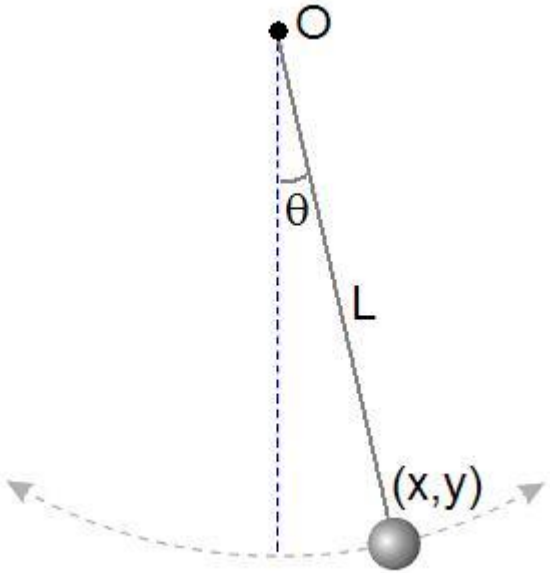
$$V(q) = \cancel{V(0)} + \sum_{s=1}^{n} \cancel{\left(\frac{\partial V}{\partial q_s}\right)_{q=0}} + \frac{1}{2}\sum_{s=1}^{n}\sum_{r=1}^{n}\left(\frac{\partial^2 V}{\partial q_s \partial q_r}\right)_{q=0} q_r q_s + \cdots$$

$$V(q) = \frac{1}{2}\sum_{s=1}^{n}\sum_{r=1}^{n} k_{rs} q_r q_s = \frac{1}{2} q^T K q$$

$$T(\dot{q}) = \frac{1}{2}\sum_{s=1}^{n}\sum_{r=1}^{n} m_{rs} \dot{q}_r \dot{q}_s = \frac{1}{2} \dot{q}^T M \dot{q}$$

$$\boxed{M\ddot{q} + Kq = 0}$$

The Linearization of the Pendulum



$$\ddot{\theta} + \frac{g}{L}\sin\theta = 0$$

$$\ddot{\theta} + \frac{g}{L}\left(\theta - \frac{\theta^3}{6} + \cdots\right) = 0$$

$\theta \ll 1$

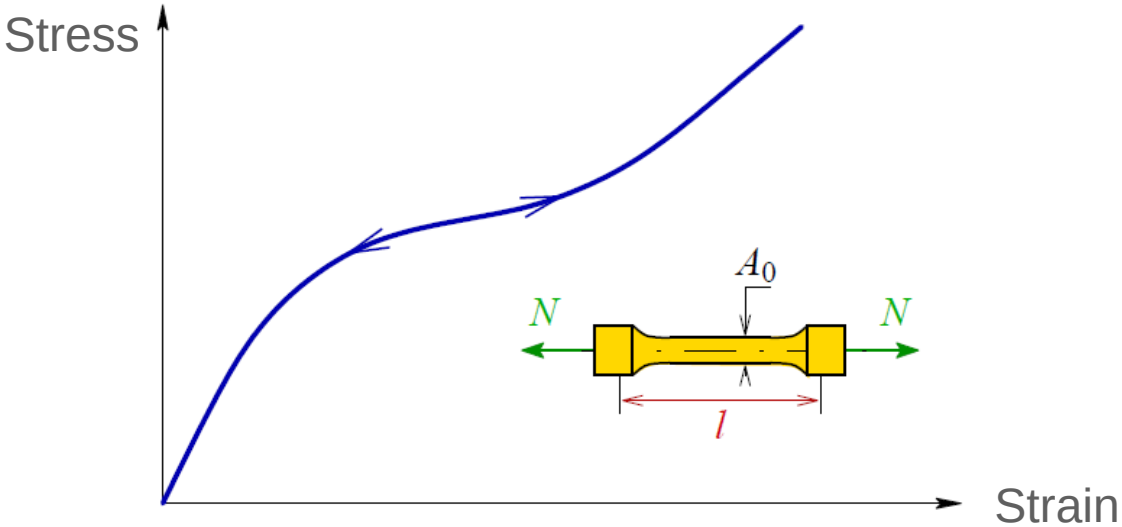
$$\boxed{\begin{gathered}\ddot{\theta} + \frac{g}{L}\theta = 0 \\ Period = 2\pi\sqrt{\frac{L}{g}}\end{gathered}}$$

3 Main Assumptions in Linear Structural Dynamics

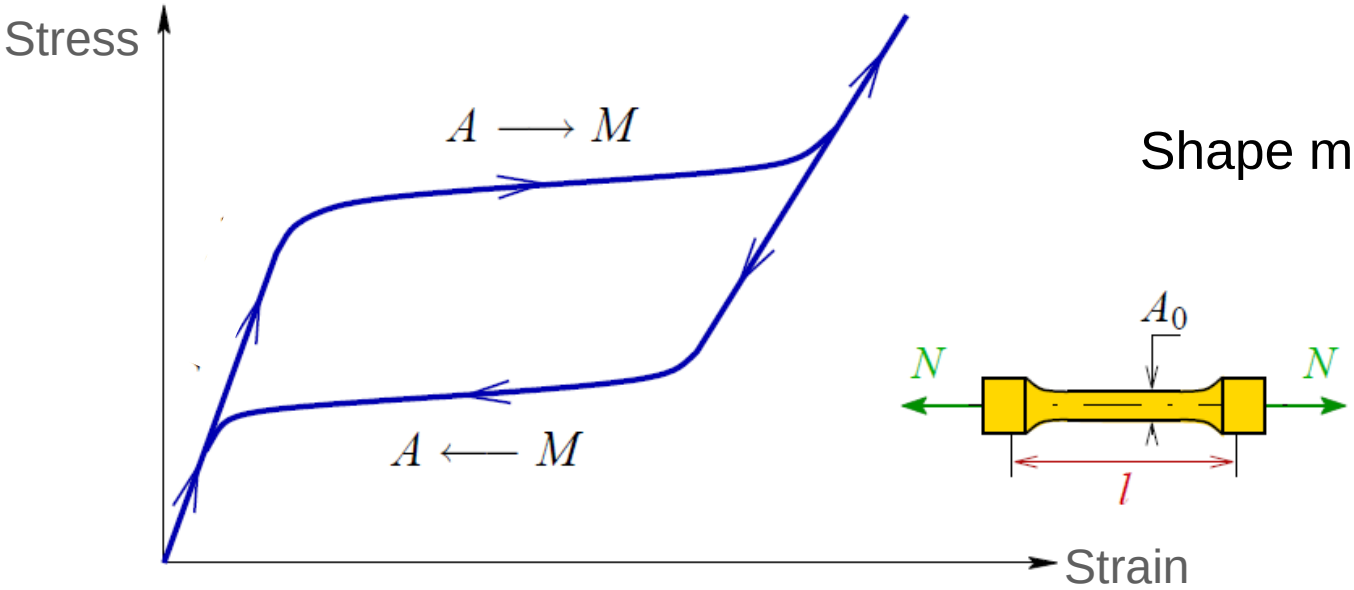
$$M\ddot{q} + C\dot{q} + Kq = 0$$

Linear elasticity	→ nonlinear materials
Small displ. and rotations	→ geometrical nonlinearity → nonlinear boundary conditions
Viscous damping	→ nonlinear damping mechanisms

Assumption 1: Nonlinear Materials

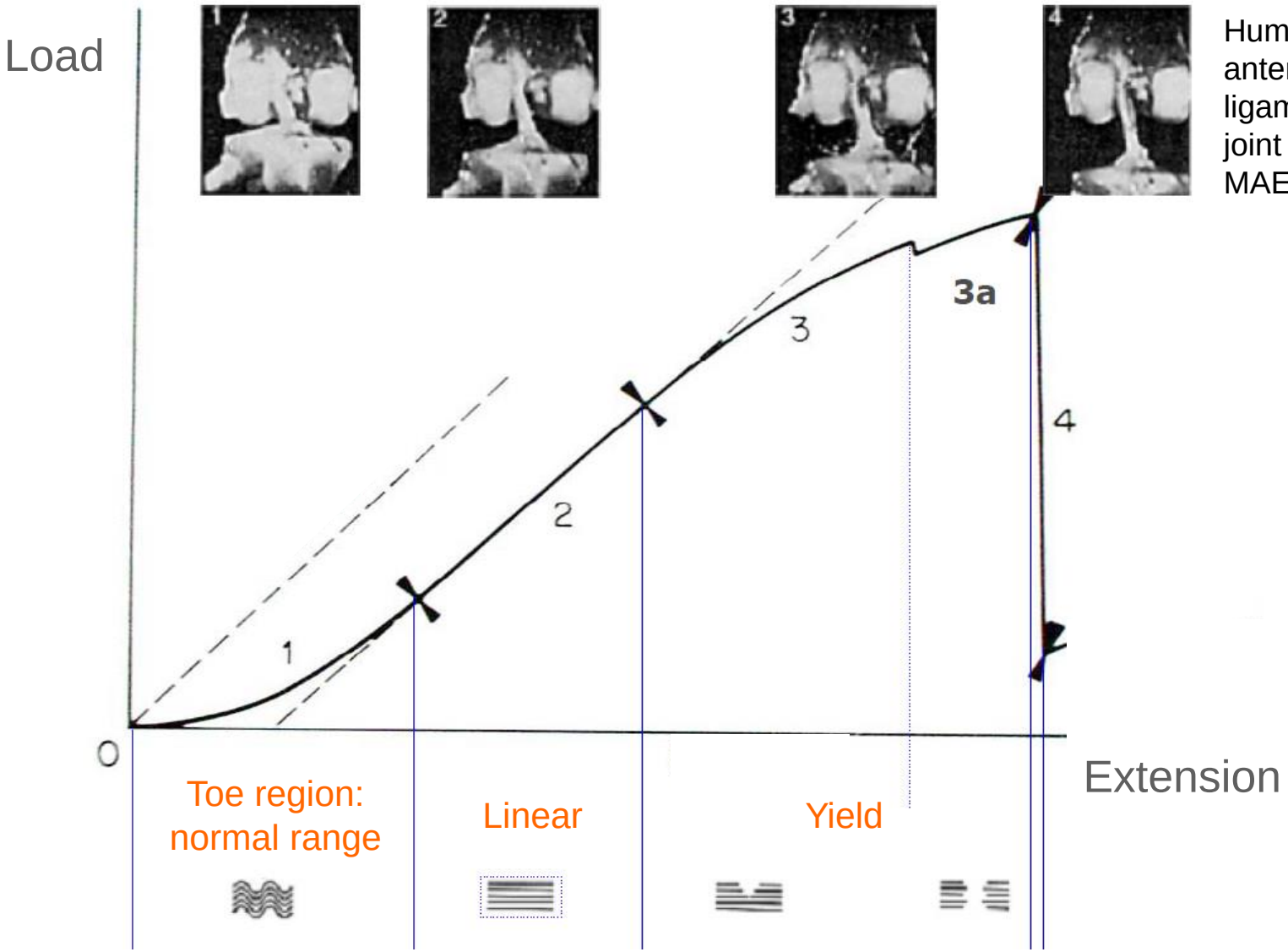


Hyperelastic material
(e.g., rubber)



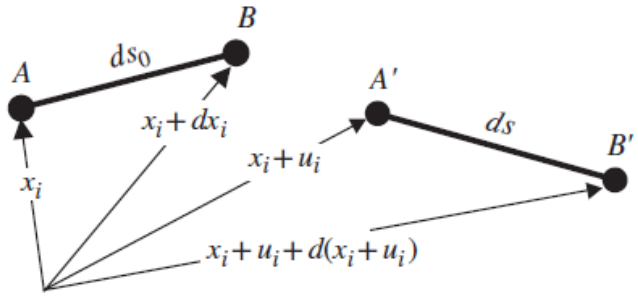
Shape memory alloy

Assumption 1: Ligament in Your Knee Joint



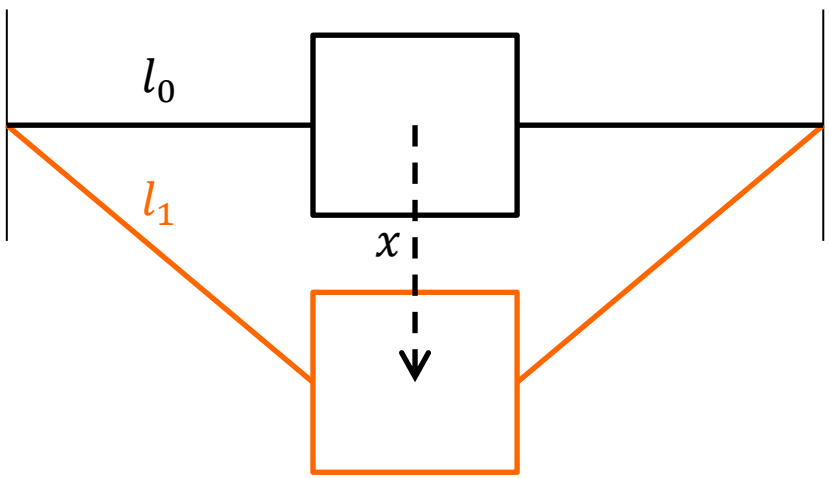
Human cadaveric anterior cruciate ligament in knee joint (Dr. Ziv, MAE, Buffalo)

Assumption 2: Geometrical Nonlinearities



$$\varepsilon_{ij} = \frac{1}{2}\left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} + \frac{\partial u_m}{\partial x_i}\frac{\partial u_m}{\partial x_j}\right)$$

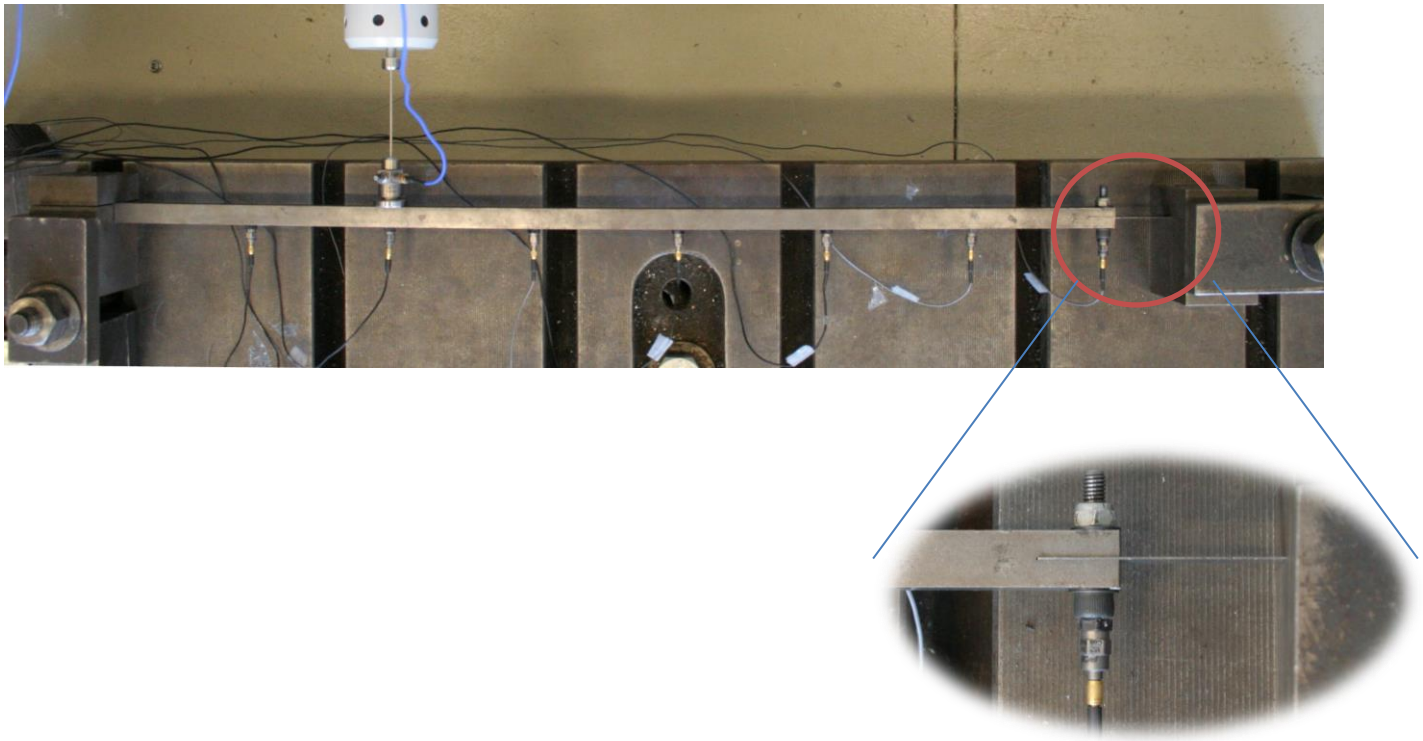
Green's strain tensor



$$F = 2k(l_1 - l_0)\frac{x}{l_1} = 2kx\left(1 - \frac{l_0}{\sqrt{x^2 + {l_0}^2}}\right)$$

$$\frac{l_0}{\sqrt{x^2 + {l_0}^2}} = 1 - \frac{x^2}{2{l_0}^2} + \frac{3x^4}{8{l_0}^4} + O(x^6)$$

Assumption 2: A Geometrical Beam in Our Lab



Assumption 3: Nonlinear Damping

Viscous damping but also…

Coulomb friction

Aerodynamic damping

The Concept of Mode Shape

$$M\ddot{q} + Kq = 0 \quad + \quad q = x\,\varphi(t)$$

Synchronous vibration of the structure

$$det(K - \omega^2 M) = 0$$

n natural frequencies

$$\left(K - \omega_{(r)}{}^2 M\right) x_{(r)} = 0$$

n normal modes

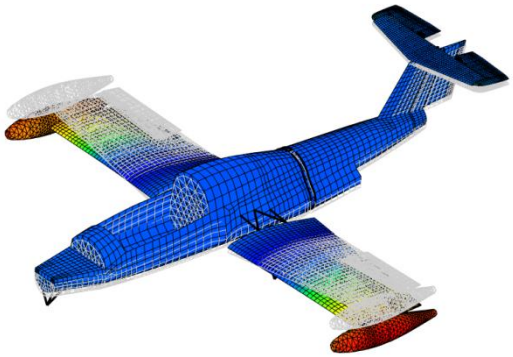
$$\varphi_r(t) = \alpha_r cos(\omega_r t) + \beta_r sin(\omega_r t)$$

normal coordinates

Normal Modes: Important Properties

Clear physical meaning:

- **Structural deformation at resonance**
- Synchronous vibration of the structure



Important mathematical properties:

- Orthogonality
- Decoupling of the equations of motion (modal superposition)
- Invariance

The Concept of FRF

$$M\ddot{q} + Kq = s\,cos(\omega t) \quad + \quad q = x\,cos(\omega t)$$

FRF

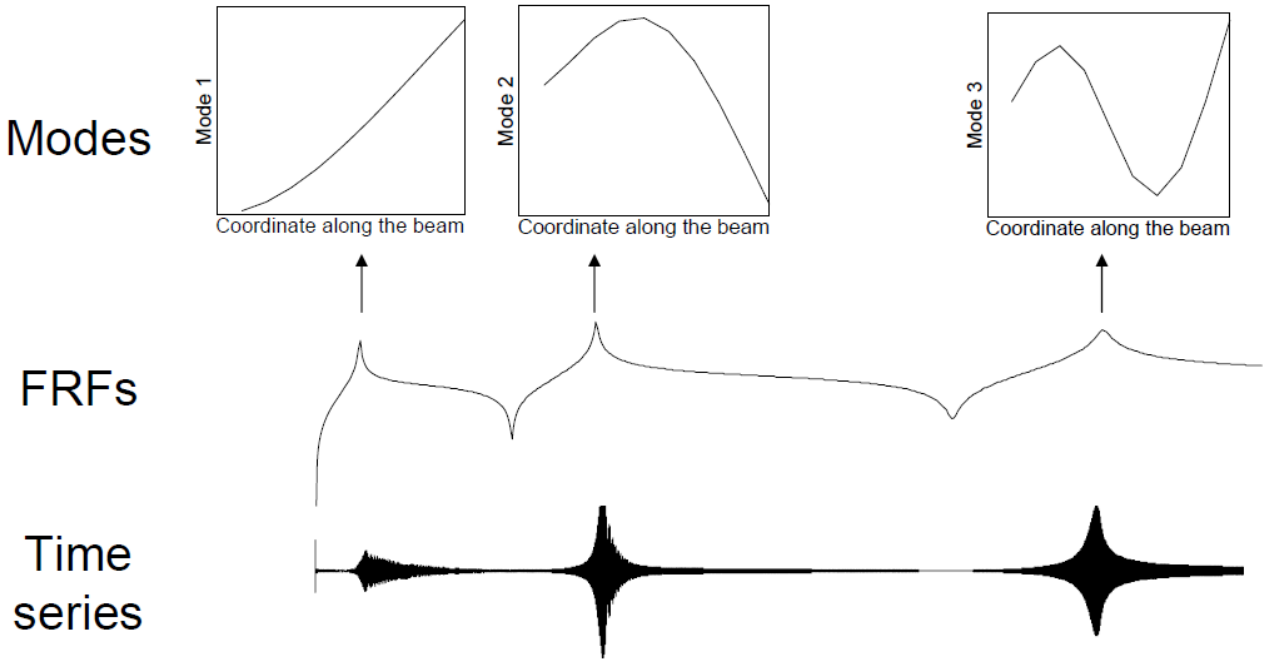
$$x = (K - \omega^2 M)^{-1} s = \boxed{H(\omega)}\, s$$

$$\boxed{H(\omega) = \sum \frac{x_{(s)} {x_{(s)}}^T}{({\omega_s}^2 - \omega^2)\mu_s}}$$

Clear link between the FRF
and the modal parameter

FRF: Important Properties

- The FRF is a constant system properties for a linear system
- FRF can be easily estimated from measured data
- Very convenient way of locating resonance frequencies



Time Response: Mode Displacement Method

$$M\ddot{q} + Kq = p(t) = g\,\varphi(t)$$

$$q(t) = \sum_{s=1}^{n} \frac{x_{(s)} x_{(s)}{}^{T} g}{\mu_s \omega_s} \int_0^t sin\omega_s(t-\tau)\,\varphi(t)d\tau$$

Exact

$$q(t) = \sum_{s=1}^{k<n} \frac{x_{(s)} x_{(s)}{}^{T} g}{\mu_s \omega_s} \int_0^t sin\omega_s(t-\tau)\,\varphi(t)d\tau$$

Approximate

Time Response: Numerical Integration

$\mathbf{M}, \mathbf{C}, \mathbf{K} \quad \mathbf{q}_0, \dot{\mathbf{q}}_0$

Compute $\ddot{\mathbf{q}}_0$

Time incrementation

$$t_{n+1} = t_n + h$$

Prediction

$$\dot{\mathbf{q}}^*_{n+1} = \dot{\mathbf{q}}_n + (1-\gamma)\, h\, \ddot{\mathbf{q}}_n$$

$$\mathbf{q}^*_{n+1} = \mathbf{q}_n + h\, \dot{\mathbf{q}}_n + (0.5-\beta)\, h^2\, \ddot{\mathbf{q}}_n$$

Computation of accelerations

$$\mathbf{S} = \mathbf{M} + h\,\gamma\,\mathbf{C} + h^2\,\beta\,\mathbf{K}$$

$$\mathbf{S}\,\ddot{\mathbf{q}}_{n+1} = \mathbf{p}_{n+1} - \mathbf{C}\,\dot{\mathbf{q}}^*_{n+1} - \mathbf{K}\,\mathbf{q}^*_{n+1}$$

Correction

$$\dot{\mathbf{q}}_{n+1} = \dot{\mathbf{q}}^*_{n+1} + h\,\gamma\,\ddot{\mathbf{q}}_{n+1}$$

$$\mathbf{q}_{n+1} = \mathbf{q}^*_{n+1} + h^2\,\beta\,\ddot{\mathbf{q}}_{n+1}$$

Newmark integration scheme for linear systems

Time Response: Numerical Integration

Newmark integration scheme for nonlinear systems

$\mathbf{M}, \mathbf{f}, \mathbf{p}, \mathbf{S} \quad \mathbf{q}_0, \dot{\mathbf{q}}_0$

Compute $\ddot{\mathbf{q}}_0$

$$\ddot{\mathbf{q}}_0 = \mathbf{M}^{-1}\left(\mathbf{g}_0 - \mathbf{f}(\dot{\mathbf{q}}_0, \mathbf{q}_0)\right)$$

Time incrementation

$$t_{n+1} = t_n + h$$

Prediction

$$\dot{\mathbf{q}}_{n+1} = \dot{\mathbf{q}}_n + (1-\gamma)\, h\, \ddot{\mathbf{q}}_n$$

$$\mathbf{q}_{n+1} = \mathbf{q}_n + h\, \dot{\mathbf{q}}_n + (0.5-\beta)\, h^2\, \ddot{\mathbf{q}}_n$$

$$\ddot{\mathbf{q}}_{n+1} = 0$$

Residual vector evaluation

$$\mathbf{r}_{n+1} = \mathbf{M}\, \ddot{\mathbf{q}}_{n+1} + \mathbf{f}_{n+1} - \mathbf{g}_{n+1}$$

Convergence ?

$$\|\mathbf{r}_{n+1}\| < \varepsilon\, \|\mathbf{f}_{n+1}\|$$

Yes

No

Calculation of the correction

$$\mathbf{S}(\mathbf{q}_{n+1})\, \Delta\mathbf{q} = -\mathbf{r}_{n+1}$$

Correction

$$\mathbf{q}_{n+1} = \mathbf{q}_{n+1} + \Delta\mathbf{q}$$

$$\dot{\mathbf{q}}_{n+1} = \dot{\mathbf{q}}_{n+1} + \frac{\gamma}{\beta\, h}\, \Delta\mathbf{q}$$

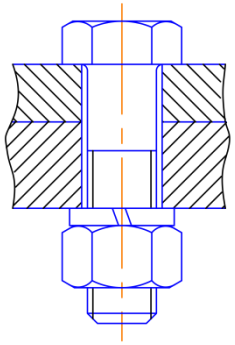
$$\ddot{\mathbf{q}}_{n+1} = \ddot{\mathbf{q}}_{n+1} + \frac{1}{\beta\, h^2}\, \Delta\mathbf{q}$$

Very Important: Sampling Frequency

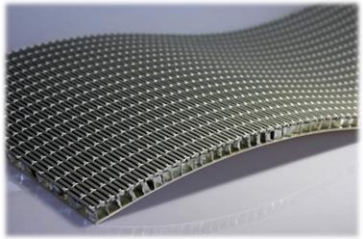
			Stability limit	Accuracy: Amplitude error	Accuracy: Periodicity error
Algorithm	γ	β	ωh	$\rho - 1$	$\frac{\Delta T}{T}$
Purely explicit	0	0	0	$\frac{\omega^2 h^2}{4}$	$-$
Central difference	$\frac{1}{2}$	0	2	0	$-\frac{\omega^2 h^2}{24}$
Fox & Goodwin	$\frac{1}{2}$	$\frac{1}{12}$	2.45	0	$O\left(h^3\right)$
Linear acceleration	$\frac{1}{2}$	$\frac{1}{6}$	3.46	0	$\frac{\omega^2 h^2}{24}$
Average constant acceleration	$\frac{1}{2}$	$\frac{1}{4}$	∞	0	$\frac{\omega^2 h^2}{12}$
Average constant acceleration (modified)	$\frac{1}{2}+\alpha$	$\frac{(1+\alpha)^2}{4}$	∞	$-\alpha\frac{\omega^2 h^2}{2}$	$\frac{\omega^2 h^2}{12}$

In Summary: Common Sources of Nonlinearity

Bolts, joints and gaps



Elastomers and composites



Friction and contact

Large amplitudes

In Summary: Important Linear Concepts/Methods

Mode shapes, resonance frequencies, damping ratios

Frequency response functions (FRFs)

Modal superposition/numerical integration

OPEN QUESTION:

Will they remain valid/useful for nonlinear systems ?